



# Functional Servicing and Stormwater Management Report

## **1580-1590 & 1650 Dundas Street East**

Official Plan Amendment and Zoning Bylaw  
Amendment Applications

Project No.: 20129

City of Mississauga, Ontario

Prepared For:

**Hazelview Investments**

Date: November 2021

Version: 1<sup>st</sup> Submission





## EXECUTIVE SUMMARY

This Functional Servicing and Stormwater Management Report ('FSSR') has been prepared to support official plan amendment ('OPA') and zoning bylaw amendment ('ZBA') applications for the site municipally known as 1580-1590 & 1650 Dundas Street East, Ontario (referred to as 'the site' or 'subject site').

The development proposal for the 7.39 ha site is to include for the development of 5 mixed-use development blocks, parkland and creek hazard dedications and an allowance for a future right of way bridge extension over Little Etobicoke Creek. The blocks will contain 13 buildings with a total of 3,027 units, along with 2,506m<sup>2</sup> and 449m<sup>2</sup> of retail and community space respectively. Mattawa Avenue is proposed to have a modified above grade cross-section, and widenings are proposed for both Mattawa Avenue and Dundas Street East.

The servicing strategy for the proposed development is summarized as follows:

### **Water Servicing:**

Mattawa Avenue contains a 300mm diameter watermain, which is the proposed watermain for all block level connections. The domestic and fire flow water demands were calculated in accordance with City of Mississauga criteria and FUS methodology. A fire hydrant connected into the Mattawa Avenue watermain was flow tested and confirmed that each block's critical water demands can be met by existing infrastructure.

### **Sanitary Servicing:**

Mattawa Avenue contains a 250mm diameter municipal sanitary sewer, which is the proposed watermain for all block level connections. The development proposal will result in an increase in equivalent population and peak flow to the Region's sewer system. A



summary of peak flow, along with the Region's multi-demand table, has been included in this report. It is our understanding that the Region will install a new 1200mm diameter trunk sewer under Mattawa Avenue, and the existing sewers in Mattawa Avenue will be connected into this trunk sewer.

### **Stormwater Servicing:**

The subject site currently drains stormwater to Mattawa Avenue and in turn Little Etobicoke Creek. All development blocks will have storm connections into the existing storm sewers within Mattawa Avenue. A comparison of City and TRCA stormwater management requirements were completed to establish required block level controls. Preliminary controls have been established in order to meet stormwater objectives.



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## 1.0 INTRODUCTION

### 1.1 Background

This Functional Servicing and Stormwater Management Report ('FSSR') has been prepared to support official plan amendment ('OPA') and zoning bylaw amendment ('ZBA') applications for the site municipally known as 1580-1590 & 1650 Dundas Street East, Ontario (referred to as 'the site' or 'subject site').

The development proposal for the 7.39 ha site is to include for the development of 5 mixed-use development blocks, parkland and creek hazard dedications and an allowance for a future right of way bridge extension over Little Etobicoke Creek. The blocks will contain 13 buildings with a total of 3,027 units, along with 2,506m<sup>2</sup> and 449m<sup>2</sup> of retail and community space respectively. Two to three levels of underground parking are contemplated, as shown on the architectural plans. Mattawa Avenue is proposed to have a new above grade cross-section along with a widening.

The subject site is currently divided into two separate blocks, with Parcel 1 being on the north-east side of Mattawa Avenue, and Parcel 2 being on the south-west side of Mattawa. Refer to the architectural plan extracts that are included in **Appendix A** for more information. **Figure 1 – Site Location** illustrates the subject site within the context of its surroundings. General project statistics are as follows in **Table 1**:



**Table 1: Project Summary**

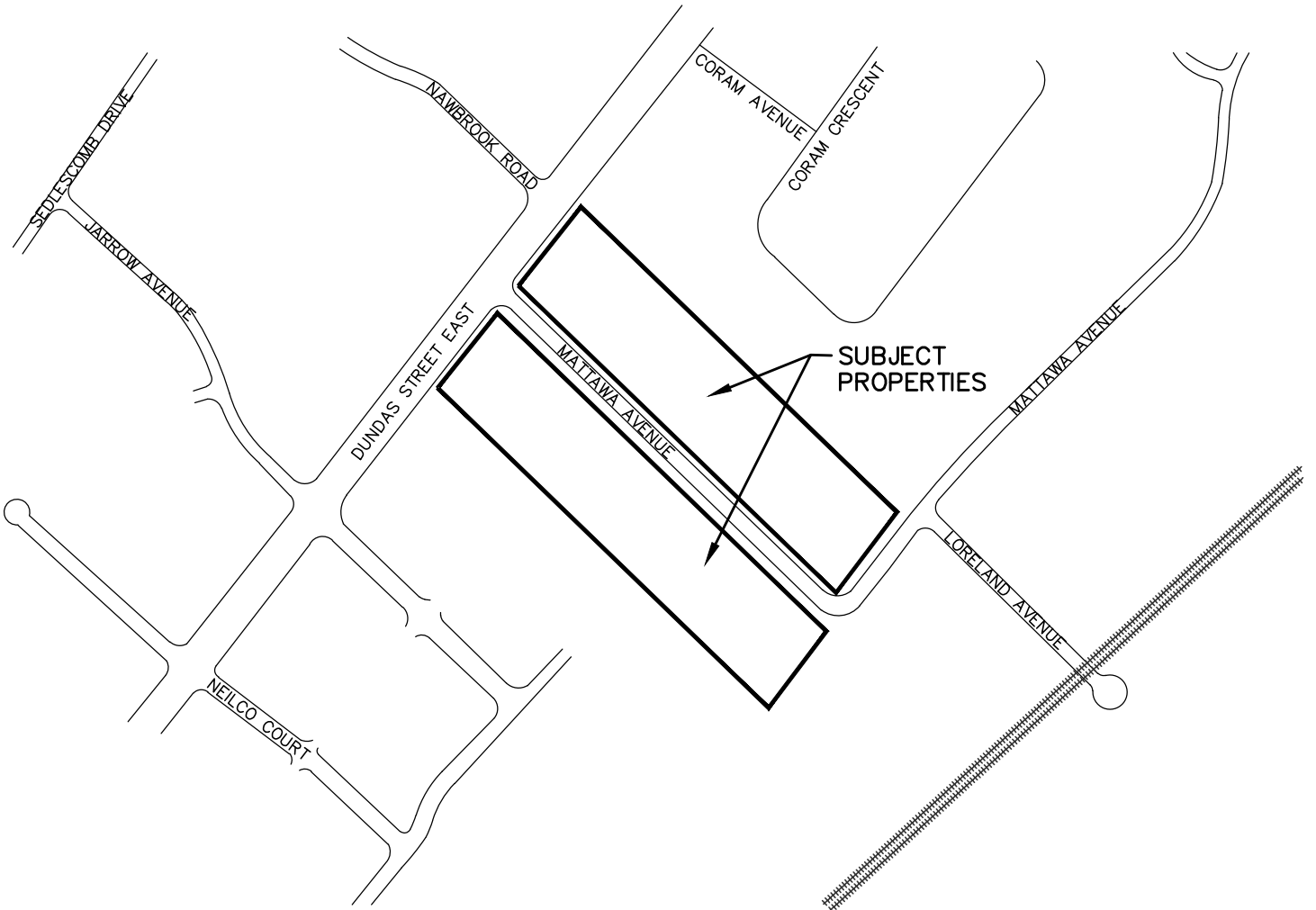
Block	ID Ref.	Building	Use	Block Area (m2)	Residential Units
<b>BLOCKS</b>					
A	1	A1, A2, A3	Residential & Retail	10,464.00	1,099
C	2	C1, C2, C3	Residential, Retail & Community	6,261.00	448
E	3	E1, E2, E3	Residential & Retail	12,779.00	533
F	4	F1, FTH-1, FTH-2, F3	Residential	12,329.00	407
G	5	G1, G2, GTH	Residential	11,255.00	540
H1	6	n/a	Creek Buffer	2,504.00	-
<b>Sub-Total - Blocks:</b>				<b>55,592.00</b>	<b>3,027</b>
<b>CONVEYANCES</b>					
B	7	n/a	Park	10,358.00	0
D1/D2	8	n/a	Hazard/Buffer	4,043.00	0
ROW 1	9	n/a	Loreland Avneue	385.00	0
ROW 2	10	n/a	Creek Overpass	1,888.84	0
ROW Widening A	11	n/a	Parcel 2 Widening	775.00	0
ROW Widening B	12	n/a	Parcel 1 Widening	847.00	0
<b>Sub-Total - Conveyances:</b>				<b>18,296.84</b>	<b>0</b>
<b>Total Parcel 1 (3+4+5+9+12):</b>				<b>37,595.00</b>	<b>1,480.00</b>
<b>Total Parcel 1 Developable Area (NIC Conveyances: 3+4+5):</b>				<b>36,363.00</b>	<b>1,480.00</b>
<b>Total Parcel 2 (1+2+6+7+8+10+11):</b>				<b>36,293.84</b>	<b>1,547.00</b>
<b>Total Parcel 2 Developable Area (NIC Conveyances: 1+2):</b>				<b>16,725.00</b>	<b>1,547.00</b>
<b>Total Original Site:</b>				<b>73,888.84</b>	<b>n/a</b>
<b>Total Developable Lands (NIC Conveyances):</b>				<b>53,088.00</b>	<b>3,027.00</b>

## 1.2 Study Parameters

This servicing assessment is based on:

- Stormwater Management Criteria, August 2012, TRCA.
- Peel Region Design Criteria (watermain and sanitary sewer), Region of Peel.
- Transportation and Works Department Requirements Manual, City of Mississauga.
- Plan and Profile and Sewershed Drawings, Region of Peel.
- MOE Design Guidelines for Drinking-water Systems, 2008.
- Architectural and Landscape Inputs, by SvN Architects + Planners.





### SITE LOCATION PLAN



DEVELOPMENT PROJECT  
AT MATTAWA AVENUE AND DUNDAS STREET EAST

MISSISSAUGA, ONTARIO

DRAWING BY: HK

CHECKED BY: DL

SCALE: N.T.S.

DATE: OCTOBER 2021

PROJECT NO.:  
**20129**

FIGURE NO.:  
**1**



## 2.0 WATER SUPPLY

### 2.1 Existing Water Supply

The adjacent municipal roadways contain available watermain servicing, as follows:

- Mattawa Avenue: 300mm diameter watermain.

A number of fire hydrants exist along Mattawa Avenue and are all connected into the existing 300mm diameter watermain. The existing development is currently serviced from the 300mm diameter watermain.

### 2.2 Proposed Water Supply

The proposed development is proposed to have multiple watermain connections into the existing 300mm diameter watermain in Mattawa Avenue. No mainline extensions are required to service the lands. The final number of block level connections will be determined at the Site Plan Approval stage of the project, however for the purpose of fire flow and domestic demand calculations, demands have been calculated on a block-by-block basis (i.e. a calculation for each of A, C, E, F and G).

The available municipal servicing should satisfy maximum day plus fire flow or the peak hour demand, whichever is greater. Fire demand is calculated using the Fire Underwriter Survey ('FUS') guidelines (1999).

Domestic water demands for the various blocks were calculated using Region of Peel criteria and by calculating equivalent populations by type of housing and land use and applying the multi-unit per capita demand of 280 l/cap/day for residential use. Given that the number of employees for retail space is not known, instead of the 300 L/employee/day rate prescribed in the Region guidelines, an MECP rate of 28 m<sup>3</sup>/floor ha/day was used.



Fire flows were estimated using FUS methodology. The following considerations were made as part of estimating fire flows:

- Fire Resistive type of construction for all buildings except townhouses, including adequately protected vertical openings.
- Ordinary Construction type construction for the townhouse blocks.
- Construction content factor for any blocks containing retail, otherwise, Limited Combustible factor.
- All system type reductions in place.

Floor-by-floor area breakdowns are not available at this stage of the project. As such, conservative area assumptions were made as part of the FUS calculations. For Block F, townhouse block F-TH1 governed the fire flow demand.

**Table 2: Summary of Water Demands**

Location	Daily Water Demand (L/sec)	Max Day Water Demand (L/sec)	Peak Hour Water Demand (L/sec)	Fire Demand Required (L/sec)	Max Day plus Fire Demand (L/sec)
A	7.37	14.72	22.10	166.67	181.38
C	3.28	6.53	9.83	116.67	123.20
E	3.96	7.90	11.87	183.33	<b>191.23</b>
F	3.16	6.32	9.48	166.67	172.23
G	4.12	8.24	12.35	150.00	158.24

As such, the governing maximum day plus fire flow demand rate is **191.23 L/s**.

A hydrant flow test was completed on July 23, 2021 by Lozzi Aqua Check, on a fire hydrant connected into the 300mm diameter watermain in Mattawa Avenue. The results of the test indicate that a flow rate of **441.34 L/s** could be achieved at a minimum fire pressure of 140 kPa (20 psi), which is greater than the governing block demand. As such, the municipal watermain system can accommodate the proposed development. Multi-



use demand tables have been included in **Appendix C**. Refer to **Appendix B** for all water demand calculations.

### 3.0 GROUNDWATER MANAGEMENT

Discharge of groundwater and foundation drains to municipal sewers must be in accordance with the Region of Peel and/or City of Mississauga requirements.

A Permit to Take Water (PTTW) from the Ontario Ministry of the Environment, Conservation and Parks (MECP) is required for short term water taking over 400 m<sup>3</sup>/day. An Environmental Activity and Sector Registry (EASR) is required from the MECP for short term water taking between 50 m<sup>3</sup>/day and 400 m<sup>3</sup>/day. A PTTW is required for long term water taking from a permanent drainage system greater than 50 m<sup>3</sup>/day.

The hydrogeological report, prepared by Terrapex, provides high level estimates of construction (short-term) and permanent (long-term) dewatering, based on various block sizes and their levels of underground parking. The rates are as follows:

**Table 3: Groundwater Discharge Summary**

Block (m <sup>2</sup> )	Construction Dewatering (L/day)			Long-Term Dewatering (L/day)
	Temporary	25mm Storm	Total	
+/- 3,300 (2 Levels)	13,000	82,500	95,500	12,000
+/- 10,350 (2 Levels)	47,400	258,750	306,150	41,778
+/- 15,000 (3 Levels)	57,786	375,000	432,786	57,786

Construction dewatering will be designed by a qualified dewatering contractor, with MECP permitting applied for as required (EASR is expected). A rate of 57,786 L/day (**0.67 L/s**), as a conservative estimate for the largest permanent long term dewatering rate by block, should be easily managed through discharge to the sewer system, subject to approval from the Region of Peel and/or City of Mississauga. It is our understanding that the Region of Peel will soon not permit groundwater connections into their sanitary sewer system.



Should this occur, either the owner will be required to design without foundation drains, or will be required to treat, control and discharge groundwater to the City's storm sewer system, in accordance with City requirements and the control requirements outlined in Section 5.0 of this report.

## 4.0 SANITARY SERVICING

### 4.1 Existing Sanitary Servicing

The adjacent municipal roadways contain available separated sanitary servicing, as follows:

- Mattawa Avenue: 250mm diameter sanitary sewers.

The sewers in Mattawa Avenue converge at the point where Mattawa turns 90 degrees, at the southern end of the property. At this point, the sewers travel through private property through an easement, travels south-east parallel to Little Etobicoke Creek and connects into the existing 1200mm diameter trunk sewer, near the railway bridge overpass.

It is our understanding that the Region will be undertaking a project that will propose a new 1200mm diameter trunk sewer in Mattawa Avenue, spanning from Dundas Street East to the existing trunk connection point at the railway bridge overpass. The existing 250mm diameter local sewers in Mattawa Avenue will remain in place, however they will be connected into this new trunk sewer in Mattawa Avenue. The continuation of the trunk sewer will require a new easement on the subject lands (within Block B).

The existing site is currently serviced by the Mattawa Avenue sanitary sewer. Based on an estimated 1.55 ha of existing retail/commercial space, the existing sanitary peak flow has been estimated to be **2.92 L/s**. Refer to **Appendix C** for sanitary calculations.



## 4.2 Proposed Sanitary Servicing

All development blocks are proposed to be serviced by the existing 250mm diameter sanitary sewers in Mattawa Avenue. An extension of the sewer at the north-east part of Mattawa Avenue will be required to service Blocks A and E. For the purpose of re-zoning, we have provided 1 control maintenance hole per building within each block, to satisfy building code requirements. The control maintenance hole allocated to each building is in **Table 4** below.

**Table 4: Servicing Connections per Building**

Block	Building	San. Control MH	Stm. Control MH
A	A1	MH1A	MH1
	A2	MH3A	
	A3	MH5A	
B	Park	n/a	MH7
C	C1	MH15A	MH3
E	E1	MH8A	MH2
	E2	MH10A	
	E3	MH12A	
F	F1	MH14A	MH4
	FTH-1	MH18A	
	FTH-2	MH19A	
	F3	MH16A	
G	G1	MH20A	MH8
	G2	MH21A	
	GTH	MH22A	
ROW 2	Creek Overpass	n/a	MH5

Unit and non-residential floor area breakdowns by building are not available at this time. However, this breakdown is available by block. As such, for the purpose of capacity



assessment, we have calculated peak flows generated by each block. Multi-use demand tables were also prepared by block and are included in **Appendix C**.

In accordance with Region criteria, person per unit rates of 1.6 and 3.0 were used for small (<750 sq.ft.) and large (>750 sq.ft.) apartment units. The architectural plans do not provide unit size information; however a reasonable assumption was made that only studio and 1 bedroom units qualify as small units. Based on these equivalent populations and a generation rate of 302.8 L/cap/day, peak flows by block are presented below in Table 5. The cumulative peak flow from each block has been calculated to be **88.51 L/s**, or an increase of **85.59 L/s**. Refer to drawing SW-S for the location of servicing connections and Appendix C for sanitary calculations and multi-use demand sheets.

Typically, the Region of Peel will analyze the capacity of the existing sewer system to determine if the development can be supported without upgrades.

**Table 5: Sanitary Peak Flow Summary**

Locations		Domestic Flows			Infiltration Flows		Totals
Area	Ctrl. MH Connections	Total Units	Total Population	Domestic Flows (L/s)	Site Area (ha)	Infiltration Flows (L/s)	Total Flow (L/s)
Block A	1A, 3A, 5A	1099	2269	<b>28.17</b>	1.05	1.05	<b>29.22</b>
Block C	15A	448	940	<b>12.58</b>	0.63	0.41	<b>12.98</b>
Block E	8A, 10A, 12A	533	1136	<b>14.98</b>	1.28	1.10	<b>16.08</b>
Block F	14A, 18A, 19A, 16A	407	910	<b>12.20</b>	1.23	1.37	<b>13.57</b>
Block G	20A, 21A, 22A	540	1186	<b>15.59</b>	1.13	1.07	<b>16.66</b>
<b>TOTALS:</b>		3027	6441	<b>83.53</b>	5.31	4.98	<b>88.51</b>



## 5.0 STORMWATER SERVICING

### 5.1 Existing Stormwater Drainage

The existing Mattawa Avenue right-of-way contains an available storm sewer system that collects and conveys drainage towards the south. The site is tributary to Little Etobicoke Creek. The entire site eventually drains towards the creek and is therefore considered to have one outlet. See drawings **SWM1A** and **SWM1B** for the Pre-Development Drainage Plans. Areas 100 and 101 represent existing developed areas that are captured in existing private site services and conveyed to Mattawa Avenue. R100 is the existing Mattawa Avenue right-of-way, while the remaining areas are uncontrolled. All flows being conveyed on-site and within Mattawa Avenue are directed towards a 1200mm storm sewer that drains northeast to southwest towards Little Etobicoke Creek.

In accordance with TRCA criteria for the Etobicoke Creek Watershed, VO6 software has been utilized to calculate pre-development peak runoff for the 2-year up to the 100-year storm event based on the 6-hour AES design storms. The results have been shown below in **Table 6**. Since Mattawa Avenue, which is represented as Area R100, is an existing right-of-way, it has been excluded from the model for the stormwater management calculations. Refer to **Appendix D** for the VO6 Model output, pre-development condition analysis. No information is available for any existing controls on the developed lands and therefore have been assumed to be uncontrolled for the purpose of the analysis.





**Table 6: Overall Site Pre-Development Peak Flows**

Return Period	Total Site to Little Etobicoke Creek (L/s)
<b>(AES 6-hours)</b>	
2-Year	543
5-Year	747
10-Year	885
25-Year	1,079
50-Year	1,214
100-Year	1,347

## **5.2 Proposed Storm Servicing**

Each development block will require a minimum of one storm connection to the existing sewers in Mattawa Avenue. Further consultation with City of Mississauga staff is required to determine the number of required connections to each block/tower in order to meet Ontario Building Code requirements. Refer to **Table 4** for a summary of control maintenance holes and the blocks they service and drawing **SW-S**.

## **5.3 Stormwater Management Criteria**

The stormwater management design has been prepared in accordance with the criteria of the City of Mississauga (City) and the Toronto and Region Conservation Authority (TRCA).

### **5.3.1 City of Mississauga Stormwater Management Criteria**

The City's SWM criteria is set out in the Transportation and Works Department Requirements Manual (Manual) dated November 2020.



#### 5.3.1.1 Water Balance

- The minimum on-site runoff retention requires the proponent to retain the first 5mm of runoff on-site, which equates to about 50% of the total average annual rainfall volume, through infiltration/bioretention, evapotranspiration and/or rainwater reuse.

**At a minimum, all runoff from a 5mm event will be retained on site through initial abstraction, infiltration, evapotranspiration and/or rainwater reuse.**

#### 5.3.1.2 Water Quality

- Require average removal of 80% of TSS on an annual loading basis from all runoff leaving the site. (Suspended solids removal efficiency is to be calculated based on 100% of the total runoff volume resulted from all storm events that occur in an average year.)
- Overall efficiency in TSS removal can be considered in combination with minimum on-site runoff retention and other conveyance & end-of-pipe controls (i.e. the treatment train).

**A TSS removal of 80% is required, calculated based on a treatment train approach.**

#### 5.3.1.3 Water Quantity

- Stormwater quantity control varies depending on the watershed and should conform to the criteria set out by the corresponding conservation authority (ie. TRCA, CH and CVC) based on the watershed.

**The quantity controls shall achieve TRCA quantity control requirements.**

#### 5.3.2 TRCA Criteria

As the site is located within the Etobicoke Creek watershed, the TRCA's Stormwater Management Criteria dated August 2012 have been assessed for requirements that are



additional to the City criteria. From Table 2.2 and Table 3-1, the criteria as it applies to this development as follows:

### 5.3.2.1 Stormwater Quantity

For Etobicoke Creek, control post-development peak flows to the Etobicoke Creek Watershed delineated unit rates for all storms up to and including the 100-year storm (i.e. 2, 5, 10, 25, 50, and 100-year storms). The site is in the Little Etobicoke Creek tributary and the specific unit release rates for the site's location are found in Table I1 of Appendix A in the TRCA Stormwater Management Criteria. The applied unit release rates and the site's resulting allowable rates are shown in **Table 7**.

**Table 7: TRCA Allowable Unit Rates Flows for the Site**

Return Period	Unit Runoff Rates (L/s/ha)	Total Site Allowable Release Rates (L/s)
2-Year	21.5	141.5
5-Year	33	217.1
10-Year	41	269.8
25-Year	55	361.9
50-Year	62.7	412.6
100-Year	71.8	472.4

The TRCA unit release rates in **Table 7** result in very small release rates, which are less than pre-development conditions rates even for landscaped areas. As such, the TRCA rates will govern quantity control release rates for the site. The return period peak flows are based on the 6-hour AES design storm events. Refer to **Appendix D** for further information on TRCA's Little Etobicoke Creek watershed Criteria and unit release rate calculations. The total site area release rates are based on the limits of the storm drainage areas of the development blocks.



**Control the site's post-development peak flows to the TRCA's Little Etobicoke Creek Watershed defined unit rates for all storms up to and including the 100-year storm.**

#### **5.3.2.2 Erosion**

- At a minimum retain 5 mm on site where conditions do not warrant the detailed analyses.
- If a site drains to a sensitive creek or a sub watershed, a study or MESP is required, then the proponent must complete a geomorphologic assessment study to determine the site appropriate erosion threshold.
- For sites with SWM ponds, 25mm - 48hr detention may also be required, depending on the results of the erosion assessment.

The proposed development does not meet the criteria requiring erosion control and we believe there will be no measurable impact on erosion in the Little Etobicoke Creek.

**The site shall apply best efforts to retain 5mm of runoff depth.**

#### **5.3.2.3 Stormwater Quality**

Enhanced Level of Protection (80% TSS removal) as per the latest MOE SWMPD Manual is required.

**TSS removal of 80% is required.**

#### **5.3.2.4 Water Balance**

- For Low Volume Groundwater Recharge Areas (LGRA), site specific water balance analyses are typically not required, and best efforts to maintain recharge are expected.



- For natural features (woodlands, wetlands, watercourses) maintain hydrologic regimes and hydroperiods.

**Reasonable best efforts to maintain or enhance groundwater recharge.**

**5.3.3 Consolidated Stormwater Criteria**

**Table 8** below presents the consolidated City and TRCA criteria.

**Table 8: Consolidated Stormwater Management Criteria**

Criteria	City	TRCA
<b>Water Balance</b>	All runoff from a 5mm event will be retained on site through infiltration, evapotranspiration & rainwater reuse.	Reasonable best efforts to maintain or enhance groundwater recharge.
<b>Stormwater Quality</b>	TSS removal of 80% is required.	TSS removal of 80% is required.
<b>Stormwater Quantity</b>	The post-development peak runoff rates shall conform to TRCA criteria. Overland flow route to safely convey major drainage to municipal right-of-way.	Control post-development peak flows to the TRCA's Little Etobicoke Creek watershed defined unit rates for all storms up to and including the 100-year storm.
<b>Erosion Control</b>	Not Required.	Retain 5mm on site

**5.4 Proposed Stormwater Management Approach**

A hierarchical approach has been used to arrive at the proposed stormwater management strategy for this development. Consistent with this approach, it is proposed that all the



development blocks will have internal treatment and control facilities that will fully address the water balance, quality treatment and quantity control requirements for the individual blocks. Refer to drawings **SWM2A** and **SWM2B** for the Post-Development Drainage Plans. The sum of the limits of the development block drainage areas have been considered as the total site area for the purposes of the stormwater management calculations. Since Mattawa Avenue is an existing public road, the drainage patterns of the road will generally be maintained and have been excluded from stormwater management calculations. However, a road widening is proposed on Mattawa Avenue, therefore the additional widening area has been accounted for by including those widened areas in the individual development blocks as a conservative approach. The site also includes a Park Block (Area 214) and a block allocated for a future right-of-way bridge (R201) that crosses over Little Etobicoke Creek. These two blocks will be public areas and shall be uncontrolled, however they were accounted for as part of the overall stormwater management approach. The private development blocks shall implement additional quantity controls to compensate for the released flows for the two public blocks to ensure that the total site released flows achieve allowable release rates. Quality control for the roads will be addressed with a treatment train approach of directing runoff from impermeable areas to landscaped areas where feasible, retaining the 5mm storm event within the blocks, and an oil/grit separator ('OGS') unit at the connection of each of the blocks. Based on the proposed plan, preliminary sizing of the storm water management facilities was completed for each development block. The detailed design of these facilities will occur as part of the future Site Plan Approval process for the development blocks.

#### 5.4.1 Residential/Retail Blocks with Underground Garages

The stormwater management requirements for these blocks will be met using a combination of green roofs/landscaping, rainwater harvesting and quantity control cisterns and oil/grit separators.



**Water Balance** – It is proposed that all rainfall events up to the 5mm storm will be retained on site for these blocks. This will be done through the use of green roofs/landscaping and rainwater harvesting. Harvested rainfall will be stored in underground garage cisterns and be used for irrigation purposes. Refer to **Table 9** and **Appendix D** for detailed calculations.

**Water Quality** - Oil/grit separators will provide 50% treatment for roof, exposed parking areas and driveways. Landscaped areas will be conveyed directly to a rainwater cistern. A level of 80% or more TSS removal will be achieved for blocks based on 100% of the total runoff volume resulted from all storm events that occur in an average year. Refer to **Table 10** and **Appendix D**, Water Quality for detailed calculations.

**Water Quantity** – The proposed 2 to 100-year storms will be controlled to allowable rates (using TRCA defined unit rates for the Little Etobicoke Creek watershed) with implementation of underground garage cisterns/storage facilities with Hydrovex units or orifice plates. See **Table 11** and **Appendix D** for calculations. The private development blocks shall overcontrol the release rates in order to compensate for the uncontrolled future right-of-way bridge (Area R201) and the public park block.

**SWM DESIGN CALCULATIONS**

**Table 9: Initial Abstraction/Water Balance Credit Summary Table (Post-development)**

**Project Name:** 1580-1590 & 1650 Dundas Street East  
**Municipality:** Mississauga, ON  
**Project No.:** 20129  
**Date:** 27-Oct-21

**Prepared by:** J.L.  
**Checked by:** R.K.  
**Last Revised:** 27-Oct-21

Block	Area (ha)	Initial Abstraction On-site Credits						Additional Credit for Reuse or Infiltration Storage		Total Block Level Water Balance Credit with Reuse Storage (mm)	Total Water Balance Credit with Reuse Storage Per 6.58ha Entire Site (mm)
		Landscape/ Permeable Pavement (5mm Credit)	Green Roof (5mm Credit)	Roof (1mm Credit)	Roof/Paved to Landscape (5mm Credit)	Paved (1mm Credit)	Total On-site Initial Abstraction Credit (mm)	Additional Reuse or Infiltration Storage (m <sup>3</sup> )	Additional Reuse or Infiltration Storage (mm)		
<b>BLOCK A</b>	1.045	15%	13%	35%	0%	37%	2.1	38	3.6	5.7	0.9
<b>BLOCK E</b>	1.299	14%	11%	34%	0%	42%	2.0	49	3.8	5.8	1.1
<b>BLOCK C</b>	0.627	30%	6%	48%	0%	16%	2.4	20	3.2	5.6	0.5
<b>BLOCK F</b>	0.950	4%	4%	11%	0%	54%	1.1	42	4.4	5.5	0.8
<b>BLOCK G</b>	1.435	16%	9%	30%	0%	45%	2.0	54	3.8	5.8	1.3
<b>ROW R201</b>	0.189	0%	0%	0%	0%	100%	1.0	0	0.0	1.0	0.0
<b>PARK BLOCK</b>	1.035	93%	0%	0%	7%	0%	5.0	0	0.0	5.0	0.8
<b>Sub-Total</b>	<b>6.580</b>						<b>2.4</b>	<b>203</b>			<b>5.5</b>

\* Therefore, in overall the site post-development Initial Abstraction credit is 5.5mm.



SWM DESIGN CALCULATIONS

Table 10: Post-development TSS Removal Calculation Results Summary (using New Jersey Stormwater Best Management Practices Manual , Chapter 4 - TSS Removal Rates for BMP's in Series)

Project Name: 1580-1590 & 1650 Dundas Street East  
Municipality: Mississauga, ON  
Project No.: 20129  
Date: 27-Oct-21

Prepared by: J.L.  
Checked by: R.K.  
Last Revised: 27-Oct-21

TSS Removal Treatment Train Approach

Block	Area (ha)	Stage 1. Land Use (% of area) for TSS Removal Credits							Stage.3 End of Pipe Quality Treatment					TSS Removal Credit Per 6.58ha Entire Site
		Landscape / Permeable Pavement (80% TSS Removal Credit)	Green Roof (80% TSS Removal Credit)	Roof (80% TSS Removal Credit)	Roof/Paved to Landscape (80% TSS Removal Credit)	Paved (0% TSS Removal Credit)	Total On-site TSS Removal Credit	Remaining Untreated TSS	5mm Retention (50% TSS Removal Credit*)	Cumulative On-site TSS Removal Credit	Remaining Untreated TSS	OGS (50% TSS Removal Credit)	Complete TSS Removal Individual	
BLOCK A	1.045	15%	13%	35%	0%	37%	51%	49%	50%	75%	25%	50%	88%	13.9%
BLOCK E	1.299	14%	11%	34%	0%	42%	47%	53%	50%	73%	27%	50%	87%	17.1%
BLOCK C	0.627	30%	6%	48%	0%	16%	67%	33%	50%	83%	17%	50%	92%	8.7%
BLOCK F	0.950	4%	4%	11%	0%	54%	16%	84%	50%	58%	42%	50%	79%	11.4%
BLOCK G	1.435	16%	9%	30%	0%	45%	44%	56%	50%	72%	28%	50%	86%	18.8%
Public ROW R201	0.189	0%	0%	0%	0%	100%	0%	100%	0%	0%	100%	0%	0%	0.0%
PARK BLOCK	1.035	93%	0%	0%	7%	0%	80%	20%	0%	80%	20%	0%	80%	12.6%
<b>Sub-Total</b>	<b>6.58</b>													<b>83%</b>

\*5mm water retention is equivalent to 50% of annual rainfall. Therefore, removing this volume from hydrologic cycle reduces TSS load by 50%.

Reference: New Jersey Stormwater Best Management Practices Manual  
Chapter 4 - TSS Removal Rates for BMP's in Series

**SWM DESIGN CALCULATIONS**  
**Table 11: Water Quantity Calculation Results Summary (SWM Matrix)**

Project Name: 1580-1590 & 1650 Dundas Street East  
Municipality: Mississauga, ON  
Project No.: 20129  
Date: 27-Oct-21

Prepared by: J.L.  
Checked by: R.K.  
Last Revised: 27-Oct-21

Block	Drainage Area [ha]	Total Roof Area (ha)	Roof Drain to Grass (ha)	Imp. Side Walk Drain to Grass (ha)	Roof / Imp. Drain to Grass (%)	Green Roof (ha)	Green Roof (% of Roof)	Paved Surface Impervious Area (ha)	Landscape / Permeable Pavement (ha)	Imperviousness (%)	X-Imperviousness (%)	Water Balance Target (mm)	Quantity Control Target	Water Balance/Cistern Storage Required (m <sup>3</sup> )	Quantity Control Storage Utilized during 100-year storm (m <sup>3</sup> )	Blocks Target 100-year Release Rate (l/s)	VO6 Model 100-year Blocks Release Rate (l/s)	Quantity Storage Provided (m <sup>3</sup> )
<b>BLOCK A</b>	1.045	0.505	0.00	0.000	0	0.136	27%	0.385	0.155	72	72	5	TRCA Unit Release Rates	38	560	58	27	561
<b>BLOCK E</b>	1.299	0.582	0.00	0.000	0	0.143	25%	0.540	0.177	75	75	5	TRCA Unit Release Rates	49	708	72	30	709
<b>BLOCK C</b>	0.627	0.335	0.00	0.000	0	0.035	10%	0.103	0.189	64	64	5	TRCA Unit Release Rates	20	317	35	16	318
<b>BLOCK F</b>	0.950	0.527	0.00	0.000	0	0.063	12%	0.382	0.041	89	89	5	TRCA Unit Release Rates	42	570	53	18	571
<b>BLOCK G</b>	1.435	0.561	0.00	0.000	0	0.133	24%	0.645	0.228	75	75	5	TRCA Unit Release Rates	54	792	79	32	793
<b>ROW R201</b>	0.189	0.000	0.00	0.000	0	0.000	-	0.189	0.000	100	100	N/A	Uncontrolled	-	-	-	39	-
<b>PARK BLOCK</b>	1.035	0.000	0.00	0.000	0	0.000	-	0.077	0.958	7	0	N/A	Uncontrolled	-	-	-	137	-
<b>SubTotal (including external areas)</b>	<b>6.580</b>	<b>2.51</b>				<b>0.51</b>		<b>2.32</b>	<b>1.75</b>					<b>203</b>	<b>2947</b>	<b>472</b>	<b>299</b>	<b>2952</b>



## 5.5 Consolidation of Stormwater Management Approach

In this section of the report, the results from overall proposed development are consolidated and it is demonstrated that the proposed stormwater management approach meets or exceeds the criteria of the City and TRCA for the overall site.

### 5.5.1 Consolidated Water Balance Control

As shown in **Table 9**, the proposed Stormwater Management Approach will retain at least 5mm of rainfall on site. Refer to **Table 9** and **Appendix D** for more detail. **Table 12** summarizes the consolidated water balance outcome for the entire site.

**Table 12: Consolidated Water Balance Summary for Entire Site**

SWM Item	Target	Post-Development
<b>Water Balance</b>	5mm Retained on Site	5.5mm Retained on Site

### 5.5.2 Consolidated Water Quality Control

As shown in **Table 10**, the proposed Stormwater Management Approach will provide an overall 83% of TSS removal for the entire site. Therefore, the 80% TSS removal requirement has been satisfied. Refer to **Table 9** and **Appendix D** for more detail. **Table 13** below summarizes the consolidated water quality outcome for the entire site.

**Table 13: Consolidated Water Quality Summary for Entire Site**

SWM Item	Target	Post-Development
<b>Water Quality</b>	80% TSS Removal	83% TSS Removal



### 5.5.3 Consolidated Water Quantity Control

#### 5.5.3.1 Design Criteria

As previously discussed, all development blocks will provide their own quantity storage to control post-development 2-year to 100-year storm flows to the TRCA allowable unit release rates or less. This will also satisfy the City's quantity control requirement for the individual development blocks.

#### 5.5.3.2 Modeling

The following section provides detail of criteria and data which have been utilized in the modeling process:

The VISUAL-OTTHYMO Version 6 (VO6) Model has been employed to analyse the 2 to 100-year storm events for both pre-development and post-development conditions. The design storm events used in this analysis are based on the 6-hours AES storm events in accordance with the TRCA guidelines for the watershed. The 2-year to 100-year storm events were modelled with a time step of 5 minutes.

The proposed site development drainage areas have been modelled in VO6 using the STANHYD commands with the SCS Formula for areas with impervious areas, and NASHYD commands with CN values for landscaped and undeveloped areas. In the post-development conditions, flows from the individual development blocks have been routed through underground storage tanks on each block. The ROUTE RESERVOIR command has been used to model the SWM storage tanks. Refer to **Appendix D** for post-development VO6 model schematic and calculations, and drawings **SWM2A** and **SWM2B** for post-development drainage areas. The post-development VO6 model input parameters have been summarized in **Table 14**.

The required quantity storage for all development blocks have been provided in **Table 11**. For the current submission, it has been assumed that each of the development blocks shall have a single flow restriction device (orifice or vortex unit) to control all the design



storms from the 2-year to the 100-year storm event. **Therefore, the development block controls have been preliminarily sized to control the 100-year storm event to the 2-year allowable release rate for the controlled portions of the blocks. However, during detailed design of the development blocks, there is opportunity to optimize the required storage volume and detention time within the stormwater storage tanks by providing a more efficient outlet, such as a multi-staged outlet. The current storage volumes provide a more general approach to the quantity controls. Refer to Appendix D for details and VO6 modeling used to arrive at these storage volumes.**

The results of the consolidated water quantity modeling for the site outletting to Little Etobicoke Creek has been summarized in **Table 15** below. As seen in the table, all total post-development flows have been controlled down to the allowable release rates or less. Quantity controls are therefore achieved.

Any overland flows exceeding minor system capacity will be conveyed safely downstream through Mattawa Avenue and towards the existing Loreland Avenue right-of-way. The overland flows include emergency and/or uncontrolled flows from the blocks, park and open space areas, which would not be captured by minor system.



**Table 14: VO6 Modelling Parameters (Post-Development)**

Block ID	Area ID	VO6 Command	Area (ha)	IMP	CN
<b>Block A (202)</b>	202	STANHYD	0.939	0.70	85
<b>Block A (202A)</b>	2022	STANHYD	0.073	0.99	85
<b>Block A (U202)</b>	2021	STANHYD	0.033	0.65	85
<b>Block C (207)</b>	207	STANHYD	0.559	0.63	85
<b>Block C (207A)</b>	2071	STANHYD	0.068	0.74	85
<b>Block E (200)</b>	200	STANHYD	0.456	0.67	85
<b>Block E (201)</b>	201	STANHYD	0.729	0.80	85
<b>Block E (201A)</b>	2011	STANHYD	0.077	0.73	85
<b>Block E (U201)</b>	2012	STANHYD	0.032	0.65	85
<b>Block E (U200)</b>	2002	NASHYD	0.005	-	85
<b>Block F (204)</b>	204	STANHYD	0.127	0.75	85
<b>Block F (205)</b>	205	STANHYD	0.221	0.99	85
<b>Block F (206)</b>	206	STANHYD	0.514	0.88	85
<b>Block F (206A)</b>	2061	STANHYD	0.045	0.82	85
<b>Block F (208)</b>	208	STANHYD	0.043	0.75	85
<b>Block G (203)</b>	203	STANHYD	0.181	0.32	85
<b>Block G (210)</b>	210	STANHYD	0.139	0.92	85
<b>Block G (211)</b>	211	STANHYD	0.106	0.75	85
<b>Block G (212)</b>	212	STANHYD	0.217	0.92	85
<b>Block G (213)</b>	213	STANHYD	0.677	0.80	85
<b>Block G (213A)</b>	2131	STANHYD	0.115	0.72	85
<b>Future ROW (R201)</b>	2201	STANHYD	0.189	0.99	85
<b>Park Block Pervious (214)</b>	2141	NASHYD	0.673	-	85
<b>Park Block 20% IMP (214)</b>	2142	STANDHYD	0.362	0.20	85



**Table 15: Consolidated Water Quantity Peak Flows Summary (L/s)**

Location	Return Period	Total Pre-Development Flows (L/s)	TRCA Unit Release Rates (L/s)	Total Post-Development Flows (L/s)
<i>Entire Site (To Little Etobicoke Creek)</i>	2-Year	543	141.5	101
	5-Year	747	217.1	152
	10-Year	885	269.8	186
	25-Year	1,079	361.9	231
	50-Year	1,214	412.6	266
	100- Year	1,347	472.4	300

### 5.6 Low Impact Development Measures

The underground structure levels of the various development blocks encompass the majority of the available private block areas. As such, there are no viable locations to implement low impact development ('LID') measures that are of the infiltration types.

However, the landscape architect has proposed LID's that will inherently improve stormwater management, as follows:

- **Green Roof Systems:** allow for absorption, detention and evapotranspiration of stormwater.
- **Rain Gardens:** provide bioretention and filtration of stormwater prior to entering the building plumbing system or municipal sewer system.
- **Rainwater Harvesting:** reuse of stormwater through irrigation means and will likely achieve the majority of the 5mm water balance target at block level design.

All LID's will be designed at the site plan approval stage of the project.



## 6.0 CONCLUSIONS

This FSSR presents a site servicing strategy for the proposed development that addresses the requirements of the applicable regulatory agencies.

Sincerely,

**Counterpoint Engineering Inc.**



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## **APPENDIX 'A'**

### **Architectural Inputs**









## **APPENDIX 'B'**

### **Water Calculations**

**Counterpoint Engineering Inc.**

**WATER DEMANDS BY BLOCK AND BUILDING**

Project: 1580-1590 & 1650 Dundas Street East  
 Project No: 20129  
 Location: Mississauga

**Per Capita Demand**

Residential	280 litres/person/day
ICI	300 litres/emp./day

**Retail/Residential Population Criteria**

Small (< 750 ft.sq.)	1.6 ppu
Large (> 750 ft.sq.)	3.0 ppu
Commercial/Retail	50 persons/ha
Community	50 persons/ha

**Unit and Floor Area Breakdown**

Block	Units	Unit Type Count		
		St. / 1 Bdrm.	2 Bdrm.	3 Bdrm.
A	1099	737	263	99
C	448	293	115	40
E	533	334	152	47
F	407	222	150	35
G	540	310	181	49
	3027	1896	861	270

	Suite Size Breakdown (> or < 750 ft.sq.)			
	Min (m2)	Max (m2)	Min (sq.ft.)	Max (sq.ft.)
Studio	34	42	366	452
1 Bedroom	45	65	484	700
2 Bedroom	68	74	732	797
3 Bedroom	80	94	861	1012

*As such, Studio and 1 Bedroom units are considered 'small' units, with 2 and 3 Bedroom units being 'Large' units.*

POPULATION AND AVERAGE DAY DEMANDS SUMMARY													
Location	1 Bedroom Units	2 Bedroom Units	3 Bedroom Units	Total Residential Units*	Total Residential Population	Residential Average Demand	Community (m <sup>2</sup> )	Total Community Population	Community Average Demand	Commercial (m <sup>2</sup> )	Total Commercial Population	Commercial Average Demand	
	1.6 persons/unit	3.0 persons/unit	3.0 persons/unit	Units	Equivalent Population	L/s	Area	Equivalent Population	L/s	Area	Equivalent Population	L/s	
A	737	263	99	1099	2265	7.34	-	0.0	0.00	759.0	3.8	0.02	
C	293	115	40	448	934	3.24	449.0	2.2	0.01	841.0	4.2	0.03	
E	334	152	47	533	1131	3.93	-	0.0	0.00	906.0	4.5	0.03	
F	222	150	35	407	355	1.23	-	0.0	0.00	-	0.0	0.00	
G	310	181	49	540	1186	4.12	-	0.0	0.00	-	0.0	0.00	
Totals:	1,896	861	270	3,027	5,872	19.86	449	2	0.01	2,506	13	0.08	

**Peaking Factors**

Land Use	Maximum Hour	Maximum Day
Residential	3.00	2.00
ICI	3.00	1.40

**Summary of Demands**

Block	Daily Water Demand (L/sec)	Max Day Water Demand (L/sec)	Peak Hour Water Demand (L/sec)	Fire Demand Required (L/sec)	Max Day plus Fire Demand (L/sec)
A	7.37	14.72	22.10	166.67	181.38
C	3.28	6.53	9.83	116.67	123.20
E	3.96	7.90	11.87	183.33	191.23
F	1.23	2.47	3.70	166.67	169.13
G	4.12	8.24	12.35	150.00	158.24

# Counterpoint Engineering Inc.

## REQUIRED FIRE FLOW WORKSHEET - PROPOSED DEVELOPMENT

Project: 1580-1590 & 1650 Dundas Street East  
 Project No: 20129  
 Building: A

Guide for Determination of Required Flow Copyright I.S.O

$$F = 220C\sqrt{A}$$

where  
 F = the required fire flow in litres per minute.  
 C = coefficient related to the type of construction.  
 = 1.5 for wood frame construction (structure essentially all combustible).  
 = 1.0 for ordinary construction (brick or other masonry walls, combustible floor and interior).  
 = 0.8 for non-combustible construction (unprotected metal structural components, masonry or metal walls).  
 = 0.6 for fire-resistive construction (fully protected frame, floors, roof).  
 A = The total floor area in square metres (including all storeys, but excluding basements at least 50 percent below grade) in the building being considered.

Type of Construction		Class Factor
WF	Wood Frame	1.5
OC	Ordinary Construction	1.0
NC	Non-Combustible	0.8
FC	Fire-Resistive	0.6

Area Notes for Fire Resistive Buildings (from FUS manual, 1999):

If Vertical Openings are inadequately protected (less than 1-hour fire rating): Area is the total of the two largest adjoining floors (above ground level) plus 50% of the area of each of the next 8 adjoining floors above that.

Contents		% Reduction
NC	Non-Combustible	25
LC	Limited Combustible	15
C	Combustible	0
FB	Free Burning	15
RB	Rapid Burning	25

If Vertical Openings are adequately protected (at least 1-hour fire rating): Area is the total of the largest floor (above ground level) plus 25% of the area of each of the next 2 immediately adjoining floors above that.

1) **Fire Flow**  
 Type of Construction: 

FC
0.6

  
 C = 

0.6
-----

  
 A = 12,600.00 m<sup>2</sup>  
 F = 14,817 L/min

2) **Occupancy Reduction/Surcharge**  
 Contents Factor: 

C
0%

  
 Reduction/Surcharge of 

0
---

 L/min  
 F = 14817 L/min + 0 L/min = 14,817 L/min

3) **System Type Reduction**  
 NFPA 13 Sprinkler: 

YES	30%
-----	-----

  
 Standard Water Supply: 

YES	10%
-----	-----

  
 Fully Supervised: 

YES	10%
-----	-----

  
**Total**

50%	50%
-----	-----

  
 Reduction of 

7,408
-------

 L/min  
 F = 14817 L/min - 7,408 L/min = 7,408 L/min

4) **Separation Charge**  
 Building Face

Dist(m)	Charge	
North	61	0%
East	32	5%
South	14	15%
West	95	0%
<b>Total</b>		20%

of 14817 L/min = 2,963 L/min  
 (max exposure charge can be 75%)

Separation	Charge	Separation	Charge
0 to 3m	25%	20.1 to 30 m	10%
3.1 to 10m	20%	30.1 to 45m	5%
10.1 to 20m	15%		

F = 7408 L/min + 2963 L/min = 10,372 L/min (2,000 L/min < F < 45,000 L/min)

F =	10,000	L/min	(round to the nearest 1,000 L/min)
F =	167	L/s	
F =	2,642	gpm	



# Counterpoint Engineering Inc.

## REQUIRED FIRE FLOW WORKSHEET - PROPOSED DEVELOPMENT

**Project:** 1580-1590 & 1650 Dundas Street East  
**Project No:** 20129  
**Building:** C

Guide for Determination of Required Flow Copyright I.S.O

$$F = 220C\sqrt{A}$$

where

- F = the required fire flow in litres per minute.  
 C = coefficient related to the type of construction.  
 = 1.5 for wood frame construction (structure essentially all combustible).  
 = 1.0 for ordinary construction (brick or other masonry walls, combustible floor and interior).  
 = 0.8 for non-combustible construction (unprotected metal structural components, masonry or metal walls).  
 = 0.6 for fire-resistive construction (fully protected frame, floors, roof).  
 A = The total floor area in square metres (including all storeys, but excluding basements at least 50 percent below grade) in the building being considered.

Type of Construction		Class Factor
WF	Wood Frame	1.5
OC	Ordinary Construction	1.0
NC	Non-Combustible	0.8
FC	Fire-Resistive	0.6

Area Notes for Fire Resistive Buildings (from FUS manual, 1999):

If Vertical Openings are inadequately protected (less than 1-hour fire rating): Area is the total of the two largest adjoining floors (above ground level) plus 50% of the area of each of the next 8 adjoining floors above that.

Contents		% Reduction
NC	Non-Combustible	25
LC	Limited Combustible	15
C	Combustible	0
FB	Free Burning	15
RB	Rapid Burning	25

If Vertical Openings are adequately protected (at least 1-hour fire rating): Area is the total of the largest floor (above ground level) plus 25% of the area of each of the next 2 immediately adjoining floors above that.

1) **Fire Flow**  
 Type of Construction: 

FC
0.6

  
 C = 

0.6
-----

  
 A = 

5,250.00
----------

 m<sup>2</sup>  
 F = 

9,564
-------

 L/min

2) **Occupancy Reduction/Surcharge**  
 Contents Factor: 

C
0%

  
 Reduction/Surcharge of = 

0
---

 L/min  
 F = 9564 L/min + 

0
---

 L/min = 

9,564
-------

 L/min

3) **System Type Reduction**  
 NFPA 13 Sprinkler: 

YES	30%
-----	-----

  
 Standard Water Supply: 

YES	10%
-----	-----

  
 Fully Supervised: 

YES	10%
-----	-----

  
**Total**

50%
-----

  
 Reduction of 

50%
-----

 L/min = 

4,782
-------

 L/min  
 F = 9564 L/min - 

4,782
-------

 L/min = 

4,782
-------

 L/min

4) **Separation Charge**  
 Building Face

Dist(m)	Charge	
North	14	15%
East	32	5%
South	100	0%
West	95	0%
<b>Total</b>	<b>20%</b>	<b>of 9564.31 L/min = 1,913 L/min</b>

(max exposure charge can be 75%)

Separation	Charge	Separation	Charge
0 to 3m	25%	20.1 to 30 m	10%
3.1 to 10m	20%	30.1 to 45m	5%
10.1 to 20m	15%		

F = 4782 L/min + 1913 L/min = 

6,695
-------

 L/min (2,000 L/min < F < 45,000 L/min)

F =	7,000	L/min	(round to the nearest 1,000 L/min)
F =	117	L/s	
F =	1,849	gpm	

# Counterpoint Engineering Inc.

## REQUIRED FIRE FLOW WORKSHEET - PROPOSED DEVELOPMENT

**Project:** 1580-1590 & 1650 Dundas Street East  
**Project No:** 20129  
**Building:** E

Guide for Determination of Required Flow Copyright I.S.O

$$F = 220C\sqrt{A}$$

where  
**F** = the required fire flow in litres per minute.  
**C** = coefficient related to the type of construction.  
 = 1.5 for wood frame construction (structure essentially all combustible).  
 = 1.0 for ordinary construction (brick or other masonry walls, combustible floor and interior).  
 = 0.8 for non-combustible construction (unprotected metal structural components, masonry or metal walls).  
 = 0.6 for fire-resistive construction (fully protected frame, floors, roof).  
**A** = The total floor area in square metres (including all storeys, but excluding basements at least 50 percent below grade) in the building being considered.

Type of Construction		Class Factor
WF	Wood Frame	1.5
OC	Ordinary Construction	1.0
NC	Non-Combustible	0.8
FC	Fire-Resistive	0.6

Area Notes for Fire Resistive Buildings (from FUS manual, 1999):

If Vertical Openings are inadequately protected (less than 1-hour fire rating): Area is the total of the two largest adjoining floors (above ground level) plus 50% of the area of each of the next 8 adjoining floors above that.

Contents		% Reduction
NC	Non-Combustible	25
LC	Limited Combustible	15
C	Combustible	0
FB	Free Burning	15
RB	Rapid Burning	25

If Vertical Openings are adequately protected (at least 1-hour fire rating): Area is the total of the largest floor (above ground level) plus 25% of the area of each of the next 2 immediately adjoining floors above that.

1) **Fire Flow**  
 Type of Construction: 

FC
0.6

  
 C = 

0.6
-----

  
 A = 

11,250.00
-----------

 m<sup>2</sup>  
 F = 

14,001
--------

 L/min

2) **Occupancy Reduction/Surcharge**  
 Contents Factor: 

C
0%

  
 Reduction/Surcharge of = 

0
---

 L/min  
 F = 14001 L/min + 

0
---

 L/min = 

14,001
--------

 L/min

3) **System Type Reduction**  
 NFPA 13 Sprinkler: 

YES	30%
-----	-----

  
 Standard Water Supply: 

YES	10%
-----	-----

  
 Fully Supervised: 

YES	10%
-----	-----

  
**Total**

50%
-----

  
 Reduction of 

50%
-----

 L/min = 

7,000
-------

 L/min  
 F = 14001 L/min - 

7,000
-------

 L/min = 

7,000
-------

 L/min

4) **Separation Charge**  
 Building Face

Dist(m)	Charge	
North	65	0%
East	29	10%
South	23	10%
West	32	5%
<b>Total</b>		<b>25%</b>

 of 14000.7 L/min = 

3,500
-------

 L/min  
 (max exposure charge can be 75%)

Separation	Charge	Separation	Charge
0 to 3m	25%	20.1 to 30 m	10%
3.1 to 10m	20%	30.1 to 45m	5%
10.1 to 20m	15%		

F = 7000 L/min + 3500 L/min = 

10,501
--------

 L/min (2,000 L/min < F < 45,000 L/min)

F =	11,000	L/min	(round to the nearest 1,000 L/min)
F =	183	L/s	
F =	2,906	gpm	

# Counterpoint Engineering Inc.

## REQUIRED FIRE FLOW WORKSHEET - PROPOSED DEVELOPMENT

**Project:** 1580-1590 & 1650 Dundas Street East  
**Project No:** 20129  
**Building:** F

Guide for Determination of Required Flow Copyright I.S.O

$$F = 220C\sqrt{A}$$

where  
**F** = the required fire flow in litres per minute.  
**C** = coefficient related to the type of construction.  
 = 1.5 for wood frame construction (structure essentially all combustible).  
 = 1.0 for ordinary construction (brick or other masonry walls, combustible floor and interior).  
 = 0.8 for non-combustible construction (unprotected metal structural components, masonry or metal walls).  
 = 0.6 for fire-resistive construction (fully protected frame, floors, roof).  
**A** = The total floor area in square metres (including all storeys, but excluding basements at least 50 percent below grade) in the building being considered.

Type of Construction		Class Factor
WF	Wood Frame	1.5
OC	Ordinary Construction	1.0
NC	Non-Combustible	0.8
FC	Fire-Resistive	0.6

Area Notes for Fire Resistive Buildings (from FUS manual, 1999):

If Vertical Openings are inadequately protected (less than 1-hour fire rating): Area is the total of the two largest adjoining floors (above ground level) plus 50% of the area of each of the next 8 adjoining floors above that.

Contents		% Reduction
NC	Non-Combustible	25
LC	Limited Combustible	15
C	Combustible	0
FB	Free Burning	15
RB	Rapid Burning	25

If Vertical Openings are adequately protected (at least 1-hour fire rating): Area is the total of the largest floor (above ground level) plus 25% of the area of each of the next 2 immediately adjoining floors above that.

1) **Fire Flow**  
 Type of Construction: 

FC
0.6

  
 C = 

0.6
-----

  
 A = 

7,875.00
----------

 m<sup>2</sup>  
 F = 

11,714
--------

 L/min

2) **Occupancy Reduction/Surcharge**  
 Contents Factor: 

LC
-15%

  
 Reduction/Surcharge of 

-15%
------

 = 

-1,757
--------

 L/min  
 F = 11714 L/min + 

-1757
-------

 L/min = 

9,957
-------

 L/min

3) **System Type Reduction**  
 NFPA 13 Sprinkler: 

YES	30%
-----	-----

  
 Standard Water Supply: 

YES	10%
-----	-----

  
 Fully Supervised: 

YES	10%
-----	-----

  
**Total**

50%
-----

  
 Reduction of 

50%
-----

 L/min = 

4,978
-------

 L/min  
 F = 9957 L/min - 

4,978
-------

 L/min = 

4,978
-------

 L/min

4) **Separation Charge**  
 Building Face

Dist(m)	Charge	
North	23	10%
East	18	15%
South	29	10%
West	32	5%
<b>Total</b>	<b>40%</b>	

 of 9956.76 L/min = 

3,983
-------

 L/min  
 (max exposure charge can be 75%)

Separation	Charge	Separation	Charge
0 to 3m	25%	20.1 to 30 m	10%
3.1 to 10m	20%	30.1 to 45m	5%
10.1 to 20m	15%		

F = 4978 L/min + 3983 L/min = 

8,961
-------

 L/min (2,000 L/min < F < 45,000 L/min)

<b>F</b> =	<b>9,000</b>	<b>L/min</b>	(round to the nearest 1,000 L/min)
<b>F</b> =	<b>150</b>	<b>L/s</b>	
<b>F</b> =	<b>2,378</b>	<b>gpm</b>	

# Counterpoint Engineering Inc.

## REQUIRED FIRE FLOW WORKSHEET - PROPOSED DEVELOPMENT

**Project:** 1580-1590 & 1650 Dundas Street East  
**Project No:** 20129  
**Building:** F TH1

Guide for Determination of Required Flow Copyright I.S.O

$$F = 220C\sqrt{A}$$

where  
**F** = the required fire flow in litres per minute.  
**C** = coefficient related to the type of construction.  
 = 1.5 for wood frame construction (structure essentially all combustible).  
 = 1.0 for ordinary construction (brick or other masonry walls, combustible floor and interior).  
 = 0.8 for non-combustible construction (unprotected metal structural components, masonry or metal walls).  
 = 0.6 for fire-resistive construction (fully protected frame, floors, roof).  
**A** = The total floor area in square metres (including all storeys, but excluding basements at least 50 percent below grade) in the building being considered.

Type of Construction	Class Factor	
WF	Wood Frame	1.5
OC	Ordinary Construction	1.0
NC	Non-Combustible	0.8
FC	Fire-Resistive	0.6

Area Notes for Fire Resistive Buildings (from FUS manual, 1999):

If Vertical Openings are inadequately protected (less than 1-hour fire rating): Area is the total of the two largest adjoining floors (above ground level) plus 50% of the area of each of the next 8 adjoining floors above that.

Contents	% Reduction	
NC	Non-Combustible	25
LC	Limited Combustible	15
C	Combustible	0
FB	Free Burning	15
RB	Rapid Burning	25

If Vertical Openings are adequately protected (at least 1-hour fire rating): Area is the total of the largest floor (above ground level) plus 25% of the area of each of the next 2 immediately adjoining floors above that.

1) **Fire Flow**  
 Type of Construction: 

OC
1

  
**C** = 

1
---

  
**A**\* = 

3,000.00
----------

 m<sup>2</sup>  
**F** = 

12,050
--------

 L/min

2) **Occupancy Reduction/Surcharge**  
 Contents Factor: 

LC
-15%

  
 Reduction/Surcharge of **F** = 

12050 L/min
-------------

 + 

-1807
-------

 L/min = 

-1,807
--------

 L/min = 

10,242
--------

 L/min

3) **System Type Reduction**  
 NFPA 13 Sprinkler: 

YES	30%
-----	-----

  
 Standard Water Supply: 

YES	10%
-----	-----

  
 Fully Supervised: 

YES	10%
-----	-----

  
**Total**

50%
-----

  
 Reduction of **F** = 

10242 L/min
-------------

 - 

5,121
-------

 L/min = 

5,121
-------

 L/min = 

5,121
-------

 L/min

4) **Separation Charge**  
 Building Face

Dist(m)	Charge	
North	23	10%
East	34	5%
South	8	20%
West	18	15%
<b>Total</b>	<b>50%</b>	

 of **10242.4** L/min = 

5,121
-------

 L/min  
 (max exposure charge can be 75%)

Separation	Charge	Separation	Charge
0 to 3m	25%	20.1 to 30 m	10%
3.1 to 10m	20%	30.1 to 45m	5%
10.1 to 20m	15%		

**F** = 

5121
------

 L/min + 

5121
------

 L/min = 

10,242
--------

 L/min (2,000L/min < F < 45,000L/min)

<b>F</b> =	<b>10,000</b>	<b>L/min</b>	(round to the nearest 1,000L/min)
<b>F</b> =	<b>167</b>	<b>L/s</b>	
<b>F</b> =	<b>2,642</b>	<b>gpm</b>	

# Counterpoint Engineering Inc.

## REQUIRED FIRE FLOW WORKSHEET - PROPOSED DEVELOPMENT

Project: 1580-1590 & 1650 Dundas Street East  
 Project No: 20129  
 Building: F TH2

Guide for Determination of Required Flow Copyright I.S.O

$$F = 220C\sqrt{A}$$

where  
 F = the required fire flow in litres per minute.  
 C = coefficient related to the type of construction.  
 = 1.5 for wood frame construction (structure essentially all combustible).  
 = 1.0 for ordinary construction (brick or other masonry walls, combustible floor and interior).  
 = 0.8 for non-combustible construction (unprotected metal structural components, masonry or metal walls).  
 = 0.6 for fire-resistive construction (fully protected frame, floors, roof).  
 A = The total floor area in square metres (including all storeys, but excluding basements at least 50 percent below grade) in the building being considered.

Type of Construction		Class Factor
WF	Wood Frame	1.5
OC	Ordinary Construction	1.0
NC	Non-Combustible	0.8
FC	Fire-Resistive	0.6

Area Notes for Fire Resistive Buildings (from FUS manual, 1999):

If Vertical Openings are inadequately protected (less than 1-hour fire rating): Area is the total of the two largest adjoining floors (above ground level) plus 50% of the area of each of the next 8 adjoining floors above that.

Contents		% Reduction
NC	Non-Combustible	25
LC	Limited Combustible	15
C	Combustible	0
FB	Free Burning	15
RB	Rapid Burning	25

If Vertical Openings are adequately protected (at least 1-hour fire rating): Area is the total of the largest floor (above ground level) plus 25% of the area of each of the next 2 immediately adjoining floors above that.

1) **Fire Flow**  
 Type of Construction: 

OC
1

  
 C = 

1
---

  
 A\* = 

1,200.00
----------

 m<sup>2</sup>  
 F = 

7,621
-------

 L/min

2) **Occupancy Reduction/Surcharge**  
 Contents Factor: 

LC
-15%

  
 Reduction/Surcharge of 

-15%
------

 = 

-1,143
--------

 L/min  
 F = 7621 L/min + 

-1,143
--------

 L/min = 

6,478
-------

 L/min

3) **System Type Reduction**  
 NFPA 13 Sprinkler: 

YES	30%
-----	-----

  
 Standard Water Supply: 

YES	10%
-----	-----

  
 Fully Supervised: 

YES	10%
-----	-----

  
 Total 

50%	50%
-----	-----

  
 Reduction of 

50%
-----

 L/min = 

3,239
-------

 L/min  
 F = 6478 L/min - 

3,239
-------

 L/min = 

3,239
-------

 L/min

4) **Separation Charge**  
 Building Face

Dist(m)	Charge	
North	8	20%
East	34	5%
South	24	10%
West	18	15%
Total	50%	

 of 6477.87 L/min = 

3,239
-------

 L/min  
 (max exposure charge can be 75%)

Separation	Charge	Separation	Charge
0 to 3m	25%	20.1 to 30 m	10%
3.1 to 10m	20%	30.1 to 45m	5%
10.1 to 20m	15%		

F = 3239 L/min + 3239 L/min = 

6,478
-------

 L/min (2,000 L/min < F < 45,000 L/min)

F =	6,000	L/min	(round to the nearest 1,000 L/min)
F =	100	L/s	
F =	1,585	gpm	

# Counterpoint Engineering Inc.

## REQUIRED FIRE FLOW WORKSHEET - PROPOSED DEVELOPMENT

Project: 1580-1590 & 1650 Dundas Street East  
 Project No: 20129  
 Building: G

Guide for Determination of Required Flow Copyright I.S.O

$$F = 220C\sqrt{A}$$

where  
 F = the required fire flow in litres per minute.  
 C = coefficient related to the type of construction.  
 = 1.5 for wood frame construction (structure essentially all combustible).  
 = 1.0 for ordinary construction (brick or other masonry walls, combustible floor and interior).  
 = 0.8 for non-combustible construction (unprotected metal structural components, masonry or metal walls).  
 = 0.6 for fire-resistive construction (fully protected frame, floors, roof).  
 A = The total floor area in square metres (including all storeys, but excluding basements at least 50 percent below grade) in the building being considered.

Type of Construction		Class Factor
WF	Wood Frame	1.5
OC	Ordinary Construction	1.0
NC	Non-Combustible	0.8
FC	Fire-Resistive	0.6

Area Notes for Fire Resistive Buildings (from FUS manual, 1999):

If Vertical Openings are inadequately protected (less than 1-hour fire rating): Area is the total of the two largest adjoining floors (above ground level) plus 50% of the area of each of the next 8 adjoining floors above that.

Contents		% Reduction
NC	Non-Combustible	25
LC	Limited Combustible	15
C	Combustible	0
FB	Free Burning	15
RB	Rapid Burning	25

If Vertical Openings are adequately protected (at least 1-hour fire rating): Area is the total of the largest floor (above ground level) plus 25% of the area of each of the next 2 immediately adjoining floors above that.

1) **Fire Flow**  
 Type of Construction: 

FC
0.6

  
 C = 

0.6
-----

  
 A\* = 

9,900.00
----------

 m<sup>2</sup>  
 F = 

13,134
--------

 L/min

2) **Occupancy Reduction/Surcharge**  
 Contents Factor: 

LC
-15%

  
 Reduction/Surcharge of 

-15%
------

 = 

-1,970
--------

 L/min  
 F = 13134 L/min + 

-1970
-------

 L/min = 

11,164
--------

 L/min

3) **System Type Reduction**  
 NFPA 13 Sprinkler: 

YES	30%
-----	-----

  
 Standard Water Supply: 

YES	10%
-----	-----

  
 Fully Supervised: 

YES	10%
-----	-----

  
 Total 

50%
-----

  
 Reduction of 

50%
-----

 L/min = 

5,582
-------

 L/min  
 F = 11164 L/min - 

5,582
-------

 L/min = 

5,582
-------

 L/min

4) **Separation Charge**  
 Building Face

Dist(m)	Charge	
North	17	15%
East	18	15%
South	58	0%
West	32	5%
Total		35%

 of 11163.8 L/min = 

3,907
-------

 L/min  
 (max exposure charge can be 75%)

Separation	Charge	Separation	Charge
0 to 3m	25%	20.1 to 30 m	10%
3.1 to 10m	20%	30.1 to 45m	5%
10.1 to 20m	15%		

F = 5582 L/min + 3907 L/min = 

9,489
-------

 L/min (2,000 L/min < F < 45,000 L/min)

F =	9,000	L/min	(round to the nearest 1,000 L/min)
F =	150	L/s	
F =	2,378	gpm	

# Counterpoint Engineering Inc.

## REQUIRED FIRE FLOW WORKSHEET - PROPOSED DEVELOPMENT

Project: 1580-1590 & 1650 Dundas Street East  
 Project No: 20129  
 Building: G TH1

Guide for Determination of Required Flow Copyright I.S.O

$$F = 220C\sqrt{A}$$

where  
 F = the required fire flow in litres per minute.  
 C = coefficient related to the type of construction.  
 = 1.5 for wood frame construction (structure essentially all combustible).  
 = 1.0 for ordinary construction (brick or other masonry walls, combustible floor and interior).  
 = 0.8 for non-combustible construction (unprotected metal structural components, masonry or metal walls).  
 = 0.6 for fire-resistive construction (fully protected frame, floors, roof).  
 A = The total floor area in square metres (including all storeys, but excluding basements at least 50 percent below grade) in the building being considered.

Type of Construction		Class Factor
WF	Wood Frame	1.5
OC	Ordinary Construction	1.0
NC	Non-Combustible	0.8
FC	Fire-Resistive	0.6

Area Notes for Fire Resistive Buildings (from FUS manual, 1999):

If Vertical Openings are inadequately protected (less than 1-hour fire rating): Area is the total of the two largest adjoining floors (above ground level) plus 50% of the area of each of the next 8 adjoining floors above that.

Contents		% Reduction
NC	Non-Combustible	25
LC	Limited Combustible	15
C	Combustible	0
FB	Free Burning	15
RB	Rapid Burning	25

If Vertical Openings are adequately protected (at least 1-hour fire rating): Area is the total of the largest floor (above ground level) plus 25% of the area of each of the next 2 immediately adjoining floors above that.

1) **Fire Flow**  
 Type of Construction: 

OC
1

  
 C = 

1
---

  
 A\* = 

1,680.00
----------

 m<sup>2</sup>  
 F = 

9,017
-------

 L/min

2) **Occupancy Reduction/Surcharge**  
 Contents Factor: 

LC
-15%

  
 Reduction/Surcharge of = 

-1,353
--------

 L/min  
 F = 9017 L/min + 

-1353
-------

 L/min = 

7,665
-------

 L/min

3) **System Type Reduction**  
 NFPA 13 Sprinkler: 

YES	30%
-----	-----

  
 Standard Water Supply: 

YES	10%
-----	-----

  
 Fully Supervised: 

YES	10%
-----	-----

  
 Total 

50%
-----

  
 Reduction of 

50%
-----

 L/min = 

3,832
-------

 L/min  
 F = 7665 L/min - 

3,832
-------

 L/min = 

3,832
-------

 L/min

4) **Separation Charge**  
 Building Face

Dist(m)	Charge	
North	24	10%
East	35	5%
South	17	15%
West	18	15%
Total	45%	

 of 7664.72 L/min = 

3,449
-------

 L/min  
 (max exposure charge can be 75%)

Separation	Charge	Separation	Charge
0 to 3m	25%	20.1 to 30 m	10%
3.1 to 10m	20%	30.1 to 45m	5%
10.1 to 20m	15%		

F = 3832 L/min + 3449 L/min = 

7,281
-------

 L/min (2,000 L/min < F < 45,000 L/min)

F =	7,000	L/min	(round to the nearest 1,000 L/min)
F =	117	L/s	
F =	1,849	gpm	

# Counterpoint Engineering Inc.

## NFPA Theoretical Flow Calculations

**Project:** 1580-1590 & 1650 Dundas Street East  
**Project No:** 20129  
**Hydrant:** Fire hydrants connected into 300mm diameter Mattawa Avenue watermain.

Based on National Fire Protection Association Guidelines, the available flow at the minimum residual pressure of 20psi can be calculated based on the observed flow at the observed pressure readings, as follows:

$$Q_F = 29.83 \times c \times d^2 \times p^{0.5}, \text{ where}$$

$Q_F$  = observed flow (US GPM)  
 $c$  = hydrant nozzle coefficient (0.90 - 0.95)  
 $d$  = nozzle diameter (in)  
 $p$  = observed pitot pressure

$$Q_R = Q_F \times h_F^{0.54} / h_R^{0.54}, \text{ where}$$

$Q_R$  = available flow  
 $Q_F$  = observed flow (US GPM)  
 $h_F$  = drop from measured static to desired baseline pressure  
 $h_R$  = drop from measured static to measured residual pressure

Based on flow test results obtained by *Lozzi Aqua Check, July 23, 2021.*

$c =$  0.9  
 $d =$  2.5 in  
number of ports = 2  
 $p =$  56

$$Q_F = 2511 \text{ US GPM}$$

Measured Static Pressure = 80 psi  
Measured Residual Pressure = 71 psi  
Desired Residual Pressure = 20 psi, minimum.

$$Q_R = \boxed{\begin{array}{l} 6995 \text{ US GPM} \\ 26,480 \text{ L/min} \\ 441.34 \text{ L/s} \end{array}} \text{ per fire connection}$$



Lozzi Aqua Check

Massimo Lozzi

12307 Woodbine Ave, P.O. Box 519

Cell: 416 990-2131

Gormley, ON L0H 1G0

E-mail: lozziaquacheck@gmail.com

### Hydrant Flow Test Form

Job Location: Mattawa Ave and Dundas St. E, Mississauga

Date: July 23, 2021

Time of Test: 3:00 pm

Location of Flow Hydrant: First hydrant SE of residual hydrant

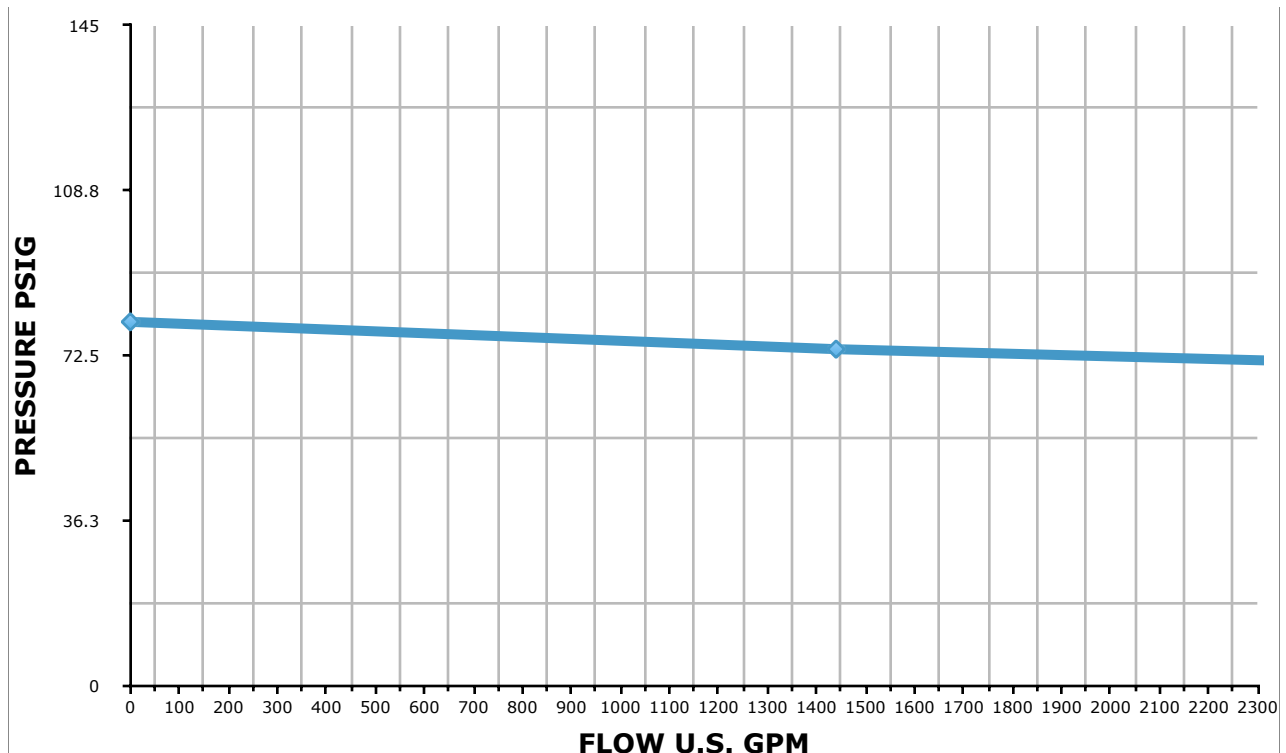
Residual : 1590 Dundas St. E hydrant on Mattawa Ave.

Main Size: 300 mm

Static Pressure: 80 psi

	Number of Outlets & Orifice Size	Pitot Pressure (psi)	Flow (U.S. G.P.M.)	Residual Pressure (psi)
1.	Static	0	0	80
2.	1 x 2 ½	74	1440	74
3.	2 x 2 ½	56	2505	71

Note: Flow test conducted in accordance with NFPA 291



Lozzi Aqua Check

Massimo Lozzi

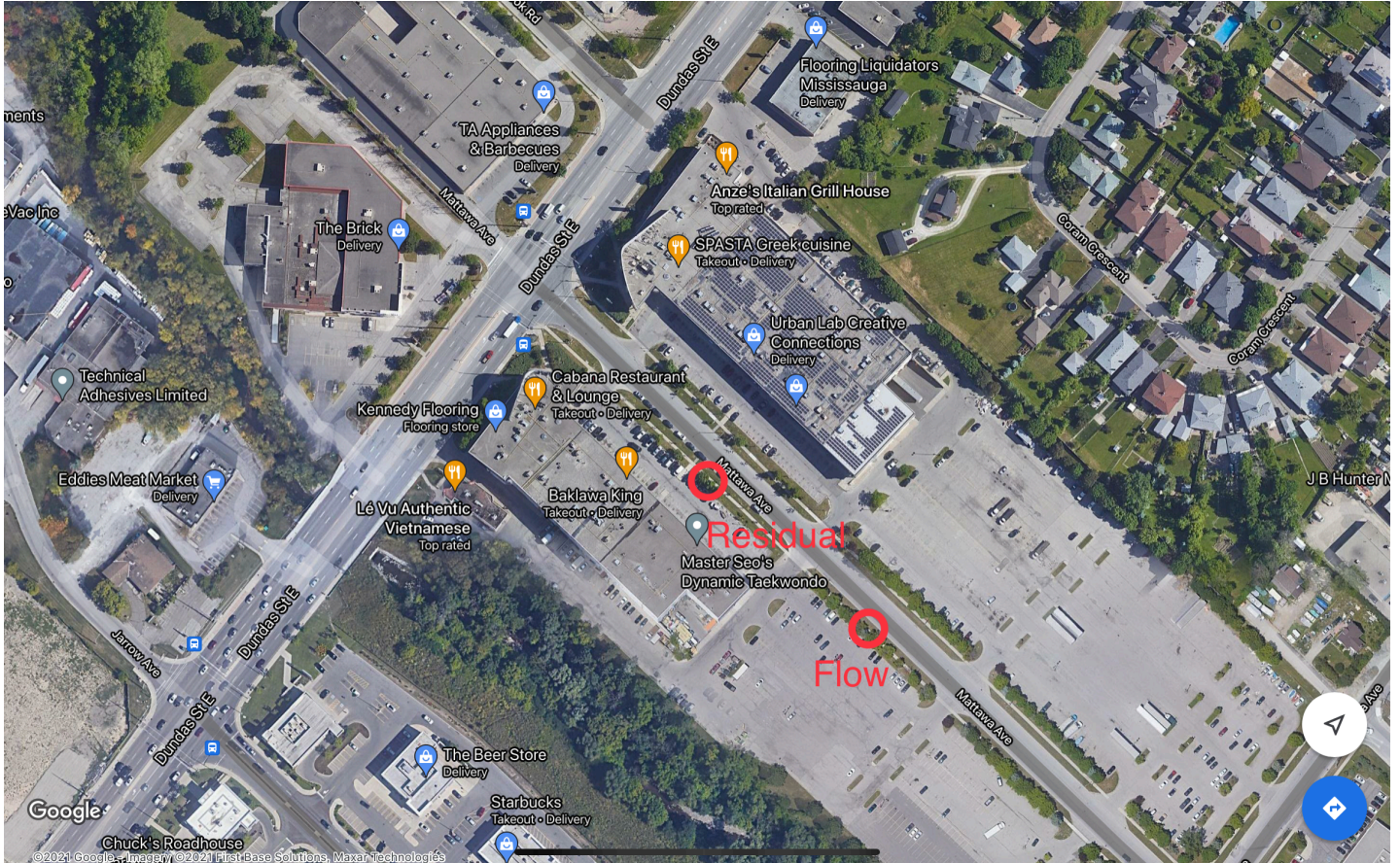
12307 Woodbine Ave, P.O. Box 519

Cell: 416 990-2131

Gormley, ON L0H 1G0

E-mail: lozziaquacheck@gmail.com

Site Map:





## **APPENDIX 'C'**

### **Sanitary Calculations and Multi-Use Demand Sheets**

**Counterpoint Engineering Inc.**  
**Sanitary Flow Generation**

**Project:** 1580-1590 & 1650 Dundas Street East  
**Project No:** 20129  
**Location:** Mississauga  
**Date:** Nov-21

**Site Sanitary Flow Summary**

Locations		Domestic Flows			Infiltration Flows		Totals
Area	Ctrl. MH Connections	Total Units	Total Population	Domestic Flows (L/s)	Site Area (ha)	Infiltration Flows (L/s)	Total Flow (L/s)
Block A	1A, 3A, 5A	1099	2269	<b>28.17</b>	1.05	1.05	<b>29.22</b>
Block C	15A	448	940	<b>12.58</b>	0.63	0.41	<b>12.98</b>
Block E	8A, 10A, 12A	533	1136	<b>14.98</b>	1.28	1.10	<b>16.08</b>
Block F	14A, 18A, 19A, 16A	407	910	<b>12.20</b>	1.23	1.37	<b>13.57</b>
Block G	20A, 21A, 22A	540	1186	<b>15.59</b>	1.13	1.07	<b>16.66</b>
<b>TOTALS:</b>		3027	6441	<b>83.53</b>	5.31	4.98	<b>88.51</b>

# Counterpoint Engineering Inc.

## Sanitary Flow Generation

Project: 1580-1590 & 1650 Dundas Street East  
 Project No: 20129  
 Location: Block A  
 Date: Nov-21

### BUILDING 1

Region of Peel Guidelines		
Large Apartments (+750 sq.ft.)	3.0	ppu
Small Apartments (<750 sq.ft.)	1.6	ppu
Average Flow	302.8	L/cap/day
Infiltration	0.20	L/s/ha
Infiltration (Manholes)	0.28	L/s/mh
Commercial	50	p/ha

Site Area 1.05 ha  
 Number of Manholes 3 each  
 Number of Large Units 362 units  
 Number of Small Units 737 units  
 Commercial Area 0.075900 ha

### Population Generation

	(units) Commercial (area - ha)	Population (Persons)
Residential	1,099	2265
Commercial	0.08	4
<b>Total Population:</b>		<b>2269</b>

### Flow Generation

	Domestic Flows		Site Area (ha)	Infiltration Flows		Total Flows
	Peaking Factor	Domestic Flows (L/s)		Number of Manholes	Infiltration Flows (L/s)	Total Flow (L/s)
Population (persons)						
2269	3.54	28.17	1.05	3	1.05	29.2

# Counterpoint Engineering Inc.

## Sanitary Flow Generation

Project: 1580-1590 & 1650 Dundas Street East  
 Project No: 20129  
 Location: Block C  
 Date: Nov-21

### BUILDING 1

Region of Peel Guidelines		
Large Apartments (+750 sq.ft.)	3.0	ppu
Small Apartments (<750 sq.ft.)	1.6	ppu
Average Flow	302.8	L/cap/day
Infiltration	0.20	L/s/ha
Infiltration (Manholes)	0.28	L/s/mh
Commercial	50	p/ha

Site Area	<span style="border: 1px solid black; padding: 2px;">0.63</span>	ha
Number of Manholes	<span style="border: 1px solid black; padding: 2px;">1</span>	each
Number of Large Units	<span style="border: 1px solid black; padding: 2px;">155</span>	units
Number of Small Units	<span style="border: 1px solid black; padding: 2px;">293</span>	units
Commercial Area	<span style="border: 1px solid black; padding: 2px;">0.129000</span>	ha

### Population Generation

	(units) Commercial (area - ha)	Population (Persons)
Residential	448	934
Commercial	0.13	6
<b>Total Population:</b>		<b>940</b>

### Flow Generation

	Domestic Flows		Site Area (ha)	Infiltration Flows		Total Flows
	Peaking Factor	Domestic Flows (L/s)		Number of Manholes	Infiltration Flows (L/s)	Total Flow (L/s)
Population (persons)						
940	3.82	12.58	0.63	1	0.41	13.0

# Counterpoint Engineering Inc.

## Sanitary Flow Generation

Project: 1580-1590 & 1650 Dundas Street East  
 Project No: 20129  
 Location: Block E  
 Date: Nov-21

### BUILDING 1

Region of Peel Guidelines		
Large Apartments (+750 sq.ft.)	3.0	ppu
Small Apartments (<750 sq.ft.)	1.6	ppu
Average Flow	302.8	L/cap/day
Infiltration	0.20	L/s/ha
Infiltration (Manholes)	0.28	L/s/mh
Commercial	50	p/ha

Site Area: 1.28 ha  
 Number of Manholes: 3 each  
 Number of Large Units: 199 units  
 Number of Small Units: 334 units  
 Commercial Area: 0.090600 ha

### Population Generation

	(units) Commercial (area - ha)	Population (Persons)
Residential	533	1131
Commercial	0.09	5
<b>Total Population:</b>		<b>1136</b>

### Flow Generation

Population (persons)	Domestic Flows		Site Area (ha)	Infiltration Flows		Total Flows
	Peaking Factor	Domestic Flows (L/s)		Number of Manholes	Infiltration Flows (L/s)	Total Flow (L/s)
1136	3.76	14.98	1.28	3	1.10	16.1

# Counterpoint Engineering Inc.

## Sanitary Flow Generation

Project: 1580-1590 & 1650 Dundas Street East  
 Project No: 20129  
 Location: Block F  
 Date: Nov-21

### BUILDING 1

Region of Peel Guidelines		
Large Apartments (+750 sq.ft.)	3.0	ppu
Small Apartments (<750 sq.ft.)	1.6	ppu
Average Flow	302.8	L/cap/day
Infiltration	0.20	L/s/ha
Infiltration (Manholes)	0.28	L/s/mh
Commercial	50	p/ha

Site Area 1.23 ha  
 Number of Manholes 4 each  
 Number of Large Units 185 units  
 Number of Small Units 222 units  
 Commercial Area 0.000000 ha

### Population Generation

	(units) Commercial (area - ha)	Population (Persons)
Residential	407	910
Commercial	0.00	0
<b>Total Population:</b>		<b>910</b>

### Flow Generation

Population (persons)	Domestic Flows		Site Area (ha)	Infiltration Flows		Total Flows
	Peaking Factor	Domestic Flows (L/s)		Number of Manholes	Infiltration Flows (L/s)	Total Flow (L/s)
910	3.83	12.20	1.23	4	1.37	13.6



# Counterpoint Engineering Inc.

## Sanitary Flow Generation

Project: 1580-1590 & 1650 Dundas Street East  
 Project No: 20129  
 Location: Block G  
 Date: Nov-21

### BUILDING 1

Region of Peel Guidelines		
Large Apartments (+750 sq.ft.)	3.0	ppu
Small Apartments (<750 sq.ft.)	1.6	ppu
Average Flow	302.8	L/cap/day
Infiltration	0.20	L/s/ha
Infiltration (Manholes)	0.28	L/s/mh
Commercial	50	p/ha

Site Area 1.13 ha  
 Number of Manholes 3 each  
 Number of Large Units 230 units  
 Number of Small Units 310 units  
 Commercial Area 0.000000 ha

### Population Generation

	(units) Commercial (area - ha)	Population (Persons)
Residential	540	1186
Commercial	0.00	0
<b>Total Population:</b>		<b>1186</b>

### Flow Generation

Population (persons)	Domestic Flows		Site Area (ha)	Infiltration Flows		Total Flows
	Peaking Factor	Domestic Flows (L/s)		Number of Manholes	Infiltration Flows (L/s)	Total Flow (L/s)
1186	3.75	15.59	1.13	3	1.07	16.7

# Counterpoint Engineering Inc.

## Sanitary Flow Generation

Project: 1580-1590 & 1650 Dundas Street East  
 Project No: 20129  
 Location: Existing Site  
 Date: Nov-21

### BUILDING 1

Region of Peel Guidelines		
Large Apartments (+750 sq.ft.)	3.0	ppu
Small Apartments (<750 sq.ft.)	1.6	ppu
Average Flow	302.8	L/cap/day
Infiltration	0.20	L/s/ha
Infiltration (Manholes)	0.28	L/s/mh
Commercial	50	p/ha

Site Area 7.39 ha  
 Number of Manholes 1 each  
 Number of Large Units units  
 Number of Small Units units  
 Commercial Area 1.550000 ha

### Population Generation

	(units) Commercial (area - ha)	Population (Persons)
Residential	0	0
Commercial	1.55	78
<b>Total Population:</b>		<b>78</b>

### Flow Generation

	Domestic Flows		Site Area (ha)	Infiltration Flows		Total Flows
	Peaking Factor	Domestic Flows (L/s)		Number of Manholes	Infiltration Flows (L/s)	Total Flow (L/s)
Population (persons)						
78	4.27	1.16	7.39	1	1.76	2.92

## Connection Multi Use Demand Table - Block A

### WATER CONNECTION

<b>Connection point</b> <sup>3)</sup>			
300mm watermain in Mattawa Avenue, south of Dundas Street East.			
<b>Pressure zone of connection point</b>		Unknown	
<b>Total equivalent population to be serviced</b> <sup>1)</sup>		2269 persons.	
<b>Total lands to be serviced</b>		1.05 ha.	
<b>Hydrant flow test</b>		300mm watermain in Mattawa Avenue, south of Dundas Street East.	
Hydrant flow test location			
	Pressure (kPa)	Flow (in l/s)	Time
Minimum water pressure	140 kPa	441.34 l/s (flow at 20 psi).	
Maximum water pressure	552 kPa	0 l/s (static pressure).	

No.	Demand type	Water demands		
		Demand (in l/s)		
		Use 1 <sup>5)</sup>	Use 2 <sup>5)</sup>	Total
1	Average day flow	7.37 l/s		7.37 l/s
2	Maximum day flow	14.72 l/s		14.72 l/s
3	Peak hour flow	22.10 l/s		22.10 l/s
4	Fire flow <sup>2)</sup>	166.67 l/s		166.67 l/s
<b>Analysis</b>				
5	Maximum day plus fire flow	181.38 l/s		181.38 l/s

Note: very minor retail use included in the residential demands.

### WASTEWATER CONNECTION

250mm diameter sanitary sewer in Mattawa Avenue.

			Total
<b>Connection point</b> <sup>4)</sup>			
<b>Total equivalent population to be serviced</b> <sup>1)</sup>			2269 persons
<b>Total lands to be serviced</b>			1.05 ha.
6	Wastewater sewer effluent (in l/s)	29.22 l/s	29.22 l/s

- <sup>1)</sup> The calculations should be based on the development estimated population (employment and/or residential).
- <sup>2)</sup> Please reference the Fire Underwriters Survey Document
- <sup>3)</sup> Please specify the connection point ID
- <sup>4)</sup> Please specify the connection point (wastewater line or manhole ID)  
Also, the "total equivalent population to be serviced" and the "total lands to be serviced" should reference the connection point. (The FSR should contain one copy of Site Servicing Plan)
- <sup>5)</sup> Please complete as many uses are necessary for the development.  
(Please specify the use)

Please include the graphs associated with the hydrant flow test information table  
Please provide Professional Engineer's signature and stamp on the demand table  
All required calculations must be submitted with the demand table submission.



## Connection Multi Use Demand Table - Block C

### WATER CONNECTION

<b>Connection point</b> <sup>3)</sup>			
300mm watermain in Mattawa Avenue, south of Dundas Street East.			
<b>Pressure zone of connection point</b>		Unknown	
<b>Total equivalent population to be serviced</b> <sup>1)</sup>		940 persons.	
<b>Total lands to be serviced</b>		0.63 ha.	
<b>Hydrant flow test</b>		300mm watermain in Mattawa Avenue, south of Dundas Street East.	
Hydrant flow test location			
	Pressure (kPa)	Flow (in l/s)	Time
Minimum water pressure	140 kPa	441.34 l/s (flow at 20 psi).	
Maximum water pressure	552 kPa	0 l/s (static pressure).	

No.	Demand type	Water demands		
		Demand (in l/s)		
		Use 1 <sup>5)</sup>	Use 2 <sup>5)</sup>	Total
1	Average day flow	3.28 l/s		3.28 l/s
2	Maximum day flow	6.53 l/s		6.53 l/s
3	Peak hour flow	9.83 l/s		9.83 l/s
4	Fire flow <sup>2)</sup>	116.67 l/s		116.67 l/s
<b>Analysis</b>				
5	Maximum day plus fire flow	123.20 l/s		123.20 l/s

Note: very minor retail use included in the residential demands.

### WASTEWATER CONNECTION

250mm diameter sanitary sewer in Mattawa Avenue.

			Total
<b>Connection point</b> <sup>4)</sup>			
<b>Total equivalent population to be serviced</b> <sup>1)</sup>			940 persons
<b>Total lands to be serviced</b>			0.63 ha
6	Wastewater sewer effluent (in l/s)	12.98 l/s	12.98 l/s

<sup>1)</sup> The calculations should be based on the development estimated population (employment and/or residential).

<sup>2)</sup> Please reference the Fire Underwriters Survey Document

<sup>3)</sup> Please specify the connection point ID

<sup>4)</sup> Please specify the connection point (wastewater line or manhole ID)  
Also, the "total equivalent population to be serviced" and the "total lands to be serviced" should reference the connection point. (The FSR should contain one copy of Site Servicing Plan)

<sup>5)</sup> Please complete as many uses are necessary for the development.  
(Please specify the use)

Please include the graphs associated with the hydrant flow test information table  
Please provide Professional Engineer's signature and stamp on the demand table  
All required calculations must be submitted with the demand table submission.



## Connection Multi Use Demand Table - Block E

### WATER CONNECTION

<b>Connection point</b> <sup>3)</sup>			
300mm watermain in Mattawa Avenue, south of Dundas Street East.			
<b>Pressure zone of connection point</b>		Unknown	
<b>Total equivalent population to be serviced</b> <sup>1)</sup>		1136 persons.	
<b>Total lands to be serviced</b>		1.28 ha.	
<b>Hydrant flow test</b>		300mm watermain in Mattawa Avenue, south of Dundas Street East.	
Hydrant flow test location			
	Pressure (kPa)	Flow (in l/s)	Time
Minimum water pressure	140 kPa	441.34 l/s (flow at 20 psi).	
Maximum water pressure	552 kPa	0 l/s (static pressure).	

No.	Demand type	Water demands		
		Demand (in l/s)		
		Use 1 <sup>5)</sup>	Use 2 <sup>5)</sup>	Total
1	Average day flow	3.96 l/s		3.96 l/s
2	Maximum day flow	7.90 l/s		7.90 l/s
3	Peak hour flow	11.87 l/s		11.87 l/s
4	Fire flow <sup>2)</sup>	183.33 l/s		183.33 l/s
<b>Analysis</b>				
5	Maximum day plus fire flow	191.23 l/s		191.23 l/s

Note: very minor retail use included in the residential demands.

### WASTEWATER CONNECTION

250mm diameter sanitary sewer in Mattawa Avenue.

			Total
<b>Connection point</b> <sup>4)</sup>			
<b>Total equivalent population to be serviced</b> <sup>1)</sup>			1136 persons
<b>Total lands to be serviced</b>			1.28 ha
6	Wastewater sewer effluent (in l/s)	16.08 l/s	16.08 l/s

<sup>1)</sup> The calculations should be based on the development estimated population (employment and/or residential).

<sup>2)</sup> Please reference the Fire Underwriters Survey Document

<sup>3)</sup> Please specify the connection point ID

<sup>4)</sup> Please specify the connection point (wastewater line or manhole ID)  
Also, the "total equivalent population to be serviced" and the "total lands to be serviced" should reference the connection point. (The FSR should contain one copy of Site Servicing Plan)

<sup>5)</sup> Please complete as many uses are necessary for the development.  
(Please specify the use)

Please include the graphs associated with the hydrant flow test information table  
Please provide Professional Engineer's signature and stamp on the demand table  
All required calculations must be submitted with the demand table submission.



## Connection Multi Use Demand Table - Block F

### WATER CONNECTION

<b>Connection point</b> <sup>3)</sup>			
300mm watermain in Mattawa Avenue, south of Dundas Street East.			
<b>Pressure zone of connection point</b>		Unknown	
<b>Total equivalent population to be serviced</b> <sup>1)</sup>		910 persons.	
<b>Total lands to be serviced</b>		1.23 ha	
<b>Hydrant flow test</b>		300mm watermain in Mattawa Avenue, south of Dundas Street East.	
Hydrant flow test location			
	Pressure (kPa)	Flow (in l/s)	Time
Minimum water pressure	140 kPa	441.34 l/s (flow at 20 psi).	
Maximum water pressure	552 kPa	0 l/s (static pressure).	

No.	Demand type	Water demands		
		Demand (in l/s)		
		Use 1 <sup>5)</sup>	Use 2 <sup>5)</sup>	Total
1	Average day flow	1.23 l/s		1.23 l/s
2	Maximum day flow	2.47 l/s		2.47 l/s
3	Peak hour flow	3.70 l/s		3.70 l/s
4	Fire flow <sup>2)</sup>	166.67 l/s		166.67 l/s
<b>Analysis</b>				
5	Maximum day plus fire flow	169.13 l/s		169.13 l/s

Note: very minor retail use included in the residential demands.

### WASTEWATER CONNECTION

250mm diameter sanitary sewer in Mattawa Avenue.

			Total
<b>Connection point</b> <sup>4)</sup>			
<b>Total equivalent population to be serviced</b> <sup>1)</sup>			910 persons
<b>Total lands to be serviced</b>			1.23 ha
6	Wastewater sewer effluent (in l/s)	13.57 l/s	13.57 l/s

<sup>1)</sup> The calculations should be based on the development estimated population (employment and/or residential).

<sup>2)</sup> Please reference the Fire Underwriters Survey Document

<sup>3)</sup> Please specify the connection point ID

<sup>4)</sup> Please specify the connection point (wastewater line or manhole ID)  
Also, the "total equivalent population to be serviced" and the "total lands to be serviced" should reference the connection point. (The FSR should contain one copy of Site Servicing Plan)

<sup>5)</sup> Please complete as many uses are necessary for the development.  
(Please specify the use)

Please include the graphs associated with the hydrant flow test information table  
Please provide Professional Engineer's signature and stamp on the demand table  
All required calculations must be submitted with the demand table submission.



## Connection Multi Use Demand Table - Block G

### WATER CONNECTION

<b>Connection point</b> <sup>3)</sup>			
300mm watermain in Mattawa Avenue, south of Dundas Street East.			
<b>Pressure zone of connection point</b>		Unknown	
<b>Total equivalent population to be serviced</b> <sup>1)</sup>		1186 persons.	
<b>Total lands to be serviced</b>		1.13 ha.	
<b>Hydrant flow test</b>		300mm watermain in Mattawa Avenue, south of Dundas Street East.	
Hydrant flow test location			
	Pressure (kPa)	Flow (in l/s)	Time
Minimum water pressure	140 kPa	441.34 l/s (flow at 20 psi).	
Maximum water pressure	552 kPa	0 l/s (static pressure).	

No.	Demand type	Water demands		
		Demand (in l/s)		
		Use 1 <sup>5)</sup>	Use 2 <sup>5)</sup>	Total
1	Average day flow	4.12 l/s		4.12 l/s
2	Maximum day flow	8.24 l/s		8.24 l/s
3	Peak hour flow	12.35 l/s		12.35 l/s
4	Fire flow <sup>2)</sup>	150.00 l/s		150.00 l/s
<b>Analysis</b>				
5	Maximum day plus fire flow	158.24 l/s		158.24 l/s

Note: very minor retail use included in the residential demands.

### WASTEWATER CONNECTION

250mm diameter sanitary sewer in Mattawa Avenue.

			Total
<b>Connection point</b> <sup>4)</sup>			
<b>Total equivalent population to be serviced</b> <sup>1)</sup>			1186 persons
<b>Total lands to be serviced</b>			1.13 ha
6	Wastewater sewer effluent (in l/s)	16.66 l/s	16.66 l/s

<sup>1)</sup> The calculations should be based on the development estimated population (employment and/or residential).

<sup>2)</sup> Please reference the Fire Underwriters Survey Document

<sup>3)</sup> Please specify the connection point ID

<sup>4)</sup> Please specify the connection point (wastewater line or manhole ID)  
Also, the "total equivalent population to be serviced" and the "total lands to be serviced" should reference the connection point. (The FSR should contain one copy of Site Servicing Plan)

<sup>5)</sup> Please complete as many uses are necessary for the development.  
(Please specify the use)

Please include the graphs associated with the hydrant flow test information table  
Please provide Professional Engineer's signature and stamp on the demand table  
All required calculations must be submitted with the demand table submission.





## **APPENDIX 'D'**

### **Stormwater Management Calculations**



**SWM DESIGN CALCULATIONS**  
**Allowable Unitary Release Rate Calculations - Little Etobicoke Creek**

**Project Name:** 1580-1590 & 1650 Dundas Street East  
**Municipality:** Mississauga, ON  
**Project No.:** 20129  
**Date:** 27-Oct-21

**Prepared by:** J.L.  
**Checked by:**  
**Last Revised:** 27-Oct-21

**Total Site Area (ha):** 6.580 ha (limits of post-development drainage areas)

**Etobicoke Creek Quantity Control Unit Release Rates (L/s/ha):**

2-year	5-year	10-year	25-year	50-year	100-year
21.5	33	41	55	62.7	71.8

Block E (201 + 200 + 201A + U200 + U201):	1.299	ha
Block A (202 + U202 + 202A):	1.045	ha
Block C (207 + 207A):	0.627	ha
Block F (204 + 205 + 206 + 208 + 206A):	0.950	ha
Block G (203 + 211 + 212 + 213 + 210 + 213A):	1.435	ha
Area R201:	0.189	ha
Park Block (214):	1.035	ha

(Uncontrolled - to be overcontrolled within Blocks A to G)

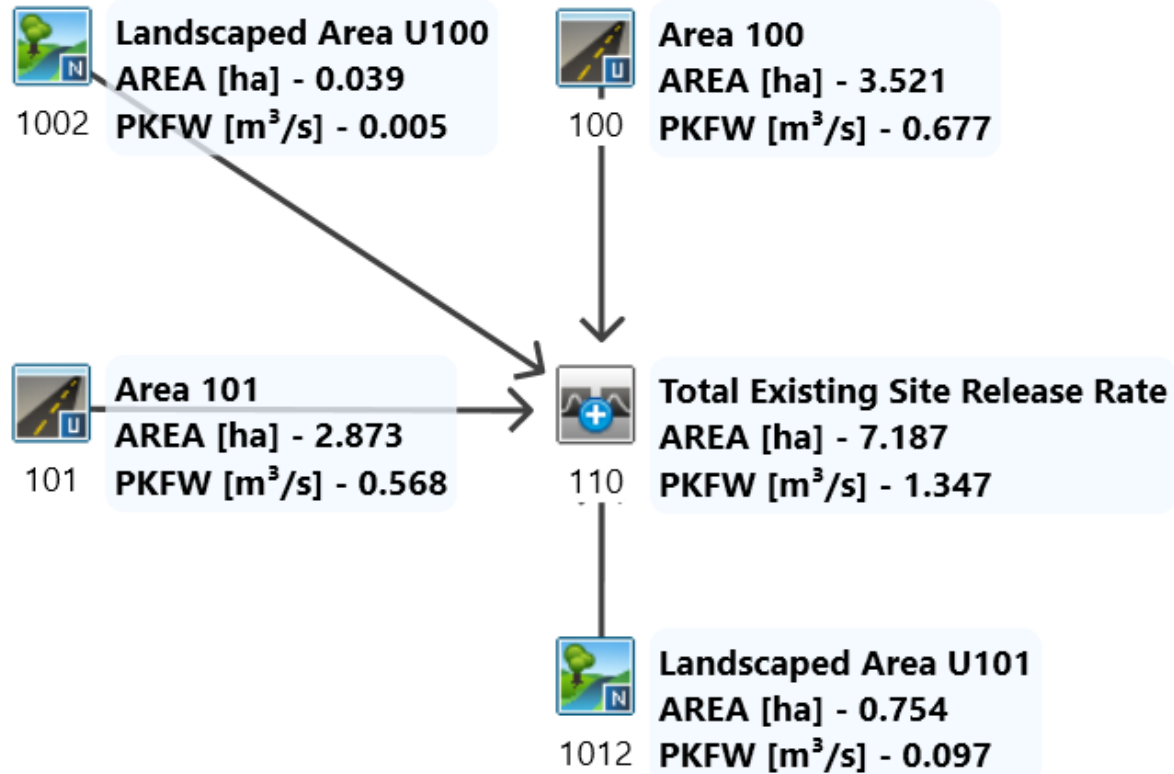
**Site Area and Block Allowable Release Rates (L/s):**

	2-year	5-year	10-year	25-year	50-year	100-year
<b>Total Site Allowable Release Rates:</b>	<b>141.5</b>	<b>217.1</b>	<b>269.8</b>	<b>361.9</b>	<b>412.6</b>	<b>472.4</b>
Block E:	21.7	32.5	40.2	55.5	62.7	71.9
Block A:	17.5	26.2	32.3	44.7	50.4	57.8
Block C:	10.5	15.7	19.4	26.8	30.3	34.7
Block F:	15.9	23.8	29.4	40.6	45.9	52.6
Block G:	24.0	35.9	44.4	61.3	69.3	79.4
Area R201:	17	23	27	32	35	39
Park Block:	35	60	77	101	119	137

\*Block release rates adjusted to overcontrol for park block and Area R201 flows to ensure entire site achieves total allowable release rate.



## Pre-Development VO6 Model Schematic





```

=====
=====
V   V   I   SSSSS U   U   A   L           (v 6.0.2001)
V   V   I   SS    U   U   A A  L
V   V   I   SS    U   U   AAAAA L
V   V   I   SS    U   U   A   A  L
  VV    I   SSSSS UUUUU A   A  LLLLL

```

```

000  TTTTT  TTTTT  H   H  Y   Y  M   M  000  TM
0   0   T    T    H   H  Y   Y  MM  MM  0   0
0   0   T    T    H   H  Y   M   M  0   0
000   T    T    H   H  Y   M   M  000

```

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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

Input filename: C:\Program Files (x86)\Visual OTTHYMO 6.0\V02\voin.dat

Output filename:

C:\Users\jliang\AppData\Local\Civica\XH5\becad37f-97fe-4a15-a3fd-f87dd2156d5f\1add8  
 6de-7f1f-4784-a8e6-7e9588c5f3d3\scena

Summary filename:

C:\Users\jliang\AppData\Local\Civica\XH5\becad37f-97fe-4a15-a3fd-f87dd2156d5f\1add8  
 6de-7f1f-4784-a8e6-7e9588c5f3d3\scena

DATE: 10-18-2021

TIME: 02:27:40

USER:

COMMENTS: \_\_\_\_\_

```

-----
-----
*****
** SIMULATION : Run 01           **
*****

```

-----  
 | READ STORM |

Filename: C:\Users\jliang\AppData  
 ata\Local\Temp\



Ptotal= 36.00 mm

f9a46910-ba32-4004-be5f-e15416527993\05bf40b2

Comments: 2-Year 6-hour AES Storm

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.25	0.72	1.75	12.24	3.25	5.04	4.75	0.72
0.50	0.72	2.00	12.24	3.50	5.04	5.00	0.72
0.75	0.72	2.25	33.12	3.75	2.88	5.25	0.72
1.00	0.72	2.50	33.12	4.00	2.88	5.50	0.72
1.25	4.32	2.75	9.36	4.25	1.44	5.75	0.72
1.50	4.32	3.00	9.36	4.50	1.44	6.00	0.72

CALIB

NASHYD ( 1012)

ID= 1 DT= 5.0 min

Area (ha)= 0.75 Curve Number (CN)= 85.0

Ia (mm)= 5.00 # of Linear Res.(N)= 3.00

U.H. Tp(hrs)= 0.20

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	0.72	1.583	12.24	3.083	5.04	4.58	0.72
0.167	0.72	1.667	12.24	3.167	5.04	4.67	0.72
0.250	0.72	1.750	12.24	3.250	5.04	4.75	0.72
0.333	0.72	1.833	12.24	3.333	5.04	4.83	0.72
0.417	0.72	1.917	12.24	3.417	5.04	4.92	0.72
0.500	0.72	2.000	12.24	3.500	5.04	5.00	0.72
0.583	0.72	2.083	33.12	3.583	2.88	5.08	0.72
0.667	0.72	2.167	33.12	3.667	2.88	5.17	0.72
0.750	0.72	2.250	33.12	3.750	2.88	5.25	0.72
0.833	0.72	2.333	33.12	3.833	2.88	5.33	0.72
0.917	0.72	2.417	33.12	3.917	2.88	5.42	0.72
1.000	0.72	2.500	33.12	4.000	2.88	5.50	0.72
1.083	4.32	2.583	9.36	4.083	1.44	5.58	0.72
1.167	4.32	2.667	9.36	4.167	1.44	5.67	0.72
1.250	4.32	2.750	9.36	4.250	1.44	5.75	0.72
1.333	4.32	2.833	9.36	4.333	1.44	5.83	0.72
1.417	4.32	2.917	9.36	4.417	1.44	5.92	0.72
1.500	4.32	3.000	9.36	4.500	1.44	6.00	0.72

Unit Hyd Qpeak (cms)= 0.144

PEAK FLOW (cms)= 0.025 (i)

TIME TO PEAK (hrs)= 2.583

RUNOFF VOLUME (mm)= 12.649



TOTAL RAINFALL (mm)= 36.000  
 RUNOFF COEFFICIENT = 0.351

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 -----  
 | CALIB |  
 | NASHYD ( 1002) | Area (ha)= 0.04 Curve Number (CN)= 85.0  
 | ID= 1 DT= 5.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
 -----  
 U.H. Tp(hrs)= 0.20

Unit Hyd Qpeak (cms)= 0.007

PEAK FLOW (cms)= 0.001 (i)  
 TIME TO PEAK (hrs)= 2.583  
 RUNOFF VOLUME (mm)= 12.630  
 TOTAL RAINFALL (mm)= 36.000  
 RUNOFF COEFFICIENT = 0.351

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 -----  
 | CALIB |  
 | STANDHYD ( 0101) | Area (ha)= 2.87  
 | ID= 1 DT= 5.0 min | Total Imp(%)= 88.00 Dir. Conn.(%)= 88.00  
 -----

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	2.53	0.34	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	138.40	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	33.12	16.12	
over (min)	5.00	10.00	
Storage Coeff. (min)=	4.83 (ii)	9.78 (ii)	
Unit Hyd. Tpeak (min)=	5.00	10.00	
Unit Hyd. peak (cms)=	0.22	0.11	
			*TOTALS*
PEAK FLOW (cms)=	0.23	0.01	0.245 (iii)
TIME TO PEAK (hrs)=	2.50	2.50	2.50
RUNOFF VOLUME (mm)=	35.00	12.67	32.32
TOTAL RAINFALL (mm)=	36.00	36.00	36.00
RUNOFF COEFFICIENT =	0.97	0.35	0.90

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL



THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB |
| STANDHYD ( 0100) |
| ID= 1 DT= 5.0 min |
-----
  
```

Area (ha)=	3.52		
Total Imp(%)=	80.00	Dir. Conn.(%)=	80.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	2.82	0.70	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	153.21	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	33.12	15.30	
over (min)	5.00	25.00	
Storage Coeff. (min)=	5.13 (ii)	20.09 (ii)	
Unit Hyd. Tpeak (min)=	5.00	25.00	
Unit Hyd. peak (cms)=	0.21	0.05	
			*TOTALS*
PEAK FLOW (cms)=	0.26	0.02	0.272 (iii)
TIME TO PEAK (hrs)=	2.50	2.75	2.50
RUNOFF VOLUME (mm)=	35.00	12.67	30.53
TOTAL RAINFALL (mm)=	36.00	36.00	36.00
RUNOFF COEFFICIENT =	0.97	0.35	0.85

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| ADD HYD ( 0110) |
| 1 + 2 = 3 |
-----
  
```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 ( 0100):	3.52	0.272	2.50	30.53
+ ID2= 2 ( 1002):	0.04	0.001	2.58	12.63
=====				
ID = 3 ( 0110):	3.56	0.273	2.50	30.34

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.



ADD HYD ( 0110)	AREA	QPEAK	TPEAK	R.V.
3 + 2 = 1	(ha)	(cms)	(hrs)	(mm)
ID1= 3 ( 0110):	3.56	0.273	2.50	30.34
+ ID2= 2 ( 0101):	2.87	0.245	2.50	32.32
=====				
ID = 1 ( 0110):	6.43	0.518	2.50	31.22

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 0110)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 0110):	6.43	0.518	2.50	31.22
+ ID2= 2 ( 1012):	0.75	0.025	2.58	12.65
=====				
ID = 3 ( 0110):	7.19	0.543	2.50	29.27

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

V   V   I   SSSSS  U   U   A   L           (v 6.0.2001)
V   V   I   SS     U   U   A A  L
V   V   I   SS     U   U  AAAAA L
V   V   I   SS     U   U   A   A  L
  VV    I   SSSSS  UUUUU  A   A  LLLLL

000  TTTTT  TTTTT  H   H  Y   Y  M   M  000  TM
O   O   T    T    H   H  Y   Y  MM  MM  O   O
O   O   T    T    H   H  Y   M   M  O   O
000  T    T    H   H  Y   M   M  000
    
```

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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

Input filename: C:\Program Files (x86)\Visual OTTHYMO 6.0\V02\voin.dat

Output filename:

C:\Users\jliang\AppData\Local\Civica\XH5\becad37f-97fe-4a15-a3fd-f87dd2156d5f\c406c1b1-3321-4edc-a7cd-766ff93cc048\scena

Summary filename:

C:\Users\jliang\AppData\Local\Civica\XH5\becad37f-97fe-4a15-a3fd-f87dd2156d5f\c406c



1b1-3321-4edc-a7cd-766ff93cc048\scena

DATE: 10-18-2021

TIME: 02:27:40

USER:

COMMENTS: \_\_\_\_\_

\*\*\*\*\*  
 \*\* SIMULATION : Run 02 \*\*  
 \*\*\*\*\*

READ STORM	Filename: C:\Users\jliang\AppData\Local\Temp\
Ptotal= 47.81 mm	f9a46910-ba32-4004-be5f-e15416527993\ca9c443b
	Comments: 5-Year 6-hour AES Storm

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.25	0.96	1.75	16.25	3.25	6.69	4.75	0.96
0.50	0.96	2.00	16.25	3.50	6.69	5.00	0.96
0.75	0.96	2.25	43.98	3.75	3.82	5.25	0.96
1.00	0.96	2.50	43.98	4.00	3.82	5.50	0.96
1.25	5.74	2.75	12.43	4.25	1.91	5.75	0.96
1.50	5.74	3.00	12.43	4.50	1.91	6.00	0.96

CALIB	
NASHYD ( 1012)	Area (ha)= 0.75 Curve Number (CN)= 85.0
ID= 1 DT= 5.0 min	Ia (mm)= 5.00 # of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= 0.20

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	0.96	1.583	16.25	3.083	6.69	4.58	0.96
0.167	0.96	1.667	16.25	3.167	6.69	4.67	0.96





0.250	0.96	1.750	16.25	3.250	6.69	4.75	0.96
0.333	0.96	1.833	16.25	3.333	6.69	4.83	0.96
0.417	0.96	1.917	16.25	3.417	6.69	4.92	0.96
0.500	0.96	2.000	16.25	3.500	6.69	5.00	0.96
0.583	0.96	2.083	43.98	3.583	3.82	5.08	0.96
0.667	0.96	2.167	43.98	3.667	3.82	5.17	0.96
0.750	0.96	2.250	43.98	3.750	3.82	5.25	0.96
0.833	0.96	2.333	43.98	3.833	3.82	5.33	0.96
0.917	0.96	2.417	43.98	3.917	3.82	5.42	0.96
1.000	0.96	2.500	43.98	4.000	3.82	5.50	0.96
1.083	5.74	2.583	12.43	4.083	1.91	5.58	0.96
1.167	5.74	2.667	12.43	4.167	1.91	5.67	0.96
1.250	5.74	2.750	12.43	4.250	1.91	5.75	0.96
1.333	5.74	2.833	12.43	4.333	1.91	5.83	0.96
1.417	5.74	2.917	12.43	4.417	1.91	5.92	0.96
1.500	5.74	3.000	12.43	4.500	1.91	6.00	0.96

Unit Hyd Qpeak (cms)= 0.144

PEAK FLOW (cms)= 0.042 (i)  
 TIME TO PEAK (hrs)= 2.500  
 RUNOFF VOLUME (mm)= 20.873  
 TOTAL RAINFALL (mm)= 47.810  
 RUNOFF COEFFICIENT = 0.437

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 -----  

CALIB			
NASHYD ( 1002)	Area (ha)= 0.04	Curve Number (CN)= 85.0	
ID= 1 DT= 5.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00	
	U.H. Tp(hrs)= 0.20		

 -----  
 -----

Unit Hyd Qpeak (cms)= 0.007

PEAK FLOW (cms)= 0.002 (i)  
 TIME TO PEAK (hrs)= 2.500  
 RUNOFF VOLUME (mm)= 20.852  
 TOTAL RAINFALL (mm)= 47.810  
 RUNOFF COEFFICIENT = 0.436

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 -----  

CALIB			
STANDHYD ( 0101)	Area (ha)= 2.87		
ID= 1 DT= 5.0 min	Total Imp(%)= 88.00	Dir. Conn.(%)= 88.00	

 -----  
 -----



	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	2.53	0.34	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	138.40	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	43.98	25.95	
over (min)	5.00	10.00	
Storage Coeff. (min)=	4.31 (ii)	8.73 (ii)	
Unit Hyd. Tpeak (min)=	5.00	10.00	
Unit Hyd. peak (cms)=	0.23	0.12	
			*TOTALS*
PEAK FLOW (cms)=	0.31	0.02	0.330 (iii)
TIME TO PEAK (hrs)=	2.50	2.50	2.50
RUNOFF VOLUME (mm)=	46.81	20.91	43.70
TOTAL RAINFALL (mm)=	47.81	47.81	47.81
RUNOFF COEFFICIENT =	0.98	0.44	0.91

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0    Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB		STANDHYD ( 0100)	
ID= 1	DT= 5.0 min	Area (ha)= 3.52	Total Imp(%)= 80.00    Dir. Conn.(%)= 80.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	2.82	0.70	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	153.21	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	43.98	24.90	
over (min)	5.00	20.00	
Storage Coeff. (min)=	4.58 (ii)	16.89 (ii)	
Unit Hyd. Tpeak (min)=	5.00	20.00	
Unit Hyd. peak (cms)=	0.23	0.06	
			*TOTALS*
PEAK FLOW (cms)=	0.34	0.03	0.373 (iii)
TIME TO PEAK (hrs)=	2.50	2.67	2.50
RUNOFF VOLUME (mm)=	46.81	20.91	41.63
TOTAL RAINFALL (mm)=	47.81	47.81	47.81
RUNOFF COEFFICIENT =	0.98	0.44	0.87



- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0    Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| ADD HYD ( 0110) |
| 1 + 2 = 3      |
-----
                AREA   QPEAK   TPEAK   R.V.
                (ha)   (cms)   (hrs)   (mm)
ID1= 1 ( 0100):  3.52  0.373  2.50   41.63
+ ID2= 2 ( 1002):  0.04  0.002  2.50   20.85
=====
ID = 3 ( 0110):  3.56  0.375  2.50   41.40
  
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| ADD HYD ( 0110) |
| 3 + 2 = 1      |
-----
                AREA   QPEAK   TPEAK   R.V.
                (ha)   (cms)   (hrs)   (mm)
ID1= 3 ( 0110):  3.56  0.375  2.50   41.40
+ ID2= 2 ( 0101):  2.87  0.330  2.50   43.70
=====
ID = 1 ( 0110):  6.43  0.705  2.50   42.43
  
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| ADD HYD ( 0110) |
| 1 + 2 = 3      |
-----
                AREA   QPEAK   TPEAK   R.V.
                (ha)   (cms)   (hrs)   (mm)
ID1= 1 ( 0110):  6.43  0.705  2.50   42.43
+ ID2= 2 ( 1012):  0.75  0.042  2.50   20.87
=====
ID = 3 ( 0110):  7.19  0.747  2.50   40.17
  
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

=====
V  V  I  SSSS  U  U  A  L          (v 6.0.2001)
V  V  I  SS   U  U  A  A  L
V  V  I  SS   U  U  AAAAA L
V  V  I  SS   U  U  A  A  L
  
```



```

VV      I      SSSSS  UUUUU  A  A  LLLLL
000    TTTTT  TTTTT  H  H  Y  Y  M  M  000  TM
0 0    T      T      H  H  Y  Y  MM MM 0 0
0 0    T      T      H  H  Y      M  M 0 0
000    T      T      H  H  Y      M  M 000
    
```

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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

Input filename: C:\Program Files (x86)\Visual OTTHYMO 6.0\V02\voin.dat

Output filename:

C:\Users\jliang\AppData\Local\Civica\XH5\becad37f-97fe-4a15-a3fd-f87dd2156d5f\d18f6c1a-1fb8-452f-924b-3a7b45c67d71\scena

Summary filename:

C:\Users\jliang\AppData\Local\Civica\XH5\becad37f-97fe-4a15-a3fd-f87dd2156d5f\d18f6c1a-1fb8-452f-924b-3a7b45c67d71\scena

DATE: 10-18-2021

TIME: 02:27:40

USER:

COMMENTS: \_\_\_\_\_

```

*****
** SIMULATION : Run 03          **
*****
    
```

```

-----
| READ STORM |      Filename: C:\Users\jliang\AppData
|            |      ata\Local\Temp\
|            |      f9a46910-ba32-4004-be5f-e15416527993\8b3892d6
| Ptotal= 55.69 mm |      Comments: 10-Year 6-hour AES Storm
-----
    
```

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.25	1.11	1.75	18.94	3.25	7.80	4.75	1.11
0.50	1.11	2.00	18.94	3.50	7.80	5.00	1.11



0.75	1.11	2.25	51.24	3.75	4.46	5.25	1.11
1.00	1.11	2.50	51.24	4.00	4.46	5.50	1.11
1.25	6.68	2.75	14.48	4.25	2.23	5.75	1.11
1.50	6.68	3.00	14.48	4.50	2.23	6.00	1.11

CALIB							
NASHYD ( 1012)	Area (ha)=	0.75	Curve Number (CN)=	85.0			
ID= 1 DT= 5.0 min	Ia (mm)=	5.00	# of Linear Res.(N)=	3.00			
	U.H. Tp(hrs)=	0.20					

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	1.11	1.583	18.94	3.083	7.80	4.58	1.11
0.167	1.11	1.667	18.94	3.167	7.80	4.67	1.11
0.250	1.11	1.750	18.94	3.250	7.80	4.75	1.11
0.333	1.11	1.833	18.94	3.333	7.80	4.83	1.11
0.417	1.11	1.917	18.94	3.417	7.80	4.92	1.11
0.500	1.11	2.000	18.94	3.500	7.80	5.00	1.11
0.583	1.11	2.083	51.24	3.583	4.46	5.08	1.11
0.667	1.11	2.167	51.24	3.667	4.46	5.17	1.11
0.750	1.11	2.250	51.24	3.750	4.46	5.25	1.11
0.833	1.11	2.333	51.24	3.833	4.46	5.33	1.11
0.917	1.11	2.417	51.24	3.917	4.46	5.42	1.11
1.000	1.11	2.500	51.24	4.000	4.46	5.50	1.11
1.083	6.68	2.583	14.48	4.083	2.23	5.58	1.11
1.167	6.68	2.667	14.48	4.167	2.23	5.67	1.11
1.250	6.68	2.750	14.48	4.250	2.23	5.75	1.11
1.333	6.68	2.833	14.48	4.333	2.23	5.83	1.11
1.417	6.68	2.917	14.48	4.417	2.23	5.92	1.11
1.500	6.68	3.000	14.48	4.500	2.23	6.00	1.11

Unit Hyd Qpeak (cms)= 0.144

PEAK FLOW (cms)= 0.055 (i)

TIME TO PEAK (hrs)= 2.500

RUNOFF VOLUME (mm)= 26.850

TOTAL RAINFALL (mm)= 55.690

RUNOFF COEFFICIENT = 0.482

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.



CALIB			
NASHYD ( 1002)	Area (ha)=	0.04	Curve Number (CN)= 85.0
ID= 1 DT= 5.0 min	Ia (mm)=	5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)=	0.20	

Unit Hyd Qpeak (cms)= 0.007

PEAK FLOW (cms)= 0.003 (i)  
 TIME TO PEAK (hrs)= 2.500  
 RUNOFF VOLUME (mm)= 26.830  
 TOTAL RAINFALL (mm)= 55.690  
 RUNOFF COEFFICIENT = 0.482

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD ( 0101)	Area (ha)=	2.87	
ID= 1 DT= 5.0 min	Total Imp(%)=	88.00	Dir. Conn.(%)= 88.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	2.53	0.34
Dep. Storage (mm)=	1.00	5.00
Average Slope (%)=	1.00	2.00
Length (m)=	138.40	40.00
Mannings n =	0.013	0.250

Max.Eff.Inten.(mm/hr)=	51.24	32.92
over (min)	5.00	10.00
Storage Coeff. (min)=	4.06 (ii)	8.21 (ii)
Unit Hyd. Tpeak (min)=	5.00	10.00
Unit Hyd. peak (cms)=	0.24	0.13

\*TOTALS\*

PEAK FLOW (cms)=	0.36	0.03	0.388 (iii)
TIME TO PEAK (hrs)=	2.50	2.50	2.50
RUNOFF VOLUME (mm)=	54.69	26.90	51.35
TOTAL RAINFALL (mm)=	55.69	55.69	55.69
RUNOFF COEFFICIENT =	0.98	0.48	0.92

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:

CN\* = 85.0 Ia = Dep. Storage (Above)

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB		
STANDHYD ( 0100)	Area (ha)=	3.52



| ID= 1 DT= 5.0 min | Total Imp(%)= 80.00 Dir. Conn.(%)= 80.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	2.82	0.70	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	153.21	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	51.24	31.75	
over (min)	5.00	20.00	
Storage Coeff. (min)=	4.31 (ii)	15.48 (ii)	
Unit Hyd. Tpeak (min)=	5.00	20.00	
Unit Hyd. peak (cms)=	0.23	0.07	
			*TOTALS*
PEAK FLOW (cms)=	0.40	0.04	0.440 (iii)
TIME TO PEAK (hrs)=	2.50	2.67	2.50
RUNOFF VOLUME (mm)=	54.69	26.90	49.13
TOTAL RAINFALL (mm)=	55.69	55.69	55.69
RUNOFF COEFFICIENT =	0.98	0.48	0.88

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD ( 0110)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 0100):	3.52	0.440	2.50	49.13
+ ID2= 2 ( 1002):	0.04	0.003	2.50	26.83
=====				
ID = 3 ( 0110):	3.56	0.443	2.50	48.89

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 0110)	AREA	QPEAK	TPEAK	R.V.
3 + 2 = 1	(ha)	(cms)	(hrs)	(mm)
ID1= 3 ( 0110):	3.56	0.443	2.50	48.89
+ ID2= 2 ( 0101):	2.87	0.388	2.50	51.35
=====				
ID = 1 ( 0110):	6.43	0.831	2.50	49.99



NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| ADD HYD ( 0110)|
| 1 + 2 = 3 |
-----
          AREA      QPEAK      TPEAK      R.V.
          (ha)      (cms)      (hrs)      (mm)
ID1= 1 ( 0110):  6.43    0.831    2.50    49.99
+ ID2= 2 ( 1012):  0.75    0.055    2.50    26.85
=====
ID = 3 ( 0110):  7.19    0.885    2.50    47.56

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
=====
V  V  I  SSSSS  U  U  A  L              (v 6.0.2001)
V  V  I  SS    U  U  A  A  L
V  V  I  SS    U  U  AAAAA  L
V  V  I  SS    U  U  A  A  L
  VV   I  SSSSS  UUUUU  A  A  LLLLL
-----
000  TTTTT  TTTTT  H  H  Y  Y  M  M  000  TM
O  O  T  T  H  H  Y  Y  MM  MM  O  O
O  O  T  T  H  H  Y  M  M  O  O
000  T  T  H  H  Y  M  M  000

```

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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

Input filename: C:\Program Files (x86)\Visual OTTHYMO 6.0\V02\voin.dat

Output filename:

C:\Users\jliang\AppData\Local\Civica\XH5\becad37f-97fe-4a15-a3fd-f87dd2156d5f\55e3b69d-a9b0-4885-b2b0-fe07fc3b0ffb\scena

Summary filename:

C:\Users\jliang\AppData\Local\Civica\XH5\becad37f-97fe-4a15-a3fd-f87dd2156d5f\55e3b69d-a9b0-4885-b2b0-fe07fc3b0ffb\scena

DATE: 10-18-2021

TIME: 02:27:40

USER:





COMMENTS: \_\_\_\_\_

\*\*\*\*\*  
 \*\* SIMULATION : Run 04 \*\*  
 \*\*\*\*\*

READ STORM	Filename: C:\Users\jliang\AppData\Local\Temp\
Ptotal= 65.59 mm	f9a46910-ba32-4004-be5f-e15416527993\88868af7
	Comments: 25-Year 6-hour AES Storm

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.25	1.31	1.75	22.30	3.25	9.18	4.75	1.31
0.50	1.31	2.00	22.30	3.50	9.18	5.00	1.31
0.75	1.31	2.25	60.35	3.75	5.25	5.25	1.31
1.00	1.31	2.50	60.35	4.00	5.25	5.50	1.31
1.25	7.87	2.75	17.06	4.25	2.62	5.75	1.31
1.50	7.87	3.00	17.06	4.50	2.62	6.00	1.31

CALIB			
NASHYD ( 1012)	Area (ha)= 0.75	Curve Number (CN)= 85.0	
ID= 1 DT= 5.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00	
	U.H. Tp(hrs)= 0.20		

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	1.31	1.583	22.30	3.083	9.18	4.58	1.31
0.167	1.31	1.667	22.30	3.167	9.18	4.67	1.31
0.250	1.31	1.750	22.30	3.250	9.18	4.75	1.31
0.333	1.31	1.833	22.30	3.333	9.18	4.83	1.31
0.417	1.31	1.917	22.30	3.417	9.18	4.92	1.31
0.500	1.31	2.000	22.30	3.500	9.18	5.00	1.31
0.583	1.31	2.083	60.35	3.583	5.25	5.08	1.31
0.667	1.31	2.167	60.35	3.667	5.25	5.17	1.31
0.750	1.31	2.250	60.35	3.750	5.25	5.25	1.31
0.833	1.31	2.333	60.35	3.833	5.25	5.33	1.31



0.917	1.31	2.417	60.35	3.917	5.25	5.42	1.31
1.000	1.31	2.500	60.35	4.000	5.25	5.50	1.31
1.083	7.87	2.583	17.06	4.083	2.62	5.58	1.31
1.167	7.87	2.667	17.06	4.167	2.62	5.67	1.31
1.250	7.87	2.750	17.06	4.250	2.62	5.75	1.31
1.333	7.87	2.833	17.06	4.333	2.62	5.83	1.31
1.417	7.87	2.917	17.06	4.417	2.62	5.92	1.31
1.500	7.87	3.000	17.06	4.500	2.62	6.00	1.31

Unit Hyd Qpeak (cms)= 0.144

PEAK FLOW (cms)= 0.071 (i)  
 TIME TO PEAK (hrs)= 2.500  
 RUNOFF VOLUME (mm)= 34.759  
 TOTAL RAINFALL (mm)= 65.590  
 RUNOFF COEFFICIENT = 0.530

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
NASHYD ( 1002)	Area (ha)= 0.04	Curve Number (CN)= 85.0	
ID= 1 DT= 5.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00	
	U.H. Tp(hrs)= 0.20		

Unit Hyd Qpeak (cms)= 0.007

PEAK FLOW (cms)= 0.004 (i)  
 TIME TO PEAK (hrs)= 2.500  
 RUNOFF VOLUME (mm)= 34.742  
 TOTAL RAINFALL (mm)= 65.590  
 RUNOFF COEFFICIENT = 0.530

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD ( 0101)	Area (ha)= 2.87		
ID= 1 DT= 5.0 min	Total Imp(%)= 88.00	Dir. Conn.(%)= 88.00	

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	2.53	0.34
Dep. Storage (mm)=	1.00	5.00
Average Slope (%)=	1.00	2.00
Length (m)=	138.40	40.00
Mannings n =	0.013	0.250
Max. Eff. Inten. (mm/hr)=	60.35	41.96



over (min)	5.00	10.00	
Storage Coeff. (min)=	3.80 (ii)	7.69 (ii)	
Unit Hyd. Tpeak (min)=	5.00	10.00	
Unit Hyd. peak (cms)=	0.25	0.13	
			*TOTALS*
PEAK FLOW (cms)=	0.42	0.04	0.460 (iii)
TIME TO PEAK (hrs)=	2.50	2.50	2.50
RUNOFF VOLUME (mm)=	64.59	34.83	61.02
TOTAL RAINFALL (mm)=	65.59	65.59	65.59
RUNOFF COEFFICIENT =	0.98	0.53	0.93

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD ( 0100)	Area (ha)=	3.52	
ID= 1 DT= 5.0 min	Total Imp(%)=	80.00	Dir. Conn.(%)= 80.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	2.82	0.70	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	153.21	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	60.35	41.96	
over (min)	5.00	10.00	
Storage Coeff. (min)=	4.04 (ii)	9.00 (ii)	
Unit Hyd. Tpeak (min)=	5.00	10.00	
Unit Hyd. peak (cms)=	0.24	0.12	
			*TOTALS*
PEAK FLOW (cms)=	0.47	0.07	0.544 (iii)
TIME TO PEAK (hrs)=	2.50	2.50	2.50
RUNOFF VOLUME (mm)=	64.59	34.83	58.64
TOTAL RAINFALL (mm)=	65.59	65.59	65.59
RUNOFF COEFFICIENT =	0.98	0.53	0.89

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.



```

-----
| ADD HYD ( 0110) |
| 1 + 2 = 3 |
-----
          AREA    QPEAK    TPEAK    R.V.
          (ha)    (cms)    (hrs)    (mm)
ID1= 1 ( 0100):  3.52    0.544    2.50    58.64
+ ID2= 2 ( 1002):  0.04    0.004    2.50    34.74
=====
ID = 3 ( 0110):  3.56    0.548    2.50    58.37
    
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| ADD HYD ( 0110) |
| 3 + 2 = 1 |
-----
          AREA    QPEAK    TPEAK    R.V.
          (ha)    (cms)    (hrs)    (mm)
ID1= 3 ( 0110):  3.56    0.548    2.50    58.37
+ ID2= 2 ( 0101):  2.87    0.460    2.50    61.02
=====
ID = 1 ( 0110):  6.43    1.008    2.50    59.55
    
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| ADD HYD ( 0110) |
| 1 + 2 = 3 |
-----
          AREA    QPEAK    TPEAK    R.V.
          (ha)    (cms)    (hrs)    (mm)
ID1= 1 ( 0110):  6.43    1.008    2.50    59.55
+ ID2= 2 ( 1012):  0.75    0.071    2.50    34.76
=====
ID = 3 ( 0110):  7.19    1.079    2.50    56.95
    
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

V V I SSSSS U U A L (v 6.0.2001)
V V I SS U U A A L
V V I SS U U AAAAA L
V V I SS U U A A L
VV I SSSSS UUUUU A A LLLLL
    
```

```

000 TTTTT TTTTT H H Y Y M M 000 TM
0 0 T T H H Y Y MM MM 0 0
0 0 T T H H Y M M 0 0
000 T T H H Y M M 000
    
```

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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

Input filename: C:\Program Files (x86)\Visual OTTHYMO 6.0\V02\voin.dat

Output filename:

C:\Users\jliang\AppData\Local\Civica\XH5\becad37f-97fe-4a15-a3fd-f87dd2156d5f\6846d  
b57-6a69-4bf8-9b3b-d317268abaa3\scena

Summary filename:

C:\Users\jliang\AppData\Local\Civica\XH5\becad37f-97fe-4a15-a3fd-f87dd2156d5f\6846d  
b57-6a69-4bf8-9b3b-d317268abaa3\scena

DATE: 10-18-2021

TIME: 02:27:40

USER:

COMMENTS: \_\_\_\_\_

-----  
-----  
\*\*\*\*\*  
\*\* SIMULATION : Run 05 \*\*  
\*\*\*\*\*

READ STORM	Filename: C:\Users\jliang\AppData\Local\Temp\
Ptotal= 73.00 mm	f9a46910-ba32-4004-be5f-e15416527993\d9be6e7f
	Comments: 50-Year 6-hour AES Storm

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.25	1.46	1.75	24.82	3.25	10.22	4.75	1.46
0.50	1.46	2.00	24.82	3.50	10.22	5.00	1.46
0.75	1.46	2.25	67.16	3.75	5.84	5.25	1.46
1.00	1.46	2.50	67.16	4.00	5.84	5.50	1.46
1.25	8.76	2.75	18.98	4.25	2.92	5.75	1.46
1.50	8.76	3.00	18.98	4.50	2.92	6.00	1.46



CALIB			
NASHYD ( 1012)	Area (ha)=	0.75	Curve Number (CN)= 85.0
ID= 1 DT= 5.0 min	Ia (mm)=	5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)=	0.20	

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

----- TRANSFORMED HYETOGRAPH -----							
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	1.46	1.583	24.82	3.083	10.22	4.58	1.46
0.167	1.46	1.667	24.82	3.167	10.22	4.67	1.46
0.250	1.46	1.750	24.82	3.250	10.22	4.75	1.46
0.333	1.46	1.833	24.82	3.333	10.22	4.83	1.46
0.417	1.46	1.917	24.82	3.417	10.22	4.92	1.46
0.500	1.46	2.000	24.82	3.500	10.22	5.00	1.46
0.583	1.46	2.083	67.16	3.583	5.84	5.08	1.46
0.667	1.46	2.167	67.16	3.667	5.84	5.17	1.46
0.750	1.46	2.250	67.16	3.750	5.84	5.25	1.46
0.833	1.46	2.333	67.16	3.833	5.84	5.33	1.46
0.917	1.46	2.417	67.16	3.917	5.84	5.42	1.46
1.000	1.46	2.500	67.16	4.000	5.84	5.50	1.46
1.083	8.76	2.583	18.98	4.083	2.92	5.58	1.46
1.167	8.76	2.667	18.98	4.167	2.92	5.67	1.46
1.250	8.76	2.750	18.98	4.250	2.92	5.75	1.46
1.333	8.76	2.833	18.98	4.333	2.92	5.83	1.46
1.417	8.76	2.917	18.98	4.417	2.92	5.92	1.46
1.500	8.76	3.000	18.98	4.500	2.92	6.00	1.46

Unit Hyd Qpeak (cms)= 0.144

PEAK FLOW (cms)= 0.084 (i)

TIME TO PEAK (hrs)= 2.500

RUNOFF VOLUME (mm)= 40.906

TOTAL RAINFALL (mm)= 73.000

RUNOFF COEFFICIENT = 0.560

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
NASHYD ( 1002)	Area (ha)=	0.04	Curve Number (CN)= 85.0
ID= 1 DT= 5.0 min	Ia (mm)=	5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)=	0.20	

Unit Hyd Qpeak (cms)= 0.007

PEAK FLOW (cms)= 0.004 (i)



TIME TO PEAK (hrs)= 2.500  
 RUNOFF VOLUME (mm)= 40.886  
 TOTAL RAINFALL (mm)= 73.000  
 RUNOFF COEFFICIENT = 0.560

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB  
 STANDHYD ( 0101)  
 ID= 1 DT= 5.0 min

Area (ha)= 2.87  
 Total Imp(%)= 88.00 Dir. Conn.(%)= 88.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	2.53	0.34	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	138.40	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	67.16	48.86	
over (min)	5.00	10.00	
Storage Coeff. (min)=	3.64 (ii)	7.37 (ii)	
Unit Hyd. Tpeak (min)=	5.00	10.00	
Unit Hyd. peak (cms)=	0.25	0.13	
			*TOTALS*
PEAK FLOW (cms)=	0.47	0.04	0.514 (iii)
TIME TO PEAK (hrs)=	2.50	2.50	2.50
RUNOFF VOLUME (mm)=	72.00	40.98	68.28
TOTAL RAINFALL (mm)=	73.00	73.00	73.00
RUNOFF COEFFICIENT =	0.99	0.56	0.94

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:

CN\* = 85.0 Ia = Dep. Storage (Above)

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB  
 STANDHYD ( 0100)  
 ID= 1 DT= 5.0 min

Area (ha)= 3.52  
 Total Imp(%)= 80.00 Dir. Conn.(%)= 80.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	2.82	0.70
Dep. Storage (mm)=	1.00	5.00
Average Slope (%)=	1.00	2.00
Length (m)=	153.21	40.00
Mannings n =	0.013	0.250



Max.Eff.Inten.(mm/hr)=	67.16	48.86	
over (min)	5.00	10.00	
Storage Coeff. (min)=	3.87 (ii)	8.62 (ii)	
Unit Hyd. Tpeak (min)=	5.00	10.00	
Unit Hyd. peak (cms)=	0.25	0.12	
			*TOTALS*
PEAK FLOW (cms)=	0.53	0.09	0.611 (iii)
TIME TO PEAK (hrs)=	2.50	2.50	2.50
RUNOFF VOLUME (mm)=	72.00	40.98	65.80
TOTAL RAINFALL (mm)=	73.00	73.00	73.00
RUNOFF COEFFICIENT =	0.99	0.56	0.90

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD ( 0110)				
1 + 2 = 3	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 0100):	3.52	0.611	2.50	65.80
+ ID2= 2 ( 1002):	0.04	0.004	2.50	40.89
=====				
ID = 3 ( 0110):	3.56	0.615	2.50	65.52

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 0110)				
3 + 2 = 1	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 3 ( 0110):	3.56	0.615	2.50	65.52
+ ID2= 2 ( 0101):	2.87	0.514	2.50	68.28
=====				
ID = 1 ( 0110):	6.43	1.130	2.50	66.75

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 0110)				
1 + 2 = 3	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 0110):	6.43	1.130	2.50	66.75





```
+ ID2= 2 ( 1012):    0.75  0.084  2.50  40.91
=====
ID = 3 ( 0110):    7.19  1.214  2.50  64.04
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```
V  V  I  SSSSS  U  U  A  L          (v 6.0.2001)
V  V  I  SS    U  U  A  A  L
V  V  I  SS    U  U  AAAAA  L
V  V  I  SS    U  U  A  A  L
VV   I  SSSSS  UUUUU  A  A  LLLLL
```

```
000  TTTTT  TTTTT  H  H  Y  Y  M  M  000  TM
O  O  T  T  H  H  Y  Y  MM  MM  O  O
O  O  T  T  H  H  Y  M  M  O  O
000  T  T  H  H  Y  M  M  000
```

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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

Input filename: C:\Program Files (x86)\Visual OTTHYMO 6.0\V02\voin.dat

Output filename:

C:\Users\jliang\AppData\Local\Civica\XH5\becad37f-97fe-4a15-a3fd-f87dd2156d5f\f7ad03e0-aec2-4f10-9784-ba897c30c5ac\scena

Summary filename:

C:\Users\jliang\AppData\Local\Civica\XH5\becad37f-97fe-4a15-a3fd-f87dd2156d5f\f7ad03e0-aec2-4f10-9784-ba897c30c5ac\scena

DATE: 10-18-2021

TIME: 02:27:40

USER:

COMMENTS: \_\_\_\_\_

```
*****
** SIMULATION : Run 06          **
```



\*\*\*\*\*

READ STORM	Filename: C:\Users\jliang\AppData\Local\Temp\
Ptotal= 80.31 mm	f9a46910-ba32-4004-be5f-e15416527993\40ddf276
	Comments: 100-Year 6-hour AES Storm

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.25	1.61	1.75	27.30	3.25	11.24	4.75	1.61
0.50	1.61	2.00	27.30	3.50	11.24	5.00	1.61
0.75	1.61	2.25	73.88	3.75	6.42	5.25	1.61
1.00	1.61	2.50	73.88	4.00	6.42	5.50	1.61
1.25	9.64	2.75	20.88	4.25	3.21	5.75	1.61
1.50	9.64	3.00	20.88	4.50	3.21	6.00	1.61

CALIB	Area (ha)= 0.75	Curve Number (CN)= 85.0
NASHYD ( 1012)	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
ID= 1 DT= 5.0 min	U.H. Tp(hrs)= 0.20	

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	1.61	1.583	27.30	3.083	11.24	4.58	1.61
0.167	1.61	1.667	27.30	3.167	11.24	4.67	1.61
0.250	1.61	1.750	27.30	3.250	11.24	4.75	1.61
0.333	1.61	1.833	27.30	3.333	11.24	4.83	1.61
0.417	1.61	1.917	27.30	3.417	11.24	4.92	1.61
0.500	1.61	2.000	27.30	3.500	11.24	5.00	1.61
0.583	1.61	2.083	73.88	3.583	6.42	5.08	1.61
0.667	1.61	2.167	73.88	3.667	6.42	5.17	1.61
0.750	1.61	2.250	73.88	3.750	6.42	5.25	1.61
0.833	1.61	2.333	73.88	3.833	6.42	5.33	1.61
0.917	1.61	2.417	73.88	3.917	6.42	5.42	1.61
1.000	1.61	2.500	73.88	4.000	6.42	5.50	1.61
1.083	9.64	2.583	20.88	4.083	3.21	5.58	1.61
1.167	9.64	2.667	20.88	4.167	3.21	5.67	1.61
1.250	9.64	2.750	20.88	4.250	3.21	5.75	1.61
1.333	9.64	2.833	20.88	4.333	3.21	5.83	1.61
1.417	9.64	2.917	20.88	4.417	3.21	5.92	1.61
1.500	9.64	3.000	20.88	4.500	3.21	6.00	1.61



Unit Hyd Qpeak (cms)= 0.144

PEAK FLOW (cms)= 0.097 (i)  
 TIME TO PEAK (hrs)= 2.500  
 RUNOFF VOLUME (mm)= 47.121  
 TOTAL RAINFALL (mm)= 80.310  
 RUNOFF COEFFICIENT = 0.587

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 -----  
 | CALIB |  
 | NASHYD ( 1002) | Area (ha)= 0.04 Curve Number (CN)= 85.0  
 | ID= 1 DT= 5.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00  
 -----  
 U.H. Tp(hrs)= 0.20

Unit Hyd Qpeak (cms)= 0.007

PEAK FLOW (cms)= 0.005 (i)  
 TIME TO PEAK (hrs)= 2.500  
 RUNOFF VOLUME (mm)= 47.103  
 TOTAL RAINFALL (mm)= 80.310  
 RUNOFF COEFFICIENT = 0.587

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 -----  
 | CALIB |  
 | STANDHYD ( 0101) | Area (ha)= 2.87  
 | ID= 1 DT= 5.0 min | Total Imp(%)= 88.00 Dir. Conn.(%)= 88.00  
 -----

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	2.53	0.34	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	138.40	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	73.88	55.75	
over (min)	5.00	10.00	
Storage Coeff. (min)=	3.50 (ii)	7.09 (ii)	
Unit Hyd. Tpeak (min)=	5.00	10.00	
Unit Hyd. peak (cms)=	0.26	0.14	
			*TOTALS*
PEAK FLOW (cms)=	0.52	0.05	0.568 (iii)
TIME TO PEAK (hrs)=	2.50	2.50	2.50
RUNOFF VOLUME (mm)=	79.31	47.21	75.46



TOTAL RAINFALL (mm)=	80.31	80.31	80.31
RUNOFF COEFFICIENT =	0.99	0.59	0.94

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----

CALIB	Area (ha)=	3.52		
STANDHYD ( 0100)	Total Imp(%)=	80.00	Dir. Conn.(%)=	80.00
ID= 1 DT= 5.0 min				

-----

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	2.82	0.70	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	153.21	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	73.88	55.75	
over (min)	5.00	10.00	
Storage Coeff. (min)=	3.72 (ii)	8.30 (ii)	
Unit Hyd. Tpeak (min)=	5.00	10.00	
Unit Hyd. peak (cms)=	0.25	0.13	
			*TOTALS*
PEAK FLOW (cms)=	0.58	0.10	0.677 (iii)
TIME TO PEAK (hrs)=	2.50	2.50	2.50
RUNOFF VOLUME (mm)=	79.31	47.21	72.89
TOTAL RAINFALL (mm)=	80.31	80.31	80.31
RUNOFF COEFFICIENT =	0.99	0.59	0.91

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----

ADD HYD ( 0110)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 0100):	3.52	0.677	2.50	72.89
+ ID2= 2 ( 1002):	0.04	0.005	2.50	47.10
=====				
ID = 3 ( 0110):	3.56	0.682	2.50	72.61



NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----

ADD HYD ( 0110)	AREA	QPEAK	TPEAK	R.V.
3 + 2 = 1	(ha)	(cms)	(hrs)	(mm)
ID1= 3 ( 0110):	3.56	0.682	2.50	72.61
+ ID2= 2 ( 0101):	2.87	0.568	2.50	75.46
=====				
ID = 1 ( 0110):	6.43	1.250	2.50	73.88

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----

ADD HYD ( 0110)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 0110):	6.43	1.250	2.50	73.88
+ ID2= 2 ( 1012):	0.75	0.097	2.50	47.12
=====				
ID = 3 ( 0110):	7.19	1.347	2.50	71.07

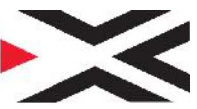
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----

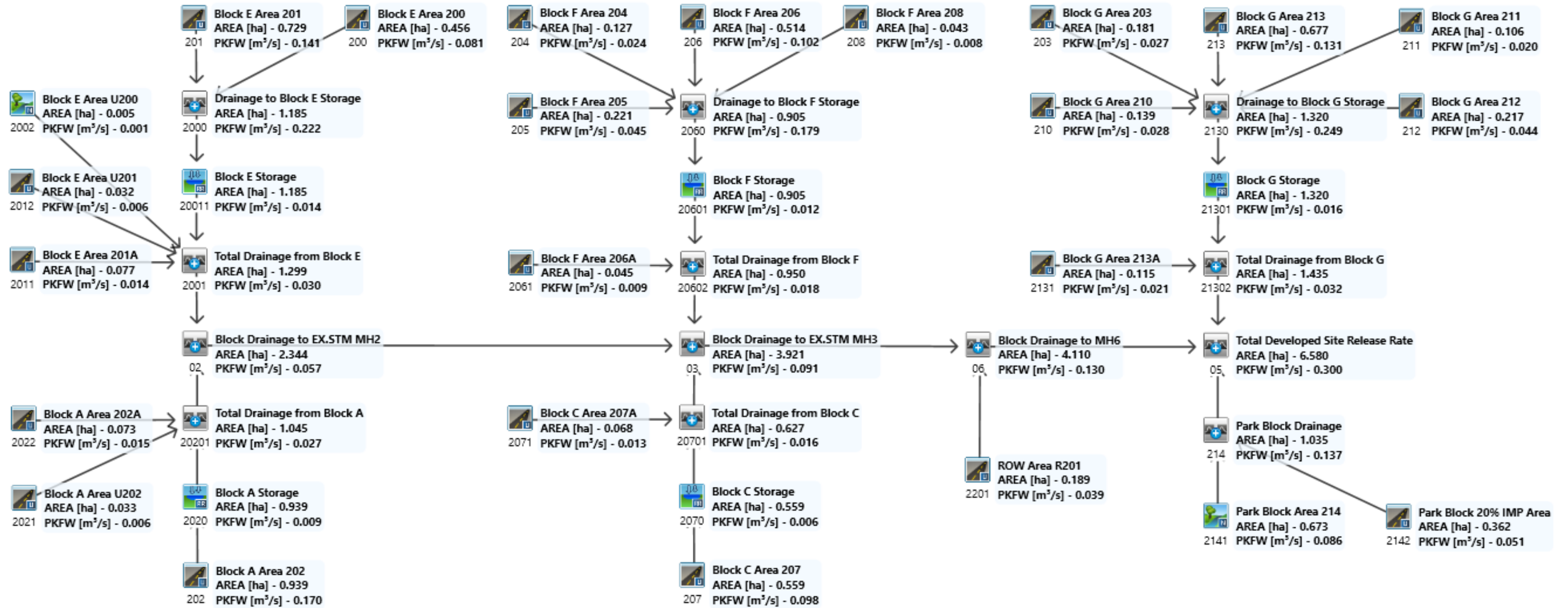
FINISH

=====

=====



# Post-Development VO6 Model Schematic





```

=====
=====
V   V   I   SSSSS U   U   A   L           (v 6.0.2001)
V   V   I   SS    U   U   A A  L
V   V   I   SS    U   U   AAAAA L
V   V   I   SS    U   U   A   A  L
  VV    I   SSSSS UUUUU A   A  LLLLL

```

```

000  TTTTT  TTTTT  H   H  Y   Y  M   M  000  TM
O   O   T    T    H   H  Y Y  MM MM  O   O
O   O   T    T    H   H  Y   M   M  O   O
000    T    T    H   H  Y   M   M  000

```

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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

Input filename: C:\Program Files (x86)\Visual OTTHYMO 6.0\V02\voin.dat

Output filename:

C:\Users\jliang\AppData\Local\Civica\XH5\becad37f-97fe-4a15-a3fd-f87dd2156d5f\b30a9  
 6aa-48fe-4f04-a2c4-f6b99f8f9cfb\scena

Summary filename:

C:\Users\jliang\AppData\Local\Civica\XH5\becad37f-97fe-4a15-a3fd-f87dd2156d5f\b30a9  
 6aa-48fe-4f04-a2c4-f6b99f8f9cfb\scena

DATE: 10-27-2021

TIME: 05:35:39

USER:

COMMENTS: \_\_\_\_\_

```

-----
-----
*****
** SIMULATION : Run 01           **
*****

```

READ STORM

Filename: C:\Users\jliang\AppData  
 ata\Local\Temp\



Ptotal= 36.00 mm

907c1cff-ccb1-41c0-9867-a9890799f0d3\05bf40b2

Comments: 2-Year 6-hour AES Storm

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.25	0.72	1.75	12.24	3.25	5.04	4.75	0.72
0.50	0.72	2.00	12.24	3.50	5.04	5.00	0.72
0.75	0.72	2.25	33.12	3.75	2.88	5.25	0.72
1.00	0.72	2.50	33.12	4.00	2.88	5.50	0.72
1.25	4.32	2.75	9.36	4.25	1.44	5.75	0.72
1.50	4.32	3.00	9.36	4.50	1.44	6.00	0.72

CALIB

NASHYD ( 2002)

ID= 1 DT= 5.0 min

Area (ha)= 0.00 Curve Number (CN)= 85.0

Ia (mm)= 5.00 # of Linear Res.(N)= 3.00

U.H. Tp(hrs)= 0.20

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	0.72	1.583	12.24	3.083	5.04	4.58	0.72
0.167	0.72	1.667	12.24	3.167	5.04	4.67	0.72
0.250	0.72	1.750	12.24	3.250	5.04	4.75	0.72
0.333	0.72	1.833	12.24	3.333	5.04	4.83	0.72
0.417	0.72	1.917	12.24	3.417	5.04	4.92	0.72
0.500	0.72	2.000	12.24	3.500	5.04	5.00	0.72
0.583	0.72	2.083	33.12	3.583	2.88	5.08	0.72
0.667	0.72	2.167	33.12	3.667	2.88	5.17	0.72
0.750	0.72	2.250	33.12	3.750	2.88	5.25	0.72
0.833	0.72	2.333	33.12	3.833	2.88	5.33	0.72
0.917	0.72	2.417	33.12	3.917	2.88	5.42	0.72
1.000	0.72	2.500	33.12	4.000	2.88	5.50	0.72
1.083	4.32	2.583	9.36	4.083	1.44	5.58	0.72
1.167	4.32	2.667	9.36	4.167	1.44	5.67	0.72
1.250	4.32	2.750	9.36	4.250	1.44	5.75	0.72
1.333	4.32	2.833	9.36	4.333	1.44	5.83	0.72
1.417	4.32	2.917	9.36	4.417	1.44	5.92	0.72
1.500	4.32	3.000	9.36	4.500	1.44	6.00	0.72

Unit Hyd Qpeak (cms)= 0.001

PEAK FLOW (cms)= 0.000 (i)

TIME TO PEAK (hrs)= 2.583

RUNOFF VOLUME (mm)= 11.244





TOTAL RAINFALL (mm)= 36.000  
 RUNOFF COEFFICIENT = 0.312

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 -----  
 | CALIB |  
 | STANDHYD ( 0201) | Area (ha)= 0.73  
 | ID= 1 DT= 5.0 min | Total Imp(%)= 80.00 Dir. Conn.(%)= 80.00  
 -----

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.58	0.15	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	69.71	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	33.12	15.30	
over (min)	5.00	20.00	
Storage Coeff. (min)=	3.20 (ii)	18.16 (ii)	
Unit Hyd. Tpeak (min)=	5.00	20.00	
Unit Hyd. peak (cms)=	0.27	0.06	
			*TOTALS*
PEAK FLOW (cms)=	0.05	0.00	0.057 (iii)
TIME TO PEAK (hrs)=	2.50	2.67	2.50
RUNOFF VOLUME (mm)=	35.00	12.67	30.52
TOTAL RAINFALL (mm)=	36.00	36.00	36.00
RUNOFF COEFFICIENT =	0.97	0.35	0.85

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 -----  
 | CALIB |  
 | STANDHYD ( 0200) | Area (ha)= 0.46  
 | ID= 1 DT= 5.0 min | Total Imp(%)= 67.00 Dir. Conn.(%)= 67.00  
 -----

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.31	0.15	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	55.14	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	33.12	15.30	



over (min)	5.00	20.00	
Storage Coeff. (min)=	2.78 (ii)	17.74 (ii)	
Unit Hyd. Tpeak (min)=	5.00	20.00	
Unit Hyd. peak (cms)=	0.28	0.06	
			*TOTALS*
PEAK FLOW (cms)=	0.03	0.00	0.032 (iii)
TIME TO PEAK (hrs)=	2.50	2.67	2.50
RUNOFF VOLUME (mm)=	35.00	12.67	27.61
TOTAL RAINFALL (mm)=	36.00	36.00	36.00
RUNOFF COEFFICIENT =	0.97	0.35	0.77

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD ( 2000)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 0200):	0.46	0.032	2.50	27.61
+ ID2= 2 ( 0201):	0.73	0.057	2.50	30.52
=====				
ID = 3 ( 2000):	1.18	0.089	2.50	29.40

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR( 20011)				
IN= 2---> OUT= 1				
DT= 5.0 min				
	OVERFLOW IS OFF			
	OUTFLOW	STORAGE	OUTFLOW	STORAGE
	(cms)	(ha.m.)	(cms)	(ha.m.)
	0.0000	0.0000	0.0140	0.0709

	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 ( 2000)	1.185	0.089	2.50	29.40
OUTFLOW: ID= 1 ( 20011)	1.185	0.006	4.08	28.32

PEAK FLOW REDUCTION [Qout/Qin](%)= 6.49  
TIME SHIFT OF PEAK FLOW (min)= 95.00  
MAXIMUM STORAGE USED (ha.m.)= 0.0291

CALIB	
STANDHYD ( 2011)	Area (ha)= 0.08



| ID= 1 DT= 5.0 min | Total Imp(%)= 73.00 Dir. Conn.(%)= 73.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.06	0.02	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	22.66	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	33.12	15.30	
over (min)	5.00	20.00	
Storage Coeff. (min)=	1.63 (ii)	16.59 (ii)	
Unit Hyd. Tpeak (min)=	5.00	20.00	
Unit Hyd. peak (cms)=	0.32	0.06	
			*TOTALS*
PEAK FLOW (cms)=	0.01	0.00	0.006 (iii)
TIME TO PEAK (hrs)=	2.50	2.67	2.50
RUNOFF VOLUME (mm)=	35.00	12.67	28.92
TOTAL RAINFALL (mm)=	36.00	36.00	36.00
RUNOFF COEFFICIENT =	0.97	0.35	0.80

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----

| CALIB |  
 | STANDHYD ( 2012) | Area (ha)= 0.03  
 | ID= 1 DT= 5.0 min | Total Imp(%)= 65.00 Dir. Conn.(%)= 65.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.02	0.01	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	14.61	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	33.12	15.30	
over (min)	5.00	20.00	
Storage Coeff. (min)=	1.25 (ii)	16.21 (ii)	
Unit Hyd. Tpeak (min)=	5.00	20.00	
Unit Hyd. peak (cms)=	0.33	0.06	
			*TOTALS*
PEAK FLOW (cms)=	0.00	0.00	0.002 (iii)
TIME TO PEAK (hrs)=	2.25	2.67	2.50
RUNOFF VOLUME (mm)=	35.00	12.67	26.10
TOTAL RAINFALL (mm)=	36.00	36.00	36.00



RUNOFF COEFFICIENT = 0.97 0.35 0.72

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| ADD HYD ( 2001) |
| 1 + 2 = 3      |
-----
          AREA    QPEAK    TPEAK    R.V.
          (ha)    (cms)    (hrs)    (mm)
ID1= 1 ( 2001):  1.18  0.006  4.08  28.32
+ ID2= 2 ( 2002):  0.00  0.000  2.58  11.24
=====
ID = 3 ( 2001):  1.19  0.006  4.08  28.25
  
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| ADD HYD ( 2001) |
| 3 + 2 = 1      |
-----
          AREA    QPEAK    TPEAK    R.V.
          (ha)    (cms)    (hrs)    (mm)
ID1= 3 ( 2001):  1.19  0.006  4.08  28.25
+ ID2= 2 ( 2011):  0.08  0.006  2.50  28.92
=====
ID = 1 ( 2001):  1.27  0.010  2.50  28.29
  
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| ADD HYD ( 2001) |
| 1 + 2 = 3      |
-----
          AREA    QPEAK    TPEAK    R.V.
          (ha)    (cms)    (hrs)    (mm)
ID1= 1 ( 2001):  1.27  0.010  2.50  28.29
+ ID2= 2 ( 2012):  0.03  0.002  2.50  26.10
=====
ID = 3 ( 2001):  1.30  0.012  2.50  28.23
  
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| CALIB          |
| STANDHYD ( 0202) | Area (ha)= 0.94
| ID= 1 DT= 5.0 min | Total Imp(%)= 70.00 Dir. Conn.(%)= 70.00
-----
  
```



	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.66	0.28	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	79.12	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	33.12	15.30	
over (min)	5.00	20.00	
Storage Coeff. (min)=	3.45 (ii)	18.41 (ii)	
Unit Hyd. Tpeak (min)=	5.00	20.00	
Unit Hyd. peak (cms)=	0.26	0.06	
			*TOTALS*
PEAK FLOW (cms)=	0.06	0.01	0.067 (iii)
TIME TO PEAK (hrs)=	2.50	2.67	2.50
RUNOFF VOLUME (mm)=	35.00	12.67	28.29
TOTAL RAINFALL (mm)=	36.00	36.00	36.00
RUNOFF COEFFICIENT =	0.97	0.35	0.79

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0    Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | RESERVOIR( 2020) |  
 | IN= 2---> OUT= 1 |  
DT= 5.0 min

OVERFLOW IS OFF

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
0.0000	0.0000	0.0090	0.0561

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 ( 0202)	0.939	0.067	2.50	28.29
OUTFLOW: ID= 1 ( 2020)	0.939	0.004	4.50	26.60

PEAK FLOW REDUCTION [Qout/Qin](%)= 5.45  
 TIME SHIFT OF PEAK FLOW (min)=120.00  
 MAXIMUM STORAGE USED (ha.m.)= 0.0227

-----  
 | CALIB |  
 | STANDHYD ( 2021) |  
ID= 1 DT= 5.0 min

Area (ha)= 0.03  
 Total Imp(%)= 65.00    Dir. Conn.(%)= 65.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	0.02	0.01



Dep. Storage	(mm)=	1.00	5.00	
Average Slope	(%)=	1.00	2.00	
Length	(m)=	14.83	40.00	
Mannings n	=	0.013	0.250	
Max.Eff.Inten.(mm/hr)=		33.12	15.30	
over (min)		5.00	20.00	
Storage Coeff. (min)=		1.26 (ii)	16.22 (ii)	
Unit Hyd. Tpeak (min)=		5.00	20.00	
Unit Hyd. peak (cms)=		0.33	0.06	
				*TOTALS*
PEAK FLOW	(cms)=	0.00	0.00	0.002 (iii)
TIME TO PEAK	(hrs)=	2.25	2.67	2.50
RUNOFF VOLUME	(mm)=	35.00	12.67	26.10
TOTAL RAINFALL	(mm)=	36.00	36.00	36.00
RUNOFF COEFFICIENT	=	0.97	0.35	0.72

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0    Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB				
STANDHYD ( 2022)	Area	(ha)=	0.07	
ID= 1 DT= 5.0 min	Total Imp(%)=	99.00	Dir. Conn.(%)=	99.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	0.07	0.00	
Dep. Storage	(mm)=	1.00	5.00	
Average Slope	(%)=	1.00	2.00	
Length	(m)=	22.06	40.00	
Mannings n	=	0.013	0.250	
Max.Eff.Inten.(mm/hr)=		33.12	16.12	
over (min)		5.00	5.00	
Storage Coeff. (min)=		1.60 (ii)	3.35 (ii)	
Unit Hyd. Tpeak (min)=		5.00	5.00	
Unit Hyd. peak (cms)=		0.32	0.26	
				*TOTALS*
PEAK FLOW	(cms)=	0.01	0.00	0.007 (iii)
TIME TO PEAK	(hrs)=	2.50	2.50	2.50
RUNOFF VOLUME	(mm)=	35.00	12.67	34.77
TOTAL RAINFALL	(mm)=	36.00	36.00	36.00
RUNOFF COEFFICIENT	=	0.97	0.35	0.97

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0    Ia = Dep. Storage (Above)



- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD ( 20201)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 2020):	0.94	0.004	4.50	26.60
+ ID2= 2 ( 2021):	0.03	0.002	2.50	26.10
=====				
ID = 3 ( 20201):	0.97	0.005	2.50	26.59

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 20201)				
3 + 2 = 1				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 3 ( 20201):	0.97	0.005	2.50	26.59
+ ID2= 2 ( 2022):	0.07	0.007	2.50	34.77
=====				
ID = 1 ( 20201):	1.04	0.011	2.50	27.16

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 0002)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 2001):	1.30	0.012	2.50	28.23
+ ID2= 2 ( 20201):	1.04	0.011	2.50	27.16
=====				
ID = 3 ( 0002):	2.34	0.023	2.50	27.75

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB				
STANDHYD ( 2071)				
ID= 1 DT= 5.0 min				
Area	(ha)=	0.07		
Total Imp(%)		74.00	Dir. Conn.(%)	74.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	0.05	0.02
Dep. Storage (mm)=	1.00	5.00
Average Slope (%)=	1.00	2.00



Length	(m)=	21.29	40.00	
Mannings n	=	0.013	0.250	
Max.Eff.Inten.(mm/hr)=		33.12	15.30	
over (min)		5.00	20.00	
Storage Coeff. (min)=		1.57 (ii)	16.53 (ii)	
Unit Hyd. Tpeak (min)=		5.00	20.00	
Unit Hyd. peak (cms)=		0.33	0.06	
				*TOTALS*
PEAK FLOW	(cms)=	0.00	0.00	0.005 (iii)
TIME TO PEAK	(hrs)=	2.42	2.67	2.50
RUNOFF VOLUME	(mm)=	35.00	12.67	29.15
TOTAL RAINFALL	(mm)=	36.00	36.00	36.00
RUNOFF COEFFICIENT	=	0.97	0.35	0.81

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB				
STANDHYD ( 0207)	Area	(ha)=	0.56	
ID= 1 DT= 5.0 min	Total Imp(%)=	63.00	Dir. Conn.(%)=	63.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	0.35	0.21	
Dep. Storage	(mm)=	1.00	5.00	
Average Slope	(%)=	1.00	2.00	
Length	(m)=	61.05	40.00	
Mannings n	=	0.013	0.250	
Max.Eff.Inten.(mm/hr)=		33.12	15.30	
over (min)		5.00	20.00	
Storage Coeff. (min)=		2.96 (ii)	17.91 (ii)	
Unit Hyd. Tpeak (min)=		5.00	20.00	
Unit Hyd. peak (cms)=		0.28	0.06	
				*TOTALS*
PEAK FLOW	(cms)=	0.03	0.01	0.037 (iii)
TIME TO PEAK	(hrs)=	2.50	2.67	2.50
RUNOFF VOLUME	(mm)=	35.00	12.67	26.72
TOTAL RAINFALL	(mm)=	36.00	36.00	36.00
RUNOFF COEFFICIENT	=	0.97	0.35	0.74

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.





(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
| RESERVOIR( 2070) | OVERFLOW IS OFF
| IN= 2---> OUT= 1 |
| DT= 5.0 min      |
-----
      OUTFLOW   STORAGE   |   OUTFLOW   STORAGE
      (cms)     (ha.m.)   |   (cms)     (ha.m.)
      0.0000    0.0000   |   0.0060    0.0318

      AREA      QPEAK     TPEAK      R.V.
      (ha)      (cms)     (hrs)     (mm)
INFLOW : ID= 2 ( 0207)  0.559     0.037     2.50     26.72
OUTFLOW: ID= 1 ( 2070)  0.559     0.002     4.33     24.32

      PEAK FLOW REDUCTION [Qout/Qin](%)= 6.35
      TIME SHIFT OF PEAK FLOW (min)=110.00
      MAXIMUM STORAGE USED (ha.m.)= 0.0125

```

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-----
| ADD HYD ( 20701) |
| 1 + 2 = 3       |
-----
      AREA      QPEAK     TPEAK     R.V.
      (ha)      (cms)     (hrs)     (mm)
      ID1= 1 ( 2070):  0.56   0.002     4.33     24.32
      + ID2= 2 ( 2071):  0.07   0.005     2.50     29.15
      =====
      ID = 3 ( 20701):  0.63   0.007     2.50     24.84

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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-----
| CALIB          |
| STANDHYD ( 0204) | Area (ha)= 0.13
| ID= 1 DT= 5.0 min | Total Imp(%)= 75.00 Dir. Conn.(%)= 75.00
-----

      IMPERVIOUS      PERVIOUS (i)
Surface Area (ha)= 0.10 0.03
Dep. Storage (mm)= 1.00 5.00
Average Slope (%)= 1.00 2.00
Length (m)= 29.10 40.00
Mannings n = 0.013 0.250

Max.Eff.Inten.(mm/hr)= 33.12 15.30
      over (min) 5.00 20.00
Storage Coeff. (min)= 1.90 (ii) 16.85 (ii)
Unit Hyd. Tpeak (min)= 5.00 20.00
Unit Hyd. peak (cms)= 0.32 0.06

```

\*TOTALS\*



PEAK FLOW	(cms)=	0.01	0.00	0.010 (iii)
TIME TO PEAK	(hrs)=	2.50	2.67	2.50
RUNOFF VOLUME	(mm)=	35.00	12.67	29.37
TOTAL RAINFALL	(mm)=	36.00	36.00	36.00
RUNOFF COEFFICIENT	=	0.97	0.35	0.82

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD ( 0208)	Area (ha)=	0.04	
ID= 1 DT= 5.0 min	Total Imp(%)=	75.00	Dir. Conn.(%)= 75.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)= 0.03	0.01	
Dep. Storage	(mm)= 1.00	5.00	
Average Slope	(%)= 1.00	2.00	
Length	(m)= 16.93	40.00	
Mannings n	= 0.013	0.250	
Max.Eff.Inten.(mm/hr)=	33.12	15.30	
over (min)	5.00	20.00	
Storage Coeff. (min)=	1.37 (ii)	16.33 (ii)	
Unit Hyd. Tpeak (min)=	5.00	20.00	
Unit Hyd. peak (cms)=	0.33	0.06	
			*TOTALS*
PEAK FLOW	(cms)= 0.00	0.00	0.003 (iii)
TIME TO PEAK	(hrs)= 2.50	2.67	2.50
RUNOFF VOLUME	(mm)= 35.00	12.67	28.33
TOTAL RAINFALL	(mm)= 36.00	36.00	36.00
RUNOFF COEFFICIENT	= 0.97	0.35	0.79

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD ( 0205)	Area (ha)=	0.22	
ID= 1 DT= 5.0 min	Total Imp(%)=	99.00	Dir. Conn.(%)= 99.00

IMPERVIOUS PERVIOUS (i)



Surface Area	(ha)=	0.22	0.00	
Dep. Storage	(mm)=	1.00	5.00	
Average Slope	(%)=	1.00	2.00	
Length	(m)=	38.38	40.00	
Mannings n	=	0.013	0.250	
Max.Eff.Inten.(mm/hr)=		33.12	16.12	
over (min)		5.00	5.00	
Storage Coeff. (min)=		2.24 (ii)	3.98 (ii)	
Unit Hyd. Tpeak (min)=		5.00	5.00	
Unit Hyd. peak (cms)=		0.30	0.24	
				*TOTALS*
PEAK FLOW	(cms)=	0.02	0.00	0.020 (iii)
TIME TO PEAK	(hrs)=	2.50	2.50	2.50
RUNOFF VOLUME	(mm)=	35.00	12.67	34.77
TOTAL RAINFALL	(mm)=	36.00	36.00	36.00
RUNOFF COEFFICIENT	=	0.97	0.35	0.97

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0    Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB				
STANDHYD ( 0206)	Area	(ha)=	0.51	
ID= 1 DT= 5.0 min	Total Imp(%)=	88.00	Dir. Conn.(%)=	88.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	0.45	0.06	
Dep. Storage	(mm)=	1.00	5.00	
Average Slope	(%)=	1.00	2.00	
Length	(m)=	58.54	40.00	
Mannings n	=	0.013	0.250	
Max.Eff.Inten.(mm/hr)=		33.12	16.12	
over (min)		5.00	10.00	
Storage Coeff. (min)=		2.88 (ii)	7.83 (ii)	
Unit Hyd. Tpeak (min)=		5.00	10.00	
Unit Hyd. peak (cms)=		0.28	0.13	
				*TOTALS*
PEAK FLOW	(cms)=	0.04	0.00	0.044 (iii)
TIME TO PEAK	(hrs)=	2.50	2.50	2.50
RUNOFF VOLUME	(mm)=	35.00	12.67	32.31
TOTAL RAINFALL	(mm)=	36.00	36.00	36.00
RUNOFF COEFFICIENT	=	0.97	0.35	0.90

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:



- CN\* = 85.0    Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD ( 2060)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 0204):	0.13	0.010	2.50	29.37
+ ID2= 2 ( 0205):	0.22	0.020	2.50	34.77
=====				
ID = 3 ( 2060):	0.35	0.030	2.50	32.80

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 2060)	AREA	QPEAK	TPEAK	R.V.
3 + 2 = 1	(ha)	(cms)	(hrs)	(mm)
ID1= 3 ( 2060):	0.35	0.030	2.50	32.80
+ ID2= 2 ( 0206):	0.51	0.044	2.50	32.31
=====				
ID = 1 ( 2060):	0.86	0.074	2.50	32.51

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 2060)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 2060):	0.86	0.074	2.50	32.51
+ ID2= 2 ( 0208):	0.04	0.003	2.50	28.33
=====				
ID = 3 ( 2060):	0.90	0.077	2.50	32.31

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR( 20601)	OVERFLOW IS OFF			
IN= 2---> OUT= 1	OUTFLOW	STORAGE	OUTFLOW	STORAGE
DT= 5.0 min	(cms)	(ha.m.)	(cms)	(ha.m.)
	0.0000	0.0000	0.0120	0.0571
	AREA	QPEAK	TPEAK	R.V.



	(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 ( 2060)	0.905	0.077	2.50	32.31
OUTFLOW: ID= 1 ( 20601)	0.905	0.005	4.08	30.98

PEAK FLOW REDUCTION [Qout/Qin](%)= 6.67  
 TIME SHIFT OF PEAK FLOW (min)= 95.00  
 MAXIMUM STORAGE USED (ha.m.)= 0.0244

-----  
 | CALIB |  
 | STANDHYD ( 2061) | Area (ha)= 0.05  
 | ID= 1 DT= 5.0 min | Total Imp(%)= 82.00 Dir. Conn.(%)= 82.00  
 -----

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.04	0.01	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	17.32	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	33.12	15.30	
over (min)	5.00	20.00	
Storage Coeff. (min)=	1.39 (ii)	16.34 (ii)	
Unit Hyd. Tpeak (min)=	5.00	20.00	
Unit Hyd. peak (cms)=	0.33	0.06	
			*TOTALS*
PEAK FLOW (cms)=	0.00	0.00	0.004 (iii)
TIME TO PEAK (hrs)=	2.50	2.67	2.50
RUNOFF VOLUME (mm)=	35.00	12.67	29.96
TOTAL RAINFALL (mm)=	36.00	36.00	36.00
RUNOFF COEFFICIENT =	0.97	0.35	0.83

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | ADD HYD ( 20602) |  
 | 1 + 2 = 3 | AREA QPEAK TPEAK R.V.  
 | | (ha) (cms) (hrs) (mm)  
 ID1= 1 ( 20601): 0.90 0.005 4.08 30.98  
 + ID2= 2 ( 2061): 0.05 0.004 2.50 29.96  
 =====  
 ID = 3 ( 20602): 0.95 0.007 2.50 30.93  
 -----



NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 0003)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 0002):	2.34	0.023	2.50	27.75
+ ID2= 2 ( 20602):	0.95	0.007	2.50	30.93
=====				
ID = 3 ( 0003):	3.29	0.031	2.50	28.67

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 0003)	AREA	QPEAK	TPEAK	R.V.
3 + 2 = 1	(ha)	(cms)	(hrs)	(mm)
ID1= 3 ( 0003):	3.29	0.031	2.50	28.67
+ ID2= 2 ( 20701):	0.63	0.007	2.50	24.84
=====				
ID = 1 ( 0003):	3.92	0.037	2.50	28.06

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB	Area	(ha)=	0.19
STANDHYD ( 2201)	Total Imp(%)=	99.00	Dir. Conn.(%)= 99.00
ID= 1 DT= 5.0 min			

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.19	0.00	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	35.50	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	33.12	16.12	
over (min)	5.00	5.00	
Storage Coeff. (min)=	2.14 (ii)	3.88 (ii)	
Unit Hyd. Tpeak (min)=	5.00	5.00	
Unit Hyd. peak (cms)=	0.31	0.25	
			*TOTALS*
PEAK FLOW (cms)=	0.02	0.00	0.017 (iii)
TIME TO PEAK (hrs)=	2.50	2.50	2.50
RUNOFF VOLUME (mm)=	35.00	12.67	34.77
TOTAL RAINFALL (mm)=	36.00	36.00	36.00
RUNOFF COEFFICIENT =	0.97	0.35	0.97



- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD ( 0006)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 0003):	3.92	0.037	2.50	28.06
+ ID2= 2 ( 2201):	0.19	0.017	2.50	34.77
=====				
ID = 3 ( 0006):	4.11	0.054	2.50	28.37

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB	Area	(ha)=	0.67	Curve Number	(CN)= 85.0
NASHYD ( 2141)	Ia	(mm)=	5.00	# of Linear Res.(N)=	3.00
ID= 1 DT= 5.0 min	U.H. Tp	(hrs)=	0.20		

Unit Hyd Qpeak (cms)= 0.128

PEAK FLOW (cms)= 0.023 (i)  
 TIME TO PEAK (hrs)= 2.583  
 RUNOFF VOLUME (mm)= 12.649  
 TOTAL RAINFALL (mm)= 36.000  
 RUNOFF COEFFICIENT = 0.351

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	Area	(ha)=	0.36	Dir. Conn.(%)=	5.00
STANDHYD ( 2142)	Total Imp	(%)=	20.00		
ID= 1 DT= 5.0 min					

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	0.07	0.29
Dep. Storage (mm)=	1.00	5.00
Average Slope (%)=	1.00	2.00
Length (m)=	49.14	40.00
Mannings n =	0.013	0.250
Max.Eff.Inten.(mm/hr)=	33.12	20.67
over (min)	5.00	20.00



Storage Coeff. (min)=	2.60 (ii)	15.85 (ii)	
Unit Hyd. Tpeak (min)=	5.00	20.00	
Unit Hyd. peak (cms)=	0.29	0.07	
			*TOTALS*
PEAK FLOW (cms)=	0.00	0.01	0.012 (iii)
TIME TO PEAK (hrs)=	2.50	2.67	2.67
RUNOFF VOLUME (mm)=	35.00	14.53	15.53
TOTAL RAINFALL (mm)=	36.00	36.00	36.00
RUNOFF COEFFICIENT =	0.97	0.40	0.43

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----				
ADD HYD ( 0214)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 2141):	0.67	0.023	2.58	12.65
+ ID2= 2 ( 2142):	0.36	0.012	2.67	15.53
=====				
ID = 3 ( 0214):	1.03	0.035	2.58	13.66

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----			
CALIB			
STANDHYD ( 0210)			
ID= 1 DT= 5.0 min			
Area (ha)=	0.14		
Total Imp(%)=	92.00	Dir. Conn.(%)=	92.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.13	0.01	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	30.44	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	33.12	16.12	
over (min)	5.00	10.00	
Storage Coeff. (min)=	1.95 (ii)	6.08 (ii)	
Unit Hyd. Tpeak (min)=	5.00	10.00	
Unit Hyd. peak (cms)=	0.31	0.15	
			*TOTALS*
PEAK FLOW (cms)=	0.01	0.00	0.012 (iii)
TIME TO PEAK (hrs)=	2.42	2.50	2.50
RUNOFF VOLUME (mm)=	35.00	12.67	33.20





TOTAL RAINFALL (mm)=	36.00	36.00	36.00
RUNOFF COEFFICIENT =	0.97	0.35	0.92

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD ( 0211)	Area (ha)=	0.11	
ID= 1 DT= 5.0 min	Total Imp(%)=	75.00	Dir. Conn.(%)= 75.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.08	0.03	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	26.58	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	33.12	15.30	
over (min)	5.00	20.00	
Storage Coeff. (min)=	1.79 (ii)	16.75 (ii)	
Unit Hyd. Tpeak (min)=	5.00	20.00	
Unit Hyd. peak (cms)=	0.32	0.06	
			*TOTALS*
PEAK FLOW (cms)=	0.01	0.00	0.008 (iii)
TIME TO PEAK (hrs)=	2.42	2.67	2.50
RUNOFF VOLUME (mm)=	35.00	12.67	29.37
TOTAL RAINFALL (mm)=	36.00	36.00	36.00
RUNOFF COEFFICIENT =	0.97	0.35	0.82

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD ( 0203)	Area (ha)=	0.18	
ID= 1 DT= 5.0 min	Total Imp(%)=	32.00	Dir. Conn.(%)= 32.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.06	0.12	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	



Length	(m)=	34.74	40.00	
Mannings n	=	0.013	0.250	
Max.Eff.Inten.(mm/hr)=		33.12	15.30	
over (min)		5.00	20.00	
Storage Coeff. (min)=		2.11 (ii)	17.06 (ii)	
Unit Hyd. Tpeak (min)=		5.00	20.00	
Unit Hyd. peak (cms)=		0.31	0.06	
				*TOTALS*
PEAK FLOW (cms)=		0.01	0.00	0.008 (iii)
TIME TO PEAK (hrs)=		2.50	2.67	2.50
RUNOFF VOLUME (mm)=		35.00	12.67	19.76
TOTAL RAINFALL (mm)=		36.00	36.00	36.00
RUNOFF COEFFICIENT =		0.97	0.35	0.55

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB				
STANDHYD ( 0213)	Area (ha)=	0.68		
ID= 1 DT= 5.0 min	Total Imp(%)=	80.00	Dir. Conn.(%)=	80.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	0.54	0.14	
Dep. Storage	(mm)=	1.00	5.00	
Average Slope	(%)=	1.00	2.00	
Length	(m)=	67.18	40.00	
Mannings n	=	0.013	0.250	
Max.Eff.Inten.(mm/hr)=		33.12	15.30	
over (min)		5.00	20.00	
Storage Coeff. (min)=		3.13 (ii)	18.09 (ii)	
Unit Hyd. Tpeak (min)=		5.00	20.00	
Unit Hyd. peak (cms)=		0.27	0.06	
				*TOTALS*
PEAK FLOW (cms)=		0.05	0.00	0.053 (iii)
TIME TO PEAK (hrs)=		2.50	2.67	2.50
RUNOFF VOLUME (mm)=		35.00	12.67	30.52
TOTAL RAINFALL (mm)=		36.00	36.00	36.00
RUNOFF COEFFICIENT =		0.97	0.35	0.85

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.



(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB |
| STANDHYD ( 0212) |
| ID= 1 DT= 5.0 min |
-----

```

Area (ha)=	0.22		
Total Imp(%)=	92.00	Dir. Conn.(%)=	92.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.20	0.02	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	38.04	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	33.12	16.12	
over (min)	5.00	10.00	
Storage Coeff. (min)=	2.23 (ii)	6.36 (ii)	
Unit Hyd. Tpeak (min)=	5.00	10.00	
Unit Hyd. peak (cms)=	0.30	0.15	
			*TOTALS*
PEAK FLOW (cms)=	0.02	0.00	0.019 (iii)
TIME TO PEAK (hrs)=	2.50	2.50	2.50
RUNOFF VOLUME (mm)=	35.00	12.67	33.20
TOTAL RAINFALL (mm)=	36.00	36.00	36.00
RUNOFF COEFFICIENT =	0.97	0.35	0.92

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0    Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| ADD HYD ( 2130) |
| 1 + 2 = 3 |
-----

```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 ( 0203):	0.18	0.008	2.50	19.76
+ ID2= 2 ( 0210):	0.14	0.012	2.50	33.20
=====				
ID = 3 ( 2130):	0.32	0.020	2.50	25.60

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| ADD HYD ( 2130) |
| 3 + 2 = 1 |
-----

```

	AREA	QPEAK	TPEAK	R.V.
--	------	-------	-------	------



	(ha)	(cms)	(hrs)	(mm)
ID1= 3 ( 2130):	0.32	0.020	2.50	25.60
+ ID2= 2 ( 0211):	0.11	0.008	2.50	29.37
=====				
ID = 1 ( 2130):	0.43	0.028	2.50	26.54

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 2130)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 2130):	0.43	0.028	2.50	26.54
+ ID2= 2 ( 0212):	0.22	0.019	2.50	33.20
=====				
ID = 3 ( 2130):	0.64	0.047	2.50	28.79

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 2130)				
3 + 2 = 1				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 3 ( 2130):	0.64	0.047	2.50	28.79
+ ID2= 2 ( 0213):	0.68	0.053	2.50	30.52
=====				
ID = 1 ( 2130):	1.32	0.100	2.50	29.68

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR( 21301)				
IN= 2---> OUT= 1				
DT= 5.0 min				
OVERFLOW IS OFF				
	OUTFLOW	STORAGE	OUTFLOW	STORAGE
	(cms)	(ha.m.)	(cms)	(ha.m.)
	0.0000	0.0000	0.0160	0.0793
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 ( 2130)	1.320	0.100	2.50	29.68
OUTFLOW: ID= 1 ( 21301)	1.320	0.007	4.08	28.73

PEAK FLOW REDUCTION [Qout/Qin](%)= 6.57  
 TIME SHIFT OF PEAK FLOW (min)= 95.00  
 MAXIMUM STORAGE USED (ha.m.)= 0.0327



CALIB				
STANDHYD ( 2131)	Area	(ha)=	0.12	
ID= 1 DT= 5.0 min	Total Imp(%)=	72.00	Dir. Conn.(%)=	72.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.08	0.03	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	27.69	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	33.12	15.30	
over (min)	5.00	20.00	
Storage Coeff. (min)=	1.84 (ii)	16.80 (ii)	
Unit Hyd. Tpeak (min)=	5.00	20.00	
Unit Hyd. peak (cms)=	0.32	0.06	
			*TOTALS*
PEAK FLOW (cms)=	0.01	0.00	0.008 (iii)
TIME TO PEAK (hrs)=	2.50	2.67	2.50
RUNOFF VOLUME (mm)=	35.00	12.67	28.70
TOTAL RAINFALL (mm)=	36.00	36.00	36.00
RUNOFF COEFFICIENT =	0.97	0.35	0.80

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD ( 21302)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 21301):	1.32	0.007	4.08	28.73
+ ID2= 2 ( 2131):	0.12	0.008	2.50	28.70
=====				
ID = 3 ( 21302):	1.43	0.013	2.50	28.72

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 0005)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 0006):	4.11	0.054	2.50	28.37
+ ID2= 2 ( 21302):	1.43	0.013	2.50	28.72
=====				



ID = 3 ( 0005): 5.55 0.067 2.50 28.46

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| ADD HYD ( 0005) |
| 3 + 2 = 1 |
-----

```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 3 ( 0005):	5.55	0.067	2.50	28.46
+ ID2= 2 ( 0214):	1.03	0.035	2.58	13.66
=====				
ID = 1 ( 0005):	6.58	0.101	2.50	26.13

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

V V I SSSSS U U A L (v 6.0.2001)
V V I SS U U A A L
V V I SS U U AAAAA L
V V I SS U U A A L
VV I SSSSS UUUUU A A LLLLL

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000 TTTTT TTTTT H H Y Y M M 000 TM
O O T T H H Y Y MM MM O O
O O T T H H Y M M O O
000 T T H H Y M M 000

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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

Input filename: C:\Program Files (x86)\Visual OTTHYMO 6.0\V02\voin.dat

Output filename:

C:\Users\jliang\AppData\Local\Civica\XH5\becad37f-97fe-4a15-a3fd-f87dd2156d5f\7e2f9a6-4d96-41e8-a4b2-bacf6decdaab\scena

Summary filename:

C:\Users\jliang\AppData\Local\Civica\XH5\becad37f-97fe-4a15-a3fd-f87dd2156d5f\7e2f9a6-4d96-41e8-a4b2-bacf6decdaab\scena

DATE: 10-27-2021

TIME: 05:35:39

USER:



COMMENTS: \_\_\_\_\_

\*\*\*\*\*  
 \*\* SIMULATION : Run 02 \*\*  
 \*\*\*\*\*

READ STORM Ptotal= 47.81 mm	Filename: C:\Users\jliang\AppData\Local\Temp\907c1cff-ccb1-41c0-9867-a9890799f0d3\ca9c443b Comments: 5-Year 6-hour AES Storm
--------------------------------	---

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.25	0.96	1.75	16.25	3.25	6.69	4.75	0.96
0.50	0.96	2.00	16.25	3.50	6.69	5.00	0.96
0.75	0.96	2.25	43.98	3.75	3.82	5.25	0.96
1.00	0.96	2.50	43.98	4.00	3.82	5.50	0.96
1.25	5.74	2.75	12.43	4.25	1.91	5.75	0.96
1.50	5.74	3.00	12.43	4.50	1.91	6.00	0.96

CALIB NASHYD ( 2002) ID= 1 DT= 5.0 min	Area (ha)= 0.00    Curve Number (CN)= 85.0 Ia (mm)= 5.00    # of Linear Res.(N)= 3.00 U.H. Tp(hrs)= 0.20
--	--

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	0.96	1.583	16.25	3.083	6.69	4.58	0.96
0.167	0.96	1.667	16.25	3.167	6.69	4.67	0.96
0.250	0.96	1.750	16.25	3.250	6.69	4.75	0.96
0.333	0.96	1.833	16.25	3.333	6.69	4.83	0.96
0.417	0.96	1.917	16.25	3.417	6.69	4.92	0.96
0.500	0.96	2.000	16.25	3.500	6.69	5.00	0.96
0.583	0.96	2.083	43.98	3.583	3.82	5.08	0.96
0.667	0.96	2.167	43.98	3.667	3.82	5.17	0.96



0.750	0.96	2.250	43.98	3.750	3.82	5.25	0.96
0.833	0.96	2.333	43.98	3.833	3.82	5.33	0.96
0.917	0.96	2.417	43.98	3.917	3.82	5.42	0.96
1.000	0.96	2.500	43.98	4.000	3.82	5.50	0.96
1.083	5.74	2.583	12.43	4.083	1.91	5.58	0.96
1.167	5.74	2.667	12.43	4.167	1.91	5.67	0.96
1.250	5.74	2.750	12.43	4.250	1.91	5.75	0.96
1.333	5.74	2.833	12.43	4.333	1.91	5.83	0.96
1.417	5.74	2.917	12.43	4.417	1.91	5.92	0.96
1.500	5.74	3.000	12.43	4.500	1.91	6.00	0.96

Unit Hyd Qpeak (cms)= 0.001

PEAK FLOW (cms)= 0.000 (i)

TIME TO PEAK (hrs)= 2.500

RUNOFF VOLUME (mm)= 19.476

TOTAL RAINFALL (mm)= 47.810

RUNOFF COEFFICIENT = 0.407

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	
STANDHYD ( 0201)	Area (ha)= 0.73
ID= 1 DT= 5.0 min	Total Imp(%)= 80.00 Dir. Conn.(%)= 80.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.58	0.15	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	69.71	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	43.98	24.90	
over (min)	5.00	20.00	
Storage Coeff. (min)=	2.86 (ii)	15.17 (ii)	
Unit Hyd. Tpeak (min)=	5.00	20.00	
Unit Hyd. peak (cms)=	0.28	0.07	
			*TOTALS*
PEAK FLOW (cms)=	0.07	0.01	0.078 (iii)
TIME TO PEAK (hrs)=	2.50	2.67	2.50
RUNOFF VOLUME (mm)=	46.81	20.91	41.62
TOTAL RAINFALL (mm)=	47.81	47.81	47.81
RUNOFF COEFFICIENT =	0.98	0.44	0.87

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.





(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB |
| STANDHYD ( 0200) | Area (ha)= 0.46
| ID= 1 DT= 5.0 min | Total Imp(%)= 67.00 Dir. Conn.(%)= 67.00
-----

```

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.31	0.15	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	55.14	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	43.98	24.90	
over (min)	5.00	15.00	
Storage Coeff. (min)=	2.48 (ii)	14.79 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.29	0.08	
			*TOTALS*
PEAK FLOW (cms)=	0.04	0.01	0.045 (iii)
TIME TO PEAK (hrs)=	2.50	2.58	2.50
RUNOFF VOLUME (mm)=	46.81	20.91	38.24
TOTAL RAINFALL (mm)=	47.81	47.81	47.81
RUNOFF COEFFICIENT =	0.98	0.44	0.80

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| ADD HYD ( 2000) |
| 1 + 2 = 3 |
-----
          AREA    QPEAK    TPEAK    R.V.
          (ha)    (cms)    (hrs)    (mm)
ID1= 1 ( 0200):  0.46  0.045  2.50  38.24
+ ID2= 2 ( 0201):  0.73  0.078  2.50  41.62
=====
ID = 3 ( 2000):  1.18  0.122  2.50  40.32
-----

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| RESERVOIR( 20011) | OVERFLOW IS OFF
| IN= 2---> OUT= 1 |
| DT= 5.0 min |
-----
          OUTFLOW    STORAGE    |    OUTFLOW    STORAGE

```



-----	(cms)	(ha.m.)		(cms)	(ha.m.)
	0.0000	0.0000		0.0140	0.0709

	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 ( 2000)	1.185	0.122	2.50	40.32
OUTFLOW: ID= 1 ( 20011)	1.185	0.008	4.08	39.24

PEAK FLOW REDUCTION [Qout/Qin](%)= 6.46  
 TIME SHIFT OF PEAK FLOW (min)= 95.00  
 MAXIMUM STORAGE USED (ha.m.)= 0.0400

-----				
CALIB				
STANDHYD ( 2011)		Area (ha)= 0.08		
ID= 1 DT= 5.0 min		Total Imp(%)= 73.00	Dir. Conn.(%)= 73.00	

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	0.06	0.02	
Dep. Storage	(mm)=	1.00	5.00	
Average Slope	(%)=	1.00	2.00	
Length	(m)=	22.66	40.00	
Mannings n	=	0.013	0.250	
Max.Eff.Inten.(mm/hr)=		43.98	24.90	
over (min)		5.00	15.00	
Storage Coeff. (min)=		1.46 (ii)	13.76 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		0.33	0.08	
				*TOTALS*
PEAK FLOW (cms)=		0.01	0.00	0.008 (iii)
TIME TO PEAK (hrs)=		2.42	2.58	2.50
RUNOFF VOLUME (mm)=		46.81	20.91	39.76
TOTAL RAINFALL (mm)=		47.81	47.81	47.81
RUNOFF COEFFICIENT =		0.98	0.44	0.83

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----				
CALIB				
STANDHYD ( 2012)		Area (ha)= 0.03		
ID= 1 DT= 5.0 min		Total Imp(%)= 65.00	Dir. Conn.(%)= 65.00	

	IMPERVIOUS	PERVIOUS (i)
--	------------	--------------



Surface Area	(ha)=	0.02	0.01	
Dep. Storage	(mm)=	1.00	5.00	
Average Slope	(%)=	1.00	2.00	
Length	(m)=	14.61	40.00	
Mannings n	=	0.013	0.250	
Max.Eff.Inten.(mm/hr)=		43.98	24.90	
over (min)		5.00	15.00	
Storage Coeff. (min)=		1.12 (ii)	13.43 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		0.34	0.08	
				*TOTALS*
PEAK FLOW	(cms)=	0.00	0.00	0.003 (iii)
TIME TO PEAK	(hrs)=	2.25	2.58	2.50
RUNOFF VOLUME	(mm)=	46.81	20.91	36.38
TOTAL RAINFALL	(mm)=	47.81	47.81	47.81
RUNOFF COEFFICIENT	=	0.98	0.44	0.76

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0    Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----				
ADD HYD ( 2001)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 2001):	1.18	0.008	4.08	39.24
+ ID2= 2 ( 2002):	0.00	0.000	2.50	19.48
=====				
ID = 3 ( 2001):	1.19	0.008	4.08	39.15

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----				
ADD HYD ( 2001)				
3 + 2 = 1				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 3 ( 2001):	1.19	0.008	4.08	39.15
+ ID2= 2 ( 2011):	0.08	0.008	2.50	39.76
=====				
ID = 1 ( 2001):	1.27	0.014	2.50	39.19

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.



ADD HYD ( 2001)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 ( 2001):	1.27	0.014	2.50	39.19
+ ID2= 2 ( 2012):	0.03	0.003	2.50	36.38
=====				
ID = 3 ( 2001):	1.30	0.017	2.50	39.12

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB	Area (ha)=	Dir. Conn.(%)=
STANDHYD ( 0202)	0.94	
ID= 1 DT= 5.0 min	Total Imp(%)= 70.00	70.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.66	0.28	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	79.12	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	43.98	24.90	
over (min)	5.00	20.00	
Storage Coeff. (min)=	3.08 (ii)	15.39 (ii)	
Unit Hyd. Tpeak (min)=	5.00	20.00	
Unit Hyd. peak (cms)=	0.27	0.07	
			*TOTALS*
PEAK FLOW (cms)=	0.08	0.01	0.092 (iii)
TIME TO PEAK (hrs)=	2.50	2.67	2.50
RUNOFF VOLUME (mm)=	46.81	20.91	39.03
TOTAL RAINFALL (mm)=	47.81	47.81	47.81
RUNOFF COEFFICIENT =	0.98	0.44	0.82

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR( 2020)	OVERFLOW IS OFF			
IN= 2---> OUT= 1	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
DT= 5.0 min	0.0000	0.0000	0.0090	0.0561

AREA QPEAK TPEAK R.V.



	(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 ( 0202)	0.939	0.092	2.50	39.03
OUTFLOW: ID= 1 ( 2020)	0.939	0.005	4.42	37.35

PEAK FLOW REDUCTION [Qout/Qin](%)= 5.44  
 TIME SHIFT OF PEAK FLOW (min)=115.00  
 MAXIMUM STORAGE USED (ha.m.)= 0.0313

-----  
 | CALIB |  
 | STANDHYD ( 2021) | Area (ha)= 0.03  
 | ID= 1 DT= 5.0 min | Total Imp(%)= 65.00 Dir. Conn.(%)= 65.00  
 -----

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.02	0.01	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	14.83	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	43.98	24.90	
over (min)	5.00	15.00	
Storage Coeff. (min)=	1.13 (ii)	13.44 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.34	0.08	
			*TOTALS*
PEAK FLOW (cms)=	0.00	0.00	0.003 (iii)
TIME TO PEAK (hrs)=	2.25	2.58	2.50
RUNOFF VOLUME (mm)=	46.81	20.91	36.47
TOTAL RAINFALL (mm)=	47.81	47.81	47.81
RUNOFF COEFFICIENT =	0.98	0.44	0.76

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | CALIB |  
 | STANDHYD ( 2022) | Area (ha)= 0.07  
 | ID= 1 DT= 5.0 min | Total Imp(%)= 99.00 Dir. Conn.(%)= 99.00  
 -----

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	0.07	0.00
Dep. Storage (mm)=	1.00	5.00
Average Slope (%)=	1.00	2.00
Length (m)=	22.06	40.00



Mannings n	=	0.013	0.250	
Max.Eff.Inten.(mm/hr)=		43.98	25.95	
over (min)		5.00	5.00	
Storage Coeff. (min)=		1.43 (ii)	2.99 (ii)	
Unit Hyd. Tpeak (min)=		5.00	5.00	
Unit Hyd. peak (cms)=		0.33	0.28	
				*TOTALS*
PEAK FLOW (cms)=		0.01	0.00	0.009 (iii)
TIME TO PEAK (hrs)=		2.42	2.50	2.50
RUNOFF VOLUME (mm)=		46.81	20.91	46.55
TOTAL RAINFALL (mm)=		47.81	47.81	47.81
RUNOFF COEFFICIENT =		0.98	0.44	0.97

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0    Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----				
ADD HYD ( 20201)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 2020):	0.94	0.005	4.42	37.35
+ ID2= 2 ( 2021):	0.03	0.003	2.50	36.47
=====				
ID = 3 ( 20201):	0.97	0.006	2.50	37.32

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----				
ADD HYD ( 20201)				
3 + 2 = 1				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 3 ( 20201):	0.97	0.006	2.50	37.32
+ ID2= 2 ( 2022):	0.07	0.009	2.50	46.55
=====				
ID = 1 ( 20201):	1.04	0.015	2.50	37.96

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----				
ADD HYD ( 0002)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)



ID1= 1 ( 2001):	1.30	0.017	2.50	39.12
+ ID2= 2 ( 20201):	1.04	0.015	2.50	37.96
=====				
ID = 3 ( 0002):	2.34	0.032	2.50	38.60

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB				
STANDHYD ( 2071)	Area (ha)=	0.07		
ID= 1 DT= 5.0 min	Total Imp(%)=	74.00	Dir. Conn.(%)=	74.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.05	0.02	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	21.29	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	43.98	24.90	
over (min)	5.00	15.00	
Storage Coeff. (min)=	1.40 (ii)	13.71 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.33	0.08	
			*TOTALS*
PEAK FLOW (cms)=	0.01	0.00	0.007 (iii)
TIME TO PEAK (hrs)=	2.42	2.58	2.50
RUNOFF VOLUME (mm)=	46.81	20.91	40.02
TOTAL RAINFALL (mm)=	47.81	47.81	47.81
RUNOFF COEFFICIENT =	0.98	0.44	0.84

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB				
STANDHYD ( 0207)	Area (ha)=	0.56		
ID= 1 DT= 5.0 min	Total Imp(%)=	63.00	Dir. Conn.(%)=	63.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.35	0.21	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	61.05	40.00	
Mannings n =	0.013	0.250	



Max.Eff.Inten.(mm/hr)=	43.98	24.90	
over (min)	5.00	15.00	
Storage Coeff. (min)=	2.64 (ii)	14.95 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.29	0.08	
			*TOTALS*
PEAK FLOW (cms)=	0.04	0.01	0.053 (iii)
TIME TO PEAK (hrs)=	2.50	2.58	2.50
RUNOFF VOLUME (mm)=	46.81	20.91	37.21
TOTAL RAINFALL (mm)=	47.81	47.81	47.81
RUNOFF COEFFICIENT =	0.98	0.44	0.78

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0    Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR( 2070)		OVERFLOW IS OFF			
IN= 2---> OUT= 1					
DT= 5.0 min					
	OUTFLOW	STORAGE	OUTFLOW	STORAGE	
	(cms)	(ha.m.)	(cms)	(ha.m.)	
	0.0000	0.0000	0.0060	0.0318	
	AREA	QPEAK	TPEAK	R.V.	
	(ha)	(cms)	(hrs)	(mm)	
INFLOW : ID= 2 ( 0207)	0.559	0.053	2.50	37.21	
OUTFLOW: ID= 1 ( 2070)	0.559	0.003	4.25	34.81	

PEAK FLOW REDUCTION [Qout/Qin](%)= 6.21  
 TIME SHIFT OF PEAK FLOW (min)=105.00  
 MAXIMUM STORAGE USED (ha.m.)= 0.0174

ADD HYD ( 20701)					
1 + 2 = 3					
	AREA	QPEAK	TPEAK	R.V.	
	(ha)	(cms)	(hrs)	(mm)	
ID1= 1 ( 2070):	0.56	0.003	4.25	34.81	
+ ID2= 2 ( 2071):	0.07	0.007	2.50	40.02	
=====					
ID = 3 ( 20701):	0.63	0.009	2.50	35.37	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB





| STANDHYD ( 0204) | Area (ha)= 0.13  
 | ID= 1 DT= 5.0 min | Total Imp(%)= 75.00 Dir. Conn.(%)= 75.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.10	0.03	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	29.10	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	43.98	24.90	
over (min)	5.00	15.00	
Storage Coeff. (min)=	1.69 (ii)	14.00 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.32	0.08	
			*TOTALS*
PEAK FLOW (cms)=	0.01	0.00	0.013 (iii)
TIME TO PEAK (hrs)=	2.42	2.58	2.50
RUNOFF VOLUME (mm)=	46.81	20.91	40.28
TOTAL RAINFALL (mm)=	47.81	47.81	47.81
RUNOFF COEFFICIENT =	0.98	0.44	0.84

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| CALIB |  
 | STANDHYD ( 0208) | Area (ha)= 0.04  
 | ID= 1 DT= 5.0 min | Total Imp(%)= 75.00 Dir. Conn.(%)= 75.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.03	0.01	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	16.93	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	43.98	24.90	
over (min)	5.00	15.00	
Storage Coeff. (min)=	1.22 (ii)	13.53 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.33	0.08	
			*TOTALS*
PEAK FLOW (cms)=	0.00	0.00	0.004 (iii)
TIME TO PEAK (hrs)=	2.42	2.58	2.50
RUNOFF VOLUME (mm)=	46.81	20.91	40.29



TOTAL RAINFALL (mm)=	47.81	47.81	47.81
RUNOFF COEFFICIENT =	0.98	0.44	0.84

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD ( 0205)	Area (ha)=	0.22	
ID= 1 DT= 5.0 min	Total Imp(%)=	99.00	Dir. Conn.(%)= 99.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.22	0.00	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	38.38	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	43.98	25.95	
over (min)	5.00	5.00	
Storage Coeff. (min)=	2.00 (ii)	3.56 (ii)	
Unit Hyd. Tpeak (min)=	5.00	5.00	
Unit Hyd. peak (cms)=	0.31	0.26	
			*TOTALS*
PEAK FLOW (cms)=	0.03	0.00	0.027 (iii)
TIME TO PEAK (hrs)=	2.50	2.50	2.50
RUNOFF VOLUME (mm)=	46.81	20.91	46.54
TOTAL RAINFALL (mm)=	47.81	47.81	47.81
RUNOFF COEFFICIENT =	0.98	0.44	0.97

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD ( 0206)	Area (ha)=	0.51	
ID= 1 DT= 5.0 min	Total Imp(%)=	88.00	Dir. Conn.(%)= 88.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.45	0.06	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	



Length	(m)=	58.54	40.00	
Mannings n	=	0.013	0.250	
Max.Eff.Inten.(mm/hr)=		43.98	25.95	
over (min)		5.00	10.00	
Storage Coeff. (min)=		2.57 (ii)	6.99 (ii)	
Unit Hyd. Tpeak (min)=		5.00	10.00	
Unit Hyd. peak (cms)=		0.29	0.14	
				*TOTALS*
PEAK FLOW (cms)=		0.06	0.00	0.059 (iii)
TIME TO PEAK (hrs)=		2.50	2.50	2.50
RUNOFF VOLUME (mm)=		46.81	20.91	43.70
TOTAL RAINFALL (mm)=		47.81	47.81	47.81
RUNOFF COEFFICIENT =		0.98	0.44	0.91

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----				
ADD HYD ( 2060)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 0204):	0.13	0.013	2.50	40.28
+ ID2= 2 ( 0205):	0.22	0.027	2.50	46.54
=====				
ID = 3 ( 2060):	0.35	0.040	2.50	44.26

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----				
ADD HYD ( 2060)				
3 + 2 = 1				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 3 ( 2060):	0.35	0.040	2.50	44.26
+ ID2= 2 ( 0206):	0.51	0.059	2.50	43.70
=====				
ID = 1 ( 2060):	0.86	0.099	2.50	43.92

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----				
ADD HYD ( 2060)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.



	(ha)	(cms)	(hrs)	(mm)
----- ID1= 1 ( 2060):	0.86	0.099	2.50	43.92
+ ID2= 2 ( 0208):	0.04	0.004	2.50	40.29
=====				
ID = 3 ( 2060):	0.90	0.104	2.50	43.75

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR( 20601)	OVERFLOW IS OFF			
IN= 2---> OUT= 1				
DT= 5.0 min	OUTFLOW	STORAGE	OUTFLOW	STORAGE
	(cms)	(ha.m.)	(cms)	(ha.m.)
-----	0.0000	0.0000	0.0120	0.0571

	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 ( 2060)	0.905	0.104	2.50	43.75
OUTFLOW: ID= 1 ( 20601)	0.905	0.007	4.08	42.42

PEAK FLOW REDUCTION [Qout/Qin](%)= 6.68  
 TIME SHIFT OF PEAK FLOW (min)= 95.00  
 MAXIMUM STORAGE USED (ha.m.)= 0.0330

CALIB			
STANDHYD ( 2061)	Area (ha)=	0.05	
ID= 1 DT= 5.0 min	Total Imp(%)=	82.00	Dir. Conn.(%)= 82.00
-----			

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.04	0.01	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	17.32	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	43.98	24.90	
over (min)	5.00	15.00	
Storage Coeff. (min)=	1.24 (ii)	13.55 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.33	0.08	
			*TOTALS*
PEAK FLOW (cms)=	0.00	0.00	0.005 (iii)
TIME TO PEAK (hrs)=	2.42	2.58	2.50
RUNOFF VOLUME (mm)=	46.81	20.91	42.11
TOTAL RAINFALL (mm)=	47.81	47.81	47.81
RUNOFF COEFFICIENT =	0.98	0.44	0.88

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:



- CN\* = 85.0    Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| ADD HYD ( 20602) |
| 1 + 2 = 3       |
-----
                AREA    QPEAK    TPEAK    R.V.
                (ha)    (cms)    (hrs)    (mm)
ID1= 1 ( 20601):  0.90    0.007    4.08    42.42
+ ID2= 2 ( 2061):  0.05    0.005    2.50    42.11
=====
ID = 3 ( 20602):  0.95    0.010    2.50    42.40

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| ADD HYD ( 0003) |
| 1 + 2 = 3       |
-----
                AREA    QPEAK    TPEAK    R.V.
                (ha)    (cms)    (hrs)    (mm)
ID1= 1 ( 0002):  2.34    0.032    2.50    38.60
+ ID2= 2 ( 20602):  0.95    0.010    2.50    42.40
=====
ID = 3 ( 0003):  3.29    0.042    2.50    39.70

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| ADD HYD ( 0003) |
| 3 + 2 = 1       |
-----
                AREA    QPEAK    TPEAK    R.V.
                (ha)    (cms)    (hrs)    (mm)
ID1= 3 ( 0003):  3.29    0.042    2.50    39.70
+ ID2= 2 ( 20701):  0.63    0.009    2.50    35.37
=====
ID = 1 ( 0003):  3.92    0.051    2.50    39.01

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| CALIB          |
| STANDHYD ( 2201) |
| ID= 1 DT= 5.0 min |
-----
Area    (ha)=    0.19
Total Imp(%)=  99.00   Dir. Conn.(%)=  99.00

```

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	0.19	0.00
Dep. Storage (mm)=	1.00	5.00



Average Slope (%)=	1.00	2.00	
Length (m)=	35.50	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	43.98	25.95	
over (min)	5.00	5.00	
Storage Coeff. (min)=	1.91 (ii)	3.47 (ii)	
Unit Hyd. Tpeak (min)=	5.00	5.00	
Unit Hyd. peak (cms)=	0.32	0.26	
			*TOTALS*
PEAK FLOW (cms)=	0.02	0.00	0.023 (iii)
TIME TO PEAK (hrs)=	2.50	2.50	2.50
RUNOFF VOLUME (mm)=	46.81	20.91	46.54
TOTAL RAINFALL (mm)=	47.81	47.81	47.81
RUNOFF COEFFICIENT =	0.98	0.44	0.97

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD ( 0006)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 0003):	3.92	0.051	2.50	39.01
+ ID2= 2 ( 2201):	0.19	0.023	2.50	46.54
=====				
ID = 3 ( 0006):	4.11	0.074	2.50	39.35

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB			
NASHYD ( 2141)	Area (ha)=	0.67	Curve Number (CN)= 85.0
ID= 1 DT= 5.0 min	Ia (mm)=	5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)=	0.20	

Unit Hyd Qpeak (cms)= 0.128

PEAK FLOW (cms)= 0.038 (i)

TIME TO PEAK (hrs)= 2.500

RUNOFF VOLUME (mm)= 20.872

TOTAL RAINFALL (mm)= 47.810

RUNOFF COEFFICIENT = 0.437

- (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.



-----  
 -----  
 | CALIB |  
 | STANDHYD ( 2142) | Area (ha)= 0.36  
 | ID= 1 DT= 5.0 min | Total Imp(%)= 20.00 Dir. Conn.(%)= 5.00  
 -----

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.07	0.29	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	49.14	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	43.98	32.70	
over (min)	5.00	15.00	
Storage Coeff. (min)=	2.32 (ii)	13.35 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.30	0.08	
			*TOTALS*
PEAK FLOW (cms)=	0.00	0.02	0.022 (iii)
TIME TO PEAK (hrs)=	2.50	2.58	2.50
RUNOFF VOLUME (mm)=	46.81	23.37	24.52
TOTAL RAINFALL (mm)=	47.81	47.81	47.81
RUNOFF COEFFICIENT =	0.98	0.49	0.51

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 -----  
 | ADD HYD ( 0214) |  
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 ( 2141):	0.67	0.038	2.50	20.87
+ ID2= 2 ( 2142):	0.36	0.022	2.50	24.52
=====				
ID = 3 ( 0214):	1.03	0.060	2.50	22.15

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----  
 -----  
 | CALIB |  
 | STANDHYD ( 0210) | Area (ha)= 0.14  
 | ID= 1 DT= 5.0 min | Total Imp(%)= 92.00 Dir. Conn.(%)= 92.00  
 -----



	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.13	0.01	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	30.44	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	43.98	25.95	
over (min)	5.00	10.00	
Storage Coeff. (min)=	1.74 (ii)	5.43 (ii)	
Unit Hyd. Tpeak (min)=	5.00	10.00	
Unit Hyd. peak (cms)=	0.32	0.16	
			*TOTALS*
PEAK FLOW (cms)=	0.02	0.00	0.016 (iii)
TIME TO PEAK (hrs)=	2.50	2.50	2.50
RUNOFF VOLUME (mm)=	46.81	20.91	44.73
TOTAL RAINFALL (mm)=	47.81	47.81	47.81
RUNOFF COEFFICIENT =	0.98	0.44	0.94

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0    Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB		STANDHYD ( 0211)	
ID= 1	DT= 5.0 min	Area (ha)= 0.11	Total Imp(%)= 75.00    Dir. Conn.(%)= 75.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.08	0.03	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	26.58	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	43.98	24.90	
over (min)	5.00	15.00	
Storage Coeff. (min)=	1.60 (ii)	13.91 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.32	0.08	
			*TOTALS*
PEAK FLOW (cms)=	0.01	0.00	0.011 (iii)
TIME TO PEAK (hrs)=	2.50	2.58	2.50
RUNOFF VOLUME (mm)=	46.81	20.91	40.28
TOTAL RAINFALL (mm)=	47.81	47.81	47.81
RUNOFF COEFFICIENT =	0.98	0.44	0.84





- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 -----  

CALIB			
STANDHYD ( 0203)	Area (ha)=	0.18	
ID= 1 DT= 5.0 min	Total Imp(%)=	32.00	Dir. Conn.(%)= 32.00

 -----  
 -----

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.06	0.12	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	34.74	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	43.98	24.90	
over (min)	5.00	15.00	
Storage Coeff. (min)=	1.88 (ii)	14.19 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.32	0.08	
			*TOTALS*
PEAK FLOW (cms)=	0.01	0.01	0.013 (iii)
TIME TO PEAK (hrs)=	2.50	2.58	2.50
RUNOFF VOLUME (mm)=	46.81	20.91	29.15
TOTAL RAINFALL (mm)=	47.81	47.81	47.81
RUNOFF COEFFICIENT =	0.98	0.44	0.61

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 -----  

CALIB			
STANDHYD ( 0213)	Area (ha)=	0.68	
ID= 1 DT= 5.0 min	Total Imp(%)=	80.00	Dir. Conn.(%)= 80.00

 -----  
 -----

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.54	0.14	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	67.18	40.00	
Mannings n =	0.013	0.250	



Max.Eff.Inten.(mm/hr)=	43.98	24.90	
over (min)	5.00	20.00	
Storage Coeff. (min)=	2.80 (ii)	15.10 (ii)	
Unit Hyd. Tpeak (min)=	5.00	20.00	
Unit Hyd. peak (cms)=	0.28	0.07	
			*TOTALS*
PEAK FLOW (cms)=	0.07	0.01	0.072 (iii)
TIME TO PEAK (hrs)=	2.50	2.67	2.50
RUNOFF VOLUME (mm)=	46.81	20.91	41.62
TOTAL RAINFALL (mm)=	47.81	47.81	47.81
RUNOFF COEFFICIENT =	0.98	0.44	0.87

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0    Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD ( 0212)	Area (ha)=	0.22	
ID= 1 DT= 5.0 min	Total Imp(%)=	92.00	Dir. Conn.(%)= 92.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.20	0.02	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	38.04	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	43.98	25.95	
over (min)	5.00	10.00	
Storage Coeff. (min)=	1.99 (ii)	5.68 (ii)	
Unit Hyd. Tpeak (min)=	5.00	10.00	
Unit Hyd. peak (cms)=	0.31	0.15	
			*TOTALS*
PEAK FLOW (cms)=	0.02	0.00	0.026 (iii)
TIME TO PEAK (hrs)=	2.50	2.50	2.50
RUNOFF VOLUME (mm)=	46.81	20.91	44.73
TOTAL RAINFALL (mm)=	47.81	47.81	47.81
RUNOFF COEFFICIENT =	0.98	0.44	0.94

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0    Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.



-----				
ADD HYD ( 2130)				
1 + 2 = 3				
-----				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 0203):	0.18	0.013	2.50	29.15
+ ID2= 2 ( 0210):	0.14	0.016	2.50	44.73
=====				
ID = 3 ( 2130):	0.32	0.030	2.50	35.92

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----

-----				
ADD HYD ( 2130)				
3 + 2 = 1				
-----				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 3 ( 2130):	0.32	0.030	2.50	35.92
+ ID2= 2 ( 0211):	0.11	0.011	2.50	40.28
=====				
ID = 1 ( 2130):	0.43	0.041	2.50	37.00

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----

-----				
ADD HYD ( 2130)				
1 + 2 = 3				
-----				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 2130):	0.43	0.041	2.50	37.00
+ ID2= 2 ( 0212):	0.22	0.026	2.50	44.73
=====				
ID = 3 ( 2130):	0.64	0.066	2.50	39.61

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----

-----				
ADD HYD ( 2130)				
3 + 2 = 1				
-----				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 3 ( 2130):	0.64	0.066	2.50	39.61
+ ID2= 2 ( 0213):	0.68	0.072	2.50	41.62
=====				
ID = 1 ( 2130):	1.32	0.138	2.50	40.64

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----

| RESERVOIR( 21301) |      OVERFLOW IS OFF



| IN= 2---> OUT= 1 |  
| DT= 5.0 min |

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
0.0000	0.0000	0.0160	0.0793

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 ( 2130)	1.320	0.138	2.50	40.64
OUTFLOW: ID= 1 ( 21301)	1.320	0.009	4.08	39.69

PEAK FLOW REDUCTION [Qout/Qin](%)= 6.54  
 TIME SHIFT OF PEAK FLOW (min)= 95.00  
 MAXIMUM STORAGE USED (ha.m.)= 0.0448

| CALIB  
| STANDHYD ( 2131)  
| ID= 1 DT= 5.0 min |

Area (ha)= 0.12  
 Total Imp(%)= 72.00 Dir. Conn.(%)= 72.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	0.08	0.03
Dep. Storage (mm)=	1.00	5.00
Average Slope (%)=	1.00	2.00
Length (m)=	27.69	40.00
Mannings n =	0.013	0.250

Max.Eff.Inten.(mm/hr)=	43.98	24.90
over (min)	5.00	15.00
Storage Coeff. (min)=	1.64 (ii)	13.95 (ii)
Unit Hyd. Tpeak (min)=	5.00	15.00
Unit Hyd. peak (cms)=	0.32	0.08

\*TOTALS\*

PEAK FLOW (cms)=	0.01	0.00	0.012 (iii)
TIME TO PEAK (hrs)=	2.50	2.58	2.50
RUNOFF VOLUME (mm)=	46.81	20.91	39.50
TOTAL RAINFALL (mm)=	47.81	47.81	47.81
RUNOFF COEFFICIENT =	0.98	0.44	0.83

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ADD HYD ( 21302)  
| 1 + 2 = 3 |

AREA	QPEAK	TPEAK	R.V.
------	-------	-------	------



	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 21301):	1.32	0.009	4.08	39.69
+ ID2= 2 ( 2131):	0.12	0.012	2.50	39.50
=====				
ID = 3 ( 21302):	1.43	0.018	2.50	39.67

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 0005)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 0006):	4.11	0.074	2.50	39.35
+ ID2= 2 ( 21302):	1.43	0.018	2.50	39.67
=====				
ID = 3 ( 0005):	5.55	0.092	2.50	39.44

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 0005)				
3 + 2 = 1				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 3 ( 0005):	5.55	0.092	2.50	39.44
+ ID2= 2 ( 0214):	1.03	0.060	2.50	22.15
=====				
ID = 1 ( 0005):	6.58	0.152	2.50	36.72

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

FINISH

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V	V	I	SSSSS	U	U	A	L				(v 6.0.2001)
V	V	I	SS	U	U	A A	L				
V	V	I	SS	U	U	AAAAA	L				
V	V	I	SS	U	U	A A	L				
VV		I	SSSSS	UUUUU	A	A	LLLLL				
000	TTTTT	TTTTT	H	H	Y	Y	M	M	000	TM	
0	0	T	T	H	H	Y Y	MM	MM	0	0	
0	0	T	T	H	H	Y	M	M	0	0	
000	T	T	H	H	Y	M	M	000			



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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

Input filename: C:\Program Files (x86)\Visual OTTHYMO 6.0\V02\voin.dat

Output filename:

C:\Users\jliang\AppData\Local\Civica\XH5\becad37f-97fe-4a15-a3fd-f87dd2156d5f\47ff4aa2-0856-460f-8a24-166b938b65a3\scena

Summary filename:

C:\Users\jliang\AppData\Local\Civica\XH5\becad37f-97fe-4a15-a3fd-f87dd2156d5f\47ff4aa2-0856-460f-8a24-166b938b65a3\scena

DATE: 10-27-2021

TIME: 05:35:38

USER:

COMMENTS: \_\_\_\_\_

-----  
 \*\*\*\*\*  
 \*\* SIMULATION : Run 03 \*\*  
 \*\*\*\*\*

READ STORM	Filename: C:\Users\jliang\AppData\Local\Temp\907c1cff-ccb1-41c0-9867-a9890799f0d3\8b3892d6
Ptotal= 55.69 mm	Comments: 10-Year 6-hour AES Storm

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.25	1.11	1.75	18.94	3.25	7.80	4.75	1.11
0.50	1.11	2.00	18.94	3.50	7.80	5.00	1.11
0.75	1.11	2.25	51.24	3.75	4.46	5.25	1.11
1.00	1.11	2.50	51.24	4.00	4.46	5.50	1.11
1.25	6.68	2.75	14.48	4.25	2.23	5.75	1.11
1.50	6.68	3.00	14.48	4.50	2.23	6.00	1.11



CALIB			
NASHYD ( 2002)	Area (ha)=	0.00	Curve Number (CN)= 85.0
ID= 1 DT= 5.0 min	Ia (mm)=	5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)=	0.20	

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	1.11	1.583	18.94	3.083	7.80	4.58	1.11
0.167	1.11	1.667	18.94	3.167	7.80	4.67	1.11
0.250	1.11	1.750	18.94	3.250	7.80	4.75	1.11
0.333	1.11	1.833	18.94	3.333	7.80	4.83	1.11
0.417	1.11	1.917	18.94	3.417	7.80	4.92	1.11
0.500	1.11	2.000	18.94	3.500	7.80	5.00	1.11
0.583	1.11	2.083	51.24	3.583	4.46	5.08	1.11
0.667	1.11	2.167	51.24	3.667	4.46	5.17	1.11
0.750	1.11	2.250	51.24	3.750	4.46	5.25	1.11
0.833	1.11	2.333	51.24	3.833	4.46	5.33	1.11
0.917	1.11	2.417	51.24	3.917	4.46	5.42	1.11
1.000	1.11	2.500	51.24	4.000	4.46	5.50	1.11
1.083	6.68	2.583	14.48	4.083	2.23	5.58	1.11
1.167	6.68	2.667	14.48	4.167	2.23	5.67	1.11
1.250	6.68	2.750	14.48	4.250	2.23	5.75	1.11
1.333	6.68	2.833	14.48	4.333	2.23	5.83	1.11
1.417	6.68	2.917	14.48	4.417	2.23	5.92	1.11
1.500	6.68	3.000	14.48	4.500	2.23	6.00	1.11

Unit Hyd Qpeak (cms)= 0.001

PEAK FLOW (cms)= 0.000 (i)

TIME TO PEAK (hrs)= 2.500

RUNOFF VOLUME (mm)= 26.005

TOTAL RAINFALL (mm)= 55.690

RUNOFF COEFFICIENT = 0.467

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD ( 0201)	Area (ha)=	0.73	
ID= 1 DT= 5.0 min	Total Imp(%)=	80.00	Dir. Conn.(%)= 80.00

Surface Area (ha)= IMPERVIOUS 0.58 PERVIOUS (i) 0.15



Dep. Storage	(mm)=	1.00	5.00	
Average Slope	(%)=	1.00	2.00	
Length	(m)=	69.71	40.00	
Mannings n	=	0.013	0.250	
Max.Eff.Inten.(mm/hr)=		51.24	31.75	
over (min)		5.00	15.00	
Storage Coeff. (min)=		2.69 (ii)	13.86 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		0.29	0.08	
				*TOTALS*
PEAK FLOW	(cms)=	0.08	0.01	0.092 (iii)
TIME TO PEAK	(hrs)=	2.50	2.58	2.50
RUNOFF VOLUME	(mm)=	54.69	26.90	49.12
TOTAL RAINFALL	(mm)=	55.69	55.69	55.69
RUNOFF COEFFICIENT	=	0.98	0.48	0.88

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD ( 0200)	Area (ha)=	0.46	
ID= 1 DT= 5.0 min	Total Imp(%)=	67.00	Dir. Conn.(%)= 67.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	0.31	0.15	
Dep. Storage	(mm)=	1.00	5.00	
Average Slope	(%)=	1.00	2.00	
Length	(m)=	55.14	40.00	
Mannings n	=	0.013	0.250	
Max.Eff.Inten.(mm/hr)=		51.24	31.75	
over (min)		5.00	15.00	
Storage Coeff. (min)=		2.34 (ii)	13.50 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		0.30	0.08	
				*TOTALS*
PEAK FLOW	(cms)=	0.04	0.01	0.053 (iii)
TIME TO PEAK	(hrs)=	2.50	2.58	2.50
RUNOFF VOLUME	(mm)=	54.69	26.90	45.50
TOTAL RAINFALL	(mm)=	55.69	55.69	55.69
RUNOFF COEFFICIENT	=	0.98	0.48	0.82

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)





- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD ( 2000)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 ( 0200):	0.46	0.053	2.50	45.50
+ ID2= 2 ( 0201):	0.73	0.092	2.50	49.12
=====				
ID = 3 ( 2000):	1.18	0.146	2.50	47.73

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR( 20011)	OVERFLOW IS OFF			
IN= 2---> OUT= 1	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
DT= 5.0 min	0.0000	0.0000	0.0140	0.0709
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 ( 2000)	1.185	0.146	2.50	47.73
OUTFLOW: ID= 1 ( 20011)	1.185	0.009	4.08	46.65
PEAK FLOW REDUCTION [Qout/Qin](%)= 6.41				
TIME SHIFT OF PEAK FLOW (min)= 95.00				
MAXIMUM STORAGE USED (ha.m.)= 0.0473				

CALIB	Area (ha)=	0.08
STANDHYD ( 2011)	Total Imp(%)=	73.00
ID= 1 DT= 5.0 min	Dir. Conn.(%)=	73.00
	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	0.06	0.02
Dep. Storage (mm)=	1.00	5.00
Average Slope (%)=	1.00	2.00
Length (m)=	22.66	40.00
Mannings n =	0.013	0.250
Max.Eff.Inten.(mm/hr)=	51.24	31.75
over (min)	5.00	15.00
Storage Coeff. (min)=	1.37 (ii)	12.54 (ii)
Unit Hyd. Tpeak (min)=	5.00	15.00



Unit Hyd. peak (cms)=	0.33	0.08	
			*TOTALS*
PEAK FLOW (cms)=	0.01	0.00	0.009 (iii)
TIME TO PEAK (hrs)=	2.42	2.58	2.50
RUNOFF VOLUME (mm)=	54.69	26.90	47.12
TOTAL RAINFALL (mm)=	55.69	55.69	55.69
RUNOFF COEFFICIENT =	0.98	0.48	0.85

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD ( 2012)	Area (ha)=	0.03	
ID= 1 DT= 5.0 min	Total Imp(%)=	65.00	Dir. Conn.(%)= 65.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.02	0.01	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	14.61	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	51.24	31.75	
over (min)	5.00	15.00	
Storage Coeff. (min)=	1.05 (ii)	12.22 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.34	0.09	
			*TOTALS*
PEAK FLOW (cms)=	0.00	0.00	0.004 (iii)
TIME TO PEAK (hrs)=	2.25	2.58	2.50
RUNOFF VOLUME (mm)=	54.69	26.90	43.67
TOTAL RAINFALL (mm)=	55.69	55.69	55.69
RUNOFF COEFFICIENT =	0.98	0.48	0.78

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD ( 2001)				
1 + 2 = 3	AREA	QPEAK	TPEAK	R.V.



	(ha)	(cms)	(hrs)	(mm)
-----				
ID1= 1 ( 20011):	1.18	0.009	4.08	46.65
+ ID2= 2 ( 2002):	0.00	0.000	2.50	26.00
=====				
ID = 3 ( 2001):	1.19	0.009	4.08	46.56

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 2001)				
3 + 2 = 1				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
-----				
ID1= 3 ( 2001):	1.19	0.009	4.08	46.56
+ ID2= 2 ( 2011):	0.08	0.009	2.50	47.12
=====				
ID = 1 ( 2001):	1.27	0.016	2.50	46.59

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 2001)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
-----				
ID1= 1 ( 2001):	1.27	0.016	2.50	46.59
+ ID2= 2 ( 2012):	0.03	0.004	2.50	43.67
=====				
ID = 3 ( 2001):	1.30	0.020	2.50	46.52

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB				
STANDHYD ( 0202)				
ID= 1 DT= 5.0 min				
-----				
Area	(ha)=	0.94		
Total Imp(%)=		70.00	Dir. Conn.(%)=	70.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	0.66	0.28
Dep. Storage (mm)=	1.00	5.00
Average Slope (%)=	1.00	2.00
Length (m)=	79.12	40.00
Mannings n =	0.013	0.250
Max.Eff.Inten.(mm/hr)=	51.24	31.75
over (min)	5.00	15.00
Storage Coeff. (min)=	2.90 (ii)	14.07 (ii)
Unit Hyd. Tpeak (min)=	5.00	15.00
Unit Hyd. peak (cms)=	0.28	0.08

\*TOTALS\*



PEAK FLOW	(cms)=	0.09	0.02	0.112 (iii)
TIME TO PEAK	(hrs)=	2.50	2.58	2.50
RUNOFF VOLUME	(mm)=	54.69	26.90	46.34
TOTAL RAINFALL	(mm)=	55.69	55.69	55.69
RUNOFF COEFFICIENT	=	0.98	0.48	0.83

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR( 2020)	OVERFLOW IS OFF			
IN= 2---> OUT= 1				
DT= 5.0 min				
	OUTFLOW	STORAGE	OUTFLOW	STORAGE
	(cms)	(ha.m.)	(cms)	(ha.m.)
	0.0000	0.0000	0.0090	0.0561

	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 ( 0202)	0.939	0.112	2.50	46.34
OUTFLOW: ID= 1 ( 2020)	0.939	0.006	4.33	44.66

PEAK FLOW REDUCTION [Qout/Qin](%)= 5.35  
 TIME SHIFT OF PEAK FLOW (min)=110.00  
 MAXIMUM STORAGE USED (ha.m.)= 0.0372

CALIB			
STANDHYD ( 2021)	Area (ha)=	0.03	
ID= 1 DT= 5.0 min	Total Imp(%)=	65.00	Dir. Conn.(%)= 65.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)= 0.02	0.01	
Dep. Storage	(mm)= 1.00	5.00	
Average Slope	(%)= 1.00	2.00	
Length	(m)= 14.83	40.00	
Mannings n	= 0.013	0.250	
Max.Eff.Inten.(mm/hr)=	51.24	31.75	
over (min)	5.00	15.00	
Storage Coeff. (min)=	1.06 (ii)	12.23 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.34	0.09	
			*TOTALS*
PEAK FLOW	(cms)= 0.00	0.00	0.004 (iii)
TIME TO PEAK	(hrs)= 2.25	2.58	2.50



RUNOFF VOLUME (mm)=	54.69	26.90	43.76
TOTAL RAINFALL (mm)=	55.69	55.69	55.69
RUNOFF COEFFICIENT =	0.98	0.48	0.79

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD ( 2022)	Area (ha)=	0.07	
ID= 1 DT= 5.0 min	Total Imp(%)=	99.00	Dir. Conn.(%)= 99.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.07	0.00	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	22.06	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	51.24	32.92	
over (min)	5.00	5.00	
Storage Coeff. (min)=	1.35 (ii)	2.82 (ii)	
Unit Hyd. Tpeak (min)=	5.00	5.00	
Unit Hyd. peak (cms)=	0.33	0.28	
			*TOTALS*
PEAK FLOW (cms)=	0.01	0.00	0.010 (iii)
TIME TO PEAK (hrs)=	2.50	2.50	2.50
RUNOFF VOLUME (mm)=	54.69	26.90	54.41
TOTAL RAINFALL (mm)=	55.69	55.69	55.69
RUNOFF COEFFICIENT =	0.98	0.48	0.98

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD ( 20201)				
1 + 2 = 3	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 2020):	0.94	0.006	4.33	44.66
+ ID2= 2 ( 2021):	0.03	0.004	2.50	43.76



ID = 3 ( 20201): 0.97 0.008 2.50 44.63

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| ADD HYD ( 20201) |
| 3 + 2 = 1 |
-----
          AREA      QPEAK      TPEAK      R.V.
          (ha)      (cms)      (hrs)      (mm)
ID1= 3 ( 20201):  0.97  0.008  2.50  44.63
+ ID2= 2 ( 2022):  0.07  0.010  2.50  54.41
=====
ID = 1 ( 20201):  1.04  0.018  2.50  45.32

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| ADD HYD ( 0002) |
| 1 + 2 = 3 |
-----
          AREA      QPEAK      TPEAK      R.V.
          (ha)      (cms)      (hrs)      (mm)
ID1= 1 ( 2001):  1.30  0.020  2.50  46.52
+ ID2= 2 ( 20201):  1.04  0.018  2.50  45.32
=====
ID = 3 ( 0002):  2.34  0.038  2.50  45.98

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| CALIB |
| STANDHYD ( 2071) |
| ID= 1 DT= 5.0 min |
-----
Area (ha)= 0.07
Total Imp(%)= 74.00 Dir. Conn.(%)= 74.00

```

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.05	0.02	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	21.29	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	51.24	31.75	
over (min)	5.00	15.00	
Storage Coeff. (min)=	1.32 (ii)	12.49 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.33	0.08	
			*TOTALS*
PEAK FLOW (cms)=	0.01	0.00	0.008 (iii)
TIME TO PEAK (hrs)=	2.42	2.58	2.50
RUNOFF VOLUME (mm)=	54.69	26.90	47.40
TOTAL RAINFALL (mm)=	55.69	55.69	55.69



RUNOFF COEFFICIENT = 0.98 0.48 0.85

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | CALIB |  
 | STANDHYD ( 0207) | Area (ha)= 0.56  
 | ID= 1 DT= 5.0 min | Total Imp(%)= 63.00 Dir. Conn.(%)= 63.00  
 -----

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.35	0.21	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	61.05	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	51.24	31.75	
over (min)	5.00	15.00	
Storage Coeff. (min)=	2.48 (ii)	13.65 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.29	0.08	
			*TOTALS*
PEAK FLOW (cms)=	0.05	0.01	0.064 (iii)
TIME TO PEAK (hrs)=	2.50	2.58	2.50
RUNOFF VOLUME (mm)=	54.69	26.90	44.39
TOTAL RAINFALL (mm)=	55.69	55.69	55.69
RUNOFF COEFFICIENT =	0.98	0.48	0.80

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | RESERVOIR( 2070) | OVERFLOW IS OFF  
 | IN= 2---> OUT= 1 |  
DT= 5.0 min

OUTFLOW	STORAGE	OUTFLOW	STORAGE
(cms)	(ha.m.)	(cms)	(ha.m.)
0.0000	0.0000	0.0060	0.0318

	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 ( 0207)	0.559	0.064	2.50	44.39



OUTFLOW: ID= 1 ( 2070) 0.559 0.004 4.25 41.98

PEAK FLOW REDUCTION [Qout/Qin](%)= 6.18  
 TIME SHIFT OF PEAK FLOW (min)=105.00  
 MAXIMUM STORAGE USED (ha.m.)= 0.0208

-----  
 -----  
 | ADD HYD ( 20701) |  
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 ( 2070):	0.56	0.004	4.25	41.98
+ ID2= 2 ( 2071):	0.07	0.008	2.50	47.40
=====				
ID = 3 ( 20701):	0.63	0.011	2.50	42.57

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----  
 -----  
 | CALIB |  
 | STANDHYD ( 0204) |  
ID= 1 DT= 5.0 min

Area (ha)=	0.13
Total Imp(%)=	75.00
Dir. Conn.(%)=	75.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.10	0.03	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	29.10	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	51.24	31.75	
over (min)	5.00	15.00	
Storage Coeff. (min)=	1.59 (ii)	12.76 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.33	0.08	
			*TOTALS*
PEAK FLOW (cms)=	0.01	0.00	0.016 (iii)
TIME TO PEAK (hrs)=	2.50	2.58	2.50
RUNOFF VOLUME (mm)=	54.69	26.90	47.68
TOTAL RAINFALL (mm)=	55.69	55.69	55.69
RUNOFF COEFFICIENT =	0.98	0.48	0.86

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.





```

-----
| CALIB                               |
| STANDHYD ( 0208) | Area (ha)= 0.04 |
| ID= 1 DT= 5.0 min | Total Imp(%)= 75.00 Dir. Conn.(%)= 75.00
-----

```

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.03	0.01	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	16.93	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	51.24	31.75	
over (min)	5.00	15.00	
Storage Coeff. (min)=	1.15 (ii)	12.32 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.34	0.09	
			*TOTALS*
PEAK FLOW (cms)=	0.00	0.00	0.005 (iii)
TIME TO PEAK (hrs)=	2.25	2.58	2.50
RUNOFF VOLUME (mm)=	54.69	26.90	47.69
TOTAL RAINFALL (mm)=	55.69	55.69	55.69
RUNOFF COEFFICIENT =	0.98	0.48	0.86

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB                               |
| STANDHYD ( 0205) | Area (ha)= 0.22 |
| ID= 1 DT= 5.0 min | Total Imp(%)= 99.00 Dir. Conn.(%)= 99.00
-----

```

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.22	0.00	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	38.38	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	51.24	32.92	
over (min)	5.00	5.00	
Storage Coeff. (min)=	1.88 (ii)	3.35 (ii)	
Unit Hyd. Tpeak (min)=	5.00	5.00	
Unit Hyd. peak (cms)=	0.32	0.26	
			*TOTALS*
PEAK FLOW (cms)=	0.03	0.00	0.031 (iii)



TIME TO PEAK (hrs)=	2.42	2.50	2.50
RUNOFF VOLUME (mm)=	54.69	26.90	54.40
TOTAL RAINFALL (mm)=	55.69	55.69	55.69
RUNOFF COEFFICIENT =	0.98	0.48	0.98

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD ( 0206)	Area (ha)=	0.51	
ID= 1 DT= 5.0 min	Total Imp(%)=	88.00	Dir. Conn.(%)= 88.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.45	0.06	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	58.54	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	51.24	32.92	
over (min)	5.00	10.00	
Storage Coeff. (min)=	2.42 (ii)	6.58 (ii)	
Unit Hyd. Tpeak (min)=	5.00	10.00	
Unit Hyd. peak (cms)=	0.30	0.14	
			*TOTALS*
PEAK FLOW (cms)=	0.06	0.01	0.070 (iii)
TIME TO PEAK (hrs)=	2.50	2.50	2.50
RUNOFF VOLUME (mm)=	54.69	26.90	51.35
TOTAL RAINFALL (mm)=	55.69	55.69	55.69
RUNOFF COEFFICIENT =	0.98	0.48	0.92

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD ( 2060)				
1 + 2 = 3	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 0204):	0.13	0.016	2.50	47.68
+ ID2= 2 ( 0205):	0.22	0.031	2.50	54.40



```
=====
ID = 3 ( 2060):    0.35  0.047  2.50  51.95
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```
-----
| ADD HYD ( 2060) |
| 3 + 2 = 1 |
-----
          AREA    QPEAK    TPEAK    R.V.
          (ha)    (cms)    (hrs)    (mm)
ID1= 3 ( 2060):    0.35  0.047  2.50  51.95
+ ID2= 2 ( 0206):    0.51  0.070  2.50  51.35
=====
ID = 1 ( 2060):    0.86  0.117  2.50  51.59
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```
-----
| ADD HYD ( 2060) |
| 1 + 2 = 3 |
-----
          AREA    QPEAK    TPEAK    R.V.
          (ha)    (cms)    (hrs)    (mm)
ID1= 1 ( 2060):    0.86  0.117  2.50  51.59
+ ID2= 2 ( 0208):    0.04  0.005  2.50  47.69
=====
ID = 3 ( 2060):    0.90  0.122  2.50  51.41
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```
-----
| RESERVOIR( 20601) | OVERFLOW IS OFF
| IN= 2---> OUT= 1 |
| DT= 5.0 min |
-----
          OUTFLOW    STORAGE    OUTFLOW    STORAGE
          (cms)    (ha.m.)    (cms)    (ha.m.)
          0.0000    0.0000    0.0120    0.0571
```

```

          AREA    QPEAK    TPEAK    R.V.
          (ha)    (cms)    (hrs)    (mm)
INFLOW : ID= 2 ( 2060)    0.905    0.122    2.50    51.41
OUTFLOW: ID= 1 ( 20601)    0.905    0.008    4.08    50.07
```

```

PEAK FLOW REDUCTION [Qout/Qin](%)= 6.69
TIME SHIFT OF PEAK FLOW (min)= 95.00
MAXIMUM STORAGE USED (ha.m.)= 0.0388
```

```
-----
| CALIB |
| STANDHYD ( 2061) | Area (ha)= 0.05
| ID= 1 DT= 5.0 min | Total Imp(%)= 82.00 Dir. Conn.(%)= 82.00
```



	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.04	0.01	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	17.32	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	51.24	31.75	
over (min)	5.00	15.00	
Storage Coeff. (min)=	1.17 (ii)	12.33 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.34	0.09	
			*TOTALS*
PEAK FLOW (cms)=	0.01	0.00	0.006 (iii)
TIME TO PEAK (hrs)=	2.42	2.58	2.50
RUNOFF VOLUME (mm)=	54.69	26.90	49.65
TOTAL RAINFALL (mm)=	55.69	55.69	55.69
RUNOFF COEFFICIENT =	0.98	0.48	0.89

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD ( 20602)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 20601):	0.90	0.008	4.08	50.07
+ ID2= 2 ( 2061):	0.05	0.006	2.50	49.65
=====				
ID = 3 ( 20602):	0.95	0.012	2.50	50.05

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 0003)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 0002):	2.34	0.038	2.50	45.98
+ ID2= 2 ( 20602):	0.95	0.012	2.50	50.05
=====				
ID = 3 ( 0003):	3.29	0.050	2.50	47.16

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.



ADD HYD ( 0003)	AREA	QPEAK	TPEAK	R.V.
3 + 2 = 1	(ha)	(cms)	(hrs)	(mm)
ID1= 3 ( 0003):	3.29	0.050	2.50	47.16
+ ID2= 2 ( 20701):	0.63	0.011	2.50	42.57
=====				
ID = 1 ( 0003):	3.92	0.061	2.50	46.42

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB	Area	(ha)=	0.19
STANDHYD ( 2201)	Total Imp(%)=	99.00	Dir. Conn.(%)= 99.00
ID= 1 DT= 5.0 min			

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.19	0.00	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	35.50	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	51.24	32.92	
over (min)	5.00	5.00	
Storage Coeff. (min)=	1.79 (ii)	3.26 (ii)	
Unit Hyd. Tpeak (min)=	5.00	5.00	
Unit Hyd. peak (cms)=	0.32	0.27	
			*TOTALS*
PEAK FLOW (cms)=	0.03	0.00	0.027 (iii)
TIME TO PEAK (hrs)=	2.50	2.50	2.50
RUNOFF VOLUME (mm)=	54.69	26.90	54.41
TOTAL RAINFALL (mm)=	55.69	55.69	55.69
RUNOFF COEFFICIENT =	0.98	0.48	0.98

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD ( 0006)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 0003):	3.92	0.061	2.50	46.42



+ ID2= 2 ( 2201):	0.19	0.027	2.50	54.41
=====				
ID = 3 ( <del>0006</del> ):	4.11	0.088	2.50	46.79

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB			
NASHYD ( 2141)	Area (ha)=	0.67	Curve Number (CN)= 85.0
ID= 1 DT= 5.0 min	Ia (mm)=	5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)=	0.20	

Unit Hyd Qpeak (cms)= 0.128

PEAK FLOW (cms)= 0.049 (i)  
 TIME TO PEAK (hrs)= 2.500  
 RUNOFF VOLUME (mm)= 26.850  
 TOTAL RAINFALL (mm)= 55.690  
 RUNOFF COEFFICIENT = 0.482

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD ( 2142)	Area (ha)=	0.36	
ID= 1 DT= 5.0 min	Total Imp(%)=	20.00	Dir. Conn.(%)= 5.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	0.07	0.29
Dep. Storage (mm)=	1.00	5.00
Average Slope (%)=	1.00	2.00
Length (m)=	49.14	40.00
Mannings n =	0.013	0.250

Max.Eff.Inten.(mm/hr)=	51.24	42.46
over (min)	5.00	15.00
Storage Coeff. (min)=	2.18 (ii)	12.12 (ii)
Unit Hyd. Tpeak (min)=	5.00	15.00
Unit Hyd. peak (cms)=	0.31	0.09

			*TOTALS*
PEAK FLOW (cms)=	0.00	0.03	0.029 (iii)
TIME TO PEAK (hrs)=	2.50	2.58	2.50
RUNOFF VOLUME (mm)=	54.69	29.70	30.93
TOTAL RAINFALL (mm)=	55.69	55.69	55.69
RUNOFF COEFFICIENT =	0.98	0.53	0.56

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:

CN\* = 85.0 Ia = Dep. Storage (Above)

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL



THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD ( 0214)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 ( 2141):	0.67	0.049	2.50	26.85
+ ID2= 2 ( 2142):	0.36	0.029	2.50	30.93
=====				
ID = 3 ( 0214):	1.03	0.077	2.50	28.28

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB STANDHYD ( 0210)	Area (ha)=	Total Imp(%)=	Dir. Conn.(%)=
ID= 1 DT= 5.0 min	0.14	92.00	92.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.13	0.01	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	30.44	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	51.24	32.92	
over (min)	5.00	10.00	
Storage Coeff. (min)=	1.64 (ii)	5.11 (ii)	
Unit Hyd. Tpeak (min)=	5.00	10.00	
Unit Hyd. peak (cms)=	0.32	0.16	
			*TOTALS*
PEAK FLOW (cms)=	0.02	0.00	0.019 (iii)
TIME TO PEAK (hrs)=	2.50	2.50	2.50
RUNOFF VOLUME (mm)=	54.69	26.90	52.46
TOTAL RAINFALL (mm)=	55.69	55.69	55.69
RUNOFF COEFFICIENT =	0.98	0.48	0.94

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB STANDHYD ( 0211)	Area (ha)=
	0.11



| ID= 1 DT= 5.0 min | Total Imp(%)= 75.00 Dir. Conn.(%)= 75.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.08	0.03	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	26.58	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	51.24	31.75	
over (min)	5.00	15.00	
Storage Coeff. (min)=	1.51 (ii)	12.68 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.33	0.08	
			*TOTALS*
PEAK FLOW (cms)=	0.01	0.00	0.013 (iii)
TIME TO PEAK (hrs)=	2.50	2.58	2.50
RUNOFF VOLUME (mm)=	54.69	26.90	47.68
TOTAL RAINFALL (mm)=	55.69	55.69	55.69
RUNOFF COEFFICIENT =	0.98	0.48	0.86

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----

-----

| CALIB |  
| STANDHYD ( 0203) | Area (ha)= 0.18  
| ID= 1 DT= 5.0 min | Total Imp(%)= 32.00 Dir. Conn.(%)= 32.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.06	0.12	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	34.74	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	51.24	31.75	
over (min)	5.00	15.00	
Storage Coeff. (min)=	1.77 (ii)	12.94 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.32	0.08	
			*TOTALS*
PEAK FLOW (cms)=	0.01	0.01	0.016 (iii)
TIME TO PEAK (hrs)=	2.42	2.58	2.50
RUNOFF VOLUME (mm)=	54.69	26.90	35.76
TOTAL RAINFALL (mm)=	55.69	55.69	55.69





RUNOFF COEFFICIENT = 0.98 0.48 0.64

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | CALIB |  
 | STANDHYD ( 0213) | Area (ha)= 0.68  
 | ID= 1 DT= 5.0 min | Total Imp(%)= 80.00 Dir. Conn.(%)= 80.00  
 -----

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.54	0.14	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	67.18	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	51.24	31.75	
over (min)	5.00	15.00	
Storage Coeff. (min)=	2.63 (ii)	13.80 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.29	0.08	
			*TOTALS*
PEAK FLOW (cms)=	0.08	0.01	0.086 (iii)
TIME TO PEAK (hrs)=	2.50	2.58	2.50
RUNOFF VOLUME (mm)=	54.69	26.90	49.12
TOTAL RAINFALL (mm)=	55.69	55.69	55.69
RUNOFF COEFFICIENT =	0.98	0.48	0.88

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | CALIB |  
 | STANDHYD ( 0212) | Area (ha)= 0.22  
 | ID= 1 DT= 5.0 min | Total Imp(%)= 92.00 Dir. Conn.(%)= 92.00  
 -----

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	0.20	0.02
Dep. Storage (mm)=	1.00	5.00
Average Slope (%)=	1.00	2.00
Length (m)=	38.04	40.00



Mannings n	=	0.013	0.250	
Max.Eff.Inten.(mm/hr)=		51.24	32.92	
over (min)		5.00	10.00	
Storage Coeff. (min)=		1.87 (ii)	5.34 (ii)	
Unit Hyd. Tpeak (min)=		5.00	10.00	
Unit Hyd. peak (cms)=		0.32	0.16	
				*TOTALS*
PEAK FLOW (cms)=		0.03	0.00	0.030 (iii)
TIME TO PEAK (hrs)=		2.42	2.50	2.50
RUNOFF VOLUME (mm)=		54.69	26.90	52.45
TOTAL RAINFALL (mm)=		55.69	55.69	55.69
RUNOFF COEFFICIENT =		0.98	0.48	0.94

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0    Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD ( 2130)				
1 + 2 = 3	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 0203):	0.18	0.016	2.50	35.76
+ ID2= 2 ( 0210):	0.14	0.019	2.50	52.46
=====				
ID = 3 ( 2130):	0.32	0.036	2.50	43.01

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 2130)				
3 + 2 = 1	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 3 ( 2130):	0.32	0.036	2.50	43.01
+ ID2= 2 ( 0211):	0.11	0.013	2.50	47.68
=====				
ID = 1 ( 2130):	0.43	0.049	2.50	44.17

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 2130)				
1 + 2 = 3	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)



```

ID1= 1 ( 2130):    0.43  0.049   2.50  44.17
+ ID2= 2 ( 0212):    0.22  0.030   2.50  52.45
=====
ID = 3 ( 2130):    0.64  0.079   2.50  46.97

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| ADD HYD ( 2130) |
| 3 + 2 = 1 |
-----
| AREA    QPEAK    TPEAK    R.V.
| (ha)    (cms)    (hrs)    (mm)
-----
ID1= 3 ( 2130):    0.64  0.079   2.50  46.97
+ ID2= 2 ( 0213):    0.68  0.086   2.50  49.12
-----
ID = 1 ( 2130):    1.32  0.164   2.50  48.07

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| RESERVOIR( 21301) | OVERFLOW IS OFF
| IN= 2---> OUT= 1 |
| DT= 5.0 min |
-----
| OUTFLOW    STORAGE    | OUTFLOW    STORAGE
| (cms)      (ha.m.)    | (cms)      (ha.m.)
-----
| 0.0000    0.0000    | 0.0160    0.0793
-----
| AREA    QPEAK    TPEAK    R.V.
| (ha)    (cms)    (hrs)    (mm)
-----
INFLOW : ID= 2 ( 2130)    1.320    0.164    2.50    48.07
OUTFLOW: ID= 1 ( 21301)  1.320    0.011    4.08    47.12

```

```

PEAK FLOW REDUCTION [Qout/Qin](%)= 6.51
TIME SHIFT OF PEAK FLOW (min)= 95.00
MAXIMUM STORAGE USED (ha.m.)= 0.0530

```

```

-----
| CALIB
| STANDHYD ( 2131) | Area (ha)= 0.12
| ID= 1 DT= 5.0 min | Total Imp(%)= 72.00 Dir. Conn.(%)= 72.00
-----

```

```

| IMPERVIOUS    PERVIOUS (i)
| Surface Area (ha)= 0.08    0.03
| Dep. Storage (mm)= 1.00    5.00
| Average Slope (%)= 1.00    2.00
| Length (m)= 27.69    40.00
| Mannings n = 0.013    0.250
-----
| Max.Eff.Inten.(mm/hr)= 51.24    31.75
| over (min) = 5.00    15.00

```



Storage Coeff. (min)=	1.54 (ii)	12.71 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.33	0.08	
			*TOTALS*
PEAK FLOW (cms)=	0.01	0.00	0.014 (iii)
TIME TO PEAK (hrs)=	2.42	2.58	2.50
RUNOFF VOLUME (mm)=	54.69	26.90	46.84
TOTAL RAINFALL (mm)=	55.69	55.69	55.69
RUNOFF COEFFICIENT =	0.98	0.48	0.84

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| ADD HYD ( 21302) |
| 1 + 2 = 3 |
-----

```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 ( 21301):	1.32	0.011	4.08	47.12
+ ID2= 2 ( 2131):	0.12	0.014	2.50	46.84
=====				
ID = 3 ( 21302):	1.43	0.021	2.50	47.10

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| ADD HYD ( 0005) |
| 1 + 2 = 3 |
-----

```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 ( 0006):	4.11	0.088	2.50	46.79
+ ID2= 2 ( 21302):	1.43	0.021	2.50	47.10
=====				
ID = 3 ( 0005):	5.55	0.109	2.50	46.87

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| ADD HYD ( 0005) |
| 3 + 2 = 1 |
-----

```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 3 ( 0005):	5.55	0.109	2.50	46.87
+ ID2= 2 ( 0214):	1.03	0.077	2.50	28.28
=====				
ID = 1 ( 0005):	6.58	0.186	2.50	43.95



NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

=====
=====
V   V   I   SSSSS U   U   A   L           (v 6.0.2001)
V   V   I   SS   U   U   A A   L
V   V   I   SS   U   U   AAAAA L
V   V   I   SS   U   U   A   A   L
  VV   I   SSSSS UUUUU A   A   LLLLL

```

```

  000   TTTTT TTTTT H   H   Y   Y   M   M   000   TM
O   O   T   T   H   H   Y   Y   MM MM O   O
O   O   T   T   H   H   Y   M   M   O   O
  000   T   T   H   H   Y   M   M   000

```

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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

Input filename: C:\Program Files (x86)\Visual OTTHYMO 6.0\V02\voin.dat

Output filename:

C:\Users\jliang\AppData\Local\Civica\XH5\becad37f-97fe-4a15-a3fd-f87dd2156d5f\3b3f  
 fdb-d70e-4a57-afa8-73ae081a11f9\scena

Summary filename:

C:\Users\jliang\AppData\Local\Civica\XH5\becad37f-97fe-4a15-a3fd-f87dd2156d5f\3b3f  
 fdb-d70e-4a57-afa8-73ae081a11f9\scena

DATE: 10-27-2021

TIME: 05:35:39

USER:

COMMENTS: \_\_\_\_\_

```

-----
*****
** SIMULATION : Run 04           **
*****

```



READ STORM

Filename: C:\Users\jliang\AppData\Local\Temp\

907c1cff-ccb1-41c0-9867-a9890799f0d3\88868af7

Ptotal= 65.59 mm

Comments: 25-Year 6-hour AES Storm

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.25	1.31	1.75	22.30	3.25	9.18	4.75	1.31
0.50	1.31	2.00	22.30	3.50	9.18	5.00	1.31
0.75	1.31	2.25	60.35	3.75	5.25	5.25	1.31
1.00	1.31	2.50	60.35	4.00	5.25	5.50	1.31
1.25	7.87	2.75	17.06	4.25	2.62	5.75	1.31
1.50	7.87	3.00	17.06	4.50	2.62	6.00	1.31

CALIB

NASHYD ( 2002)

ID= 1 DT= 5.0 min

Area (ha)= 0.00 Curve Number (CN)= 85.0

Ia (mm)= 5.00 # of Linear Res.(N)= 3.00

U.H. Tp(hrs)= 0.20

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	1.31	1.583	22.30	3.083	9.18	4.58	1.31
0.167	1.31	1.667	22.30	3.167	9.18	4.67	1.31
0.250	1.31	1.750	22.30	3.250	9.18	4.75	1.31
0.333	1.31	1.833	22.30	3.333	9.18	4.83	1.31
0.417	1.31	1.917	22.30	3.417	9.18	4.92	1.31
0.500	1.31	2.000	22.30	3.500	9.18	5.00	1.31
0.583	1.31	2.083	60.35	3.583	5.25	5.08	1.31
0.667	1.31	2.167	60.35	3.667	5.25	5.17	1.31
0.750	1.31	2.250	60.35	3.750	5.25	5.25	1.31
0.833	1.31	2.333	60.35	3.833	5.25	5.33	1.31
0.917	1.31	2.417	60.35	3.917	5.25	5.42	1.31
1.000	1.31	2.500	60.35	4.000	5.25	5.50	1.31
1.083	7.87	2.583	17.06	4.083	2.62	5.58	1.31
1.167	7.87	2.667	17.06	4.167	2.62	5.67	1.31
1.250	7.87	2.750	17.06	4.250	2.62	5.75	1.31
1.333	7.87	2.833	17.06	4.333	2.62	5.83	1.31
1.417	7.87	2.917	17.06	4.417	2.62	5.92	1.31
1.500	7.87	3.000	17.06	4.500	2.62	6.00	1.31

Unit Hyd Qpeak (cms)= 0.001



PEAK FLOW (cms)= 0.000 (i)  
 TIME TO PEAK (hrs)= 2.500  
 RUNOFF VOLUME (mm)= 34.114  
 TOTAL RAINFALL (mm)= 65.590  
 RUNOFF COEFFICIENT = 0.520

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | CALIB |  
 | STANDHYD ( 0201) | Area (ha)= 0.73  
 | ID= 1 DT= 5.0 min | Total Imp(%)= 80.00 Dir. Conn.(%)= 80.00  
 -----

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.58	0.15	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	69.71	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	60.35	41.96	
over (min)	5.00	10.00	
Storage Coeff. (min)=	2.52 (ii)	7.48 (ii)	
Unit Hyd. Tpeak (min)=	5.00	10.00	
Unit Hyd. peak (cms)=	0.29	0.13	
			*TOTALS*
PEAK FLOW (cms)=	0.10	0.02	0.113 (iii)
TIME TO PEAK (hrs)=	2.50	2.50	2.50
RUNOFF VOLUME (mm)=	64.59	34.83	58.63
TOTAL RAINFALL (mm)=	65.59	65.59	65.59
RUNOFF COEFFICIENT =	0.98	0.53	0.89

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:

CN\* = 85.0 Ia = Dep. Storage (Above)

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | CALIB |  
 | STANDHYD ( 0200) | Area (ha)= 0.46  
 | ID= 1 DT= 5.0 min | Total Imp(%)= 67.00 Dir. Conn.(%)= 67.00  
 -----

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	0.31	0.15
Dep. Storage (mm)=	1.00	5.00
Average Slope (%)=	1.00	2.00
Length (m)=	55.14	40.00



Mannings n	=	0.013	0.250	
Max.Eff.Inten.(mm/hr)=		60.35	41.96	
over (min)		5.00	15.00	
Storage Coeff. (min)=		2.19 (ii)	12.18 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		0.31	0.09	
				*TOTALS*
PEAK FLOW (cms)=		0.05	0.01	0.065 (iii)
TIME TO PEAK (hrs)=		2.50	2.58	2.50
RUNOFF VOLUME (mm)=		64.59	34.83	54.75
TOTAL RAINFALL (mm)=		65.59	65.59	65.59
RUNOFF COEFFICIENT =		0.98	0.53	0.83

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0    Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----					
ADD HYD ( 2000)					
1 + 2 = 3					
		AREA	QPEAK	TPEAK	R.V.
		(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 0200):		0.46	0.065	2.50	54.75
+ ID2= 2 ( 0201):		0.73	0.113	2.50	58.63
=====					
ID = 3 ( 2000):		1.18	0.178	2.50	57.14

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----					
RESERVOIR( 20011)					
IN= 2---> OUT= 1					
DT= 5.0 min					
-----					
		OVERFLOW IS OFF			
		OUTFLOW	STORAGE	OUTFLOW	STORAGE
		(cms)	(ha.m.)	(cms)	(ha.m.)
		0.0000	0.0000	0.0140	0.0709
		AREA	QPEAK	TPEAK	R.V.
		(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 ( 2000)		1.185	0.178	2.50	57.14
OUTFLOW: ID= 1 ( 20011)		1.185	0.011	4.08	56.05

PEAK FLOW REDUCTION [Qout/Qin](%)= 6.30  
 TIME SHIFT OF PEAK FLOW (min)= 95.00  
 MAXIMUM STORAGE USED (ha.m.)= 0.0568





-----  
 | CALIB |  
 | STANDHYD ( 2011) | Area (ha)= 0.08  
 | ID= 1 DT= 5.0 min | Total Imp(%)= 73.00 Dir. Conn.(%)= 73.00  
 -----

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.06	0.02	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	22.66	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	60.35	41.96	
over (min)	5.00	15.00	
Storage Coeff. (min)=	1.28 (ii)	11.27 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.33	0.09	
			*TOTALS*
PEAK FLOW (cms)=	0.01	0.00	0.011 (iii)
TIME TO PEAK (hrs)=	2.50	2.58	2.50
RUNOFF VOLUME (mm)=	64.59	34.83	56.48
TOTAL RAINFALL (mm)=	65.59	65.59	65.59
RUNOFF COEFFICIENT =	0.98	0.53	0.86

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | CALIB |  
 | STANDHYD ( 2012) | Area (ha)= 0.03  
 | ID= 1 DT= 5.0 min | Total Imp(%)= 65.00 Dir. Conn.(%)= 65.00  
 -----

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.02	0.01	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	14.61	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	60.35	41.96	
over (min)	5.00	15.00	
Storage Coeff. (min)=	0.99 (ii)	10.97 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.34	0.09	
			*TOTALS*
PEAK FLOW (cms)=	0.00	0.00	0.005 (iii)



TIME TO PEAK (hrs)=	2.25	2.58	2.50
RUNOFF VOLUME (mm)=	64.59	34.83	54.08
TOTAL RAINFALL (mm)=	65.59	65.59	65.59
RUNOFF COEFFICIENT =	0.98	0.53	0.82

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD ( 2001)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 20011):	1.18	0.011	4.08	56.05
+ ID2= 2 ( 2002):	0.00	0.000	2.50	34.11
=====				
ID = 3 ( 2001):	1.19	0.011	4.08	55.96

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 2001)	AREA	QPEAK	TPEAK	R.V.
3 + 2 = 1	(ha)	(cms)	(hrs)	(mm)
ID1= 3 ( 2001):	1.19	0.011	4.08	55.96
+ ID2= 2 ( 2011):	0.08	0.011	2.50	56.48
=====				
ID = 1 ( 2001):	1.27	0.020	2.50	55.99

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 2001)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 2001):	1.27	0.020	2.50	55.99
+ ID2= 2 ( 2012):	0.03	0.005	2.50	54.08
=====				
ID = 3 ( 2001):	1.30	0.024	2.50	55.95

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

| CALIB |



| STANDHYD ( 0202) | Area (ha)= 0.94  
 | ID= 1 DT= 5.0 min | Total Imp(%)= 70.00 Dir. Conn.(%)= 70.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.66	0.28	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	79.12	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	60.35	41.96	
over (min)	5.00	15.00	
Storage Coeff. (min)=	2.72 (ii)	12.71 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.29	0.08	
			*TOTALS*
PEAK FLOW (cms)=	0.11	0.03	0.135 (iii)
TIME TO PEAK (hrs)=	2.50	2.58	2.50
RUNOFF VOLUME (mm)=	64.59	34.83	55.65
TOTAL RAINFALL (mm)=	65.59	65.59	65.59
RUNOFF COEFFICIENT =	0.98	0.53	0.85

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| RESERVOIR( 2020) | OVERFLOW IS OFF  
 | IN= 2---> OUT= 1 |  
 | DT= 5.0 min |

OUTFLOW	STORAGE	OUTFLOW	STORAGE
(cms)	(ha.m.)	(cms)	(ha.m.)
0.0000	0.0000	0.0090	0.0561

	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 ( 0202)	0.939	0.135	2.50	55.65
OUTFLOW: ID= 1 ( 2020)	0.939	0.007	4.33	53.97

PEAK FLOW REDUCTION [Qout/Qin](%)= 5.32  
 TIME SHIFT OF PEAK FLOW (min)=110.00  
 MAXIMUM STORAGE USED (ha.m.)= 0.0447

| CALIB |  
 | STANDHYD ( 2021) | Area (ha)= 0.03  
 | ID= 1 DT= 5.0 min | Total Imp(%)= 65.00 Dir. Conn.(%)= 65.00



	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.02	0.01	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	14.83	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	60.35	41.96	
over (min)	5.00	15.00	
Storage Coeff. (min)=	0.99 (ii)	10.98 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.34	0.09	
			*TOTALS*
PEAK FLOW (cms)=	0.00	0.00	0.005 (iii)
TIME TO PEAK (hrs)=	2.25	2.58	2.50
RUNOFF VOLUME (mm)=	64.59	34.83	54.08
TOTAL RAINFALL (mm)=	65.59	65.59	65.59
RUNOFF COEFFICIENT =	0.98	0.53	0.82

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0    Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB		STANDHYD ( 2022)	
Area (ha)=	0.07	Total Imp(%)=	99.00
		Dir. Conn.(%)=	99.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.07	0.00	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	22.06	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	60.35	41.96	
over (min)	5.00	5.00	
Storage Coeff. (min)=	1.26 (ii)	2.64 (ii)	
Unit Hyd. Tpeak (min)=	5.00	5.00	
Unit Hyd. peak (cms)=	0.33	0.29	
			*TOTALS*
PEAK FLOW (cms)=	0.01	0.00	0.012 (iii)
TIME TO PEAK (hrs)=	2.42	2.50	2.50
RUNOFF VOLUME (mm)=	64.59	34.83	64.29
TOTAL RAINFALL (mm)=	65.59	65.59	65.59
RUNOFF COEFFICIENT =	0.98	0.53	0.98



- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
~~CN\* = 85.0~~ Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD ( 20201)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 2020):	0.94	0.007	4.33	53.97
+ ID2= 2 ( 2021):	0.03	0.005	2.50	54.08
=====				
ID = 3 ( 20201):	0.97	0.009	2.50	53.98

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 20201)	AREA	QPEAK	TPEAK	R.V.
3 + 2 = 1	(ha)	(cms)	(hrs)	(mm)
ID1= 3 ( 20201):	0.97	0.009	2.50	53.98
+ ID2= 2 ( 2022):	0.07	0.012	2.50	64.29
=====				
ID = 1 ( 20201):	1.04	0.022	2.50	54.70

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 0002)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 2001):	1.30	0.024	2.50	55.95
+ ID2= 2 ( 20201):	1.04	0.022	2.50	54.70
=====				
ID = 3 ( 0002):	2.34	0.046	2.50	55.39

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB	Area	(ha)=	0.07
STANDHYD ( 2071)	Total Imp(%)=	74.00	Dir. Conn.(%)= 74.00
ID= 1 DT= 5.0 min			

IMPERVIOUS      PERVIOUS (i)



Surface Area	(ha)=	0.05	0.02	
Dep. Storage	(mm)=	1.00	5.00	
Average Slope	(%)=	1.00	2.00	
Length	(m)=	21.29	40.00	
Mannings n	=	0.013	0.250	
Max.Eff.Inten.(mm/hr)=		60.35	41.96	
over (min)		5.00	15.00	
Storage Coeff. (min)=		1.24 (ii)	11.22 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		0.33	0.09	
				*TOTALS*
PEAK FLOW	(cms)=	0.01	0.00	0.010 (iii)
TIME TO PEAK	(hrs)=	2.42	2.58	2.50
RUNOFF VOLUME	(mm)=	64.59	34.83	56.78
TOTAL RAINFALL	(mm)=	65.59	65.59	65.59
RUNOFF COEFFICIENT	=	0.98	0.53	0.87

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB				
STANDHYD ( 0207)	Area	(ha)=	0.56	
ID= 1 DT= 5.0 min	Total Imp(%)=	63.00	Dir. Conn.(%)=	63.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	0.35	0.21	
Dep. Storage	(mm)=	1.00	5.00	
Average Slope	(%)=	1.00	2.00	
Length	(m)=	61.05	40.00	
Mannings n	=	0.013	0.250	
Max.Eff.Inten.(mm/hr)=		60.35	41.96	
over (min)		5.00	15.00	
Storage Coeff. (min)=		2.33 (ii)	12.31 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		0.30	0.09	
				*TOTALS*
PEAK FLOW	(cms)=	0.06	0.02	0.077 (iii)
TIME TO PEAK	(hrs)=	2.50	2.58	2.50
RUNOFF VOLUME	(mm)=	64.59	34.83	53.56
TOTAL RAINFALL	(mm)=	65.59	65.59	65.59
RUNOFF COEFFICIENT	=	0.98	0.53	0.82

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:



- CN\* = 85.0    Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR( 2070)		OVERFLOW IS OFF			
IN= 2---> OUT= 1		OUTFLOW		STORAGE	
DT= 5.0 min		(cms)	(ha.m.)	(cms)	(ha.m.)
		0.0000	0.0000	0.0060	0.0318
		AREA	QPEAK	TPEAK	R.V.
		(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 ( 0207)		0.559	0.077	2.50	53.56
OUTFLOW: ID= 1 ( 2070)		0.559	0.005	4.17	51.17
		PEAK FLOW REDUCTION [Qout/Qin](%)= 6.14			
		TIME SHIFT OF PEAK FLOW (min)=100.00			
		MAXIMUM STORAGE USED (ha.m.)= 0.0252			

ADD HYD ( 20701)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 2070):		0.56	0.005	4.17	51.17
+ ID2= 2 ( 2071):		0.07	0.010	2.50	56.78
=====					
ID = 3 ( 20701):		0.63	0.013	2.50	51.78

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB		Area	(ha)=	0.13
STANDHYD ( 0204)		Total Imp(%)=	75.00	Dir. Conn.(%)= 75.00
ID= 1 DT= 5.0 min		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	0.10	0.03	
Dep. Storage	(mm)=	1.00	5.00	
Average Slope	(%)=	1.00	2.00	
Length	(m)=	29.10	40.00	
Mannings n	=	0.013	0.250	
Max.Eff.Inten.(mm/hr)=		60.35	41.96	
over (min)		5.00	15.00	
Storage Coeff. (min)=		1.49 (ii)	11.48 (ii)	



Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.33	0.09	
			*TOTALS*
PEAK FLOW (cms)=	0.02	0.00	0.019 (iii)
TIME TO PEAK (hrs)=	2.42	2.58	2.50
RUNOFF VOLUME (mm)=	64.59	34.83	57.08
TOTAL RAINFALL (mm)=	65.59	65.59	65.59
RUNOFF COEFFICIENT =	0.98	0.53	0.87

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD ( 0208)	Area (ha)=	0.04	
ID= 1 DT= 5.0 min	Total Imp(%)=	75.00	Dir. Conn.(%)= 75.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.03	0.01	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	16.93	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	60.35	41.96	
over (min)	5.00	15.00	
Storage Coeff. (min)=	1.08 (ii)	11.07 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.34	0.09	
			*TOTALS*
PEAK FLOW (cms)=	0.01	0.00	0.006 (iii)
TIME TO PEAK (hrs)=	2.25	2.58	2.50
RUNOFF VOLUME (mm)=	64.59	34.83	57.08
TOTAL RAINFALL (mm)=	65.59	65.59	65.59
RUNOFF COEFFICIENT =	0.98	0.53	0.87

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD ( 0205)	Area (ha)=	0.22	





| ID= 1 DT= 5.0 min | Total Imp(%)= 99.00 Dir. Conn.(%)= 99.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.22	0.00	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	38.38	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	60.35	41.96	
over (min)	5.00	5.00	
Storage Coeff. (min)=	1.76 (ii)	3.13 (ii)	
Unit Hyd. Tpeak (min)=	5.00	5.00	
Unit Hyd. peak (cms)=	0.32	0.27	
			*TOTALS*
PEAK FLOW (cms)=	0.04	0.00	0.037 (iii)
TIME TO PEAK (hrs)=	2.42	2.50	2.50
RUNOFF VOLUME (mm)=	64.59	34.83	64.29
TOTAL RAINFALL (mm)=	65.59	65.59	65.59
RUNOFF COEFFICIENT =	0.98	0.53	0.98

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----

-----

| CALIB |  
| STANDHYD ( 0206) | Area (ha)= 0.51  
| ID= 1 DT= 5.0 min | Total Imp(%)= 88.00 Dir. Conn.(%)= 88.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.45	0.06	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	58.54	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	60.35	41.96	
over (min)	5.00	10.00	
Storage Coeff. (min)=	2.27 (ii)	6.16 (ii)	
Unit Hyd. Tpeak (min)=	5.00	10.00	
Unit Hyd. peak (cms)=	0.30	0.15	
			*TOTALS*
PEAK FLOW (cms)=	0.08	0.01	0.083 (iii)
TIME TO PEAK (hrs)=	2.50	2.50	2.50
RUNOFF VOLUME (mm)=	64.59	34.83	61.01
TOTAL RAINFALL (mm)=	65.59	65.59	65.59



RUNOFF COEFFICIENT = 0.98 0.53 0.93

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| ADD HYD ( 2060) |
| 1 + 2 = 3 |
-----
          AREA      QPEAK      TPEAK      R.V.
          (ha)      (cms)      (hrs)      (mm)
ID1= 1 ( 0204):  0.13  0.019  2.50  57.08
+ ID2= 2 ( 0205):  0.22  0.037  2.50  64.29
=====
ID = 3 ( 2060):  0.35  0.056  2.50  61.66
  
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| ADD HYD ( 2060) |
| 3 + 2 = 1 |
-----
          AREA      QPEAK      TPEAK      R.V.
          (ha)      (cms)      (hrs)      (mm)
ID1= 3 ( 2060):  0.35  0.056  2.50  61.66
+ ID2= 2 ( 0206):  0.51  0.083  2.50  61.01
=====
ID = 1 ( 2060):  0.86  0.138  2.50  61.27
  
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| ADD HYD ( 2060) |
| 1 + 2 = 3 |
-----
          AREA      QPEAK      TPEAK      R.V.
          (ha)      (cms)      (hrs)      (mm)
ID1= 1 ( 2060):  0.86  0.138  2.50  61.27
+ ID2= 2 ( 0208):  0.04  0.006  2.50  57.08
=====
ID = 3 ( 2060):  0.90  0.145  2.50  61.07
  
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| RESERVOIR( 20601) | OVERFLOW IS OFF
| IN= 2---> OUT= 1 |
| DT= 5.0 min |
-----
          OUTFLOW      STORAGE      OUTFLOW      STORAGE
          (cms)      (ha.m.)      (cms)      (ha.m.)
  
```



0.0000    0.0000    |    0.0120    0.0571

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 ( 2060)	0.905	0.145	2.50	61.07
OUTFLOW: ID= 1 ( 20601)	0.905	0.010	4.08	59.74

PEAK FLOW REDUCTION [Qout/Qin](%)= 6.69  
 TIME SHIFT OF PEAK FLOW (min)= 95.00  
 MAXIMUM STORAGE USED (ha.m.)= 0.0461

-----  
 -----  
 | CALIB |  
 | STANDHYD ( 2061) | Area (ha)= 0.05  
 | ID= 1 DT= 5.0 min | Total Imp(%)= 82.00 Dir. Conn.(%)= 82.00  
 -----

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.04	0.01	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	17.32	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	60.35	41.96	
over (min)	5.00	10.00	
Storage Coeff. (min)=	1.09 (ii)	5.80 (ii)	
Unit Hyd. Tpeak (min)=	5.00	10.00	
Unit Hyd. peak (cms)=	0.34	0.15	
			*TOTALS*
PEAK FLOW (cms)=	0.01	0.00	0.007 (iii)
TIME TO PEAK (hrs)=	2.25	2.50	2.50
RUNOFF VOLUME (mm)=	64.59	34.83	59.21
TOTAL RAINFALL (mm)=	65.59	65.59	65.59
RUNOFF COEFFICIENT =	0.98	0.53	0.90

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0    Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 -----  
 | ADD HYD ( 20602) |  
 | 1 + 2 = 3 | AREA QPEAK TPEAK R.V.  
 (ha) (cms) (hrs) (mm)  
 ID1= 1 ( 20601): 0.90 0.010 4.08 59.74  
 + ID2= 2 ( 2061): 0.05 0.007 2.50 59.21  
 -----



```
=====
ID = 3 ( 20602):      0.95  0.014  2.50  59.72
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```
-----
| ADD HYD ( 0003) |
| 1 + 2 = 3 |
-----
          AREA      QPEAK      TPEAK      R.V.
          (ha)      (cms)      (hrs)      (mm)
ID1= 1 ( 0002):    2.34    0.046    2.50    55.39
+ ID2= 2 ( 20602):  0.95    0.014    2.50    59.72
=====
ID = 3 ( 0003):    3.29    0.060    2.50    56.64
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```
-----
| ADD HYD ( 0003) |
| 3 + 2 = 1 |
-----
          AREA      QPEAK      TPEAK      R.V.
          (ha)      (cms)      (hrs)      (mm)
ID1= 3 ( 0003):    3.29    0.060    2.50    56.64
+ ID2= 2 ( 20701):  0.63    0.013    2.50    51.78
=====
ID = 1 ( 0003):    3.92    0.073    2.50    55.86
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```
-----
| CALIB
| STANDHYD ( 2201) |
| ID= 1 DT= 5.0 min |
-----
Area (ha)= 0.19
Total Imp(%)= 99.00 Dir. Conn.(%)= 99.00
```

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.19	0.00	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	35.50	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	60.35	41.96	
over (min)	5.00	5.00	
Storage Coeff. (min)=	1.68 (ii)	3.05 (ii)	
Unit Hyd. Tpeak (min)=	5.00	5.00	
Unit Hyd. peak (cms)=	0.32	0.27	
			*TOTALS*
PEAK FLOW (cms)=	0.03	0.00	0.032 (iii)
TIME TO PEAK (hrs)=	2.50	2.50	2.50
RUNOFF VOLUME (mm)=	64.59	34.83	64.29



TOTAL RAINFALL (mm)=	65.59	65.59	65.59
RUNOFF COEFFICIENT =	0.98	0.53	0.98

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD ( 0006)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 ( 0003):	3.92	0.073	2.50	55.86
+ ID2= 2 ( 2201):	0.19	0.032	2.50	64.29
=====				
ID = 3 ( 0006):	4.11	0.105	2.50	56.25

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB	Area (ha)=	Curve Number (CN)=
NASHYD ( 2141)	0.67	85.0
ID= 1 DT= 5.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= 0.20	

Unit Hyd Qpeak (cms)= 0.128

PEAK FLOW (cms)= 0.064 (i)  
 TIME TO PEAK (hrs)= 2.500  
 RUNOFF VOLUME (mm)= 34.759  
 TOTAL RAINFALL (mm)= 65.590  
 RUNOFF COEFFICIENT = 0.530

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	Area (ha)=	Dir. Conn.(%)=
STANDHYD ( 2142)	0.36	5.00
ID= 1 DT= 5.0 min	Total Imp(%)= 20.00	

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	0.07	0.29
Dep. Storage (mm)=	1.00	5.00
Average Slope (%)=	1.00	2.00
Length (m)=	49.14	40.00
Mannings n =	0.013	0.250



Max.Eff.Inten.(mm/hr)=	60.35	53.47	
over (min)	5.00	15.00	
Storage Coeff. (min)=	2.04 (ii)	11.11 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.31	0.09	
			*TOTALS*
PEAK FLOW (cms)=	0.00	0.03	0.037 (iii)
TIME TO PEAK (hrs)=	2.50	2.58	2.50
RUNOFF VOLUME (mm)=	64.59	38.01	39.32
TOTAL RAINFALL (mm)=	65.59	65.59	65.59
RUNOFF COEFFICIENT =	0.98	0.58	0.60

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0    Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----				
ADD HYD ( 0214)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 2141):	0.67	0.064	2.50	34.76
+ ID2= 2 ( 2142):	0.36	0.037	2.50	39.32
=====				
ID = 3 ( 0214):	1.03	0.101	2.50	36.35

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----				
CALIB				
STANDHYD ( 0210)				
ID= 1 DT= 5.0 min	Area (ha)=	0.14		
	Total Imp(%)=	92.00	Dir. Conn.(%)=	92.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	0.13	0.01
Dep. Storage (mm)=	1.00	5.00
Average Slope (%)=	1.00	2.00
Length (m)=	30.44	40.00
Mannings n =	0.013	0.250
Max.Eff.Inten.(mm/hr)=	60.35	41.96
over (min)	5.00	5.00
Storage Coeff. (min)=	1.53 (ii)	4.78 (ii)
Unit Hyd. Tpeak (min)=	5.00	5.00
Unit Hyd. peak (cms)=	0.33	0.22
		*TOTALS*



PEAK FLOW	(cms)=	0.02	0.00	0.023 (iii)
TIME TO PEAK	(hrs)=	2.42	2.50	2.50
RUNOFF VOLUME	(mm)=	64.59	34.83	62.20
TOTAL RAINFALL	(mm)=	65.59	65.59	65.59
RUNOFF COEFFICIENT	=	0.98	0.53	0.95

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD ( 0211)	Area (ha)=	0.11	
ID= 1 DT= 5.0 min	Total Imp(%)=	75.00	Dir. Conn.(%)= 75.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.08	0.03	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	26.58	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	60.35	41.96	
over (min)	5.00	15.00	
Storage Coeff. (min)=	1.41 (ii)	11.40 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.33	0.09	
			*TOTALS*
PEAK FLOW (cms)=	0.01	0.00	0.016 (iii)
TIME TO PEAK (hrs)=	2.42	2.58	2.50
RUNOFF VOLUME (mm)=	64.59	34.83	57.08
TOTAL RAINFALL (mm)=	65.59	65.59	65.59
RUNOFF COEFFICIENT =	0.98	0.53	0.87

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD ( 0203)	Area (ha)=	0.18	
ID= 1 DT= 5.0 min	Total Imp(%)=	32.00	Dir. Conn.(%)= 32.00

IMPERVIOUS PERVIOUS (i)



Surface Area	(ha)=	0.06	0.12	
Dep. Storage	(mm)=	1.00	5.00	
Average Slope	(%)=	1.00	2.00	
Length	(m)=	34.74	40.00	
Mannings n	=	0.013	0.250	
Max.Eff.Inten.(mm/hr)=		60.35	41.96	
over (min)		5.00	15.00	
Storage Coeff. (min)=		1.66 (ii)	11.65 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		0.32	0.09	
				*TOTALS*
PEAK FLOW	(cms)=	0.01	0.01	0.021 (iii)
TIME TO PEAK	(hrs)=	2.42	2.58	2.50
RUNOFF VOLUME	(mm)=	64.59	34.83	44.32
TOTAL RAINFALL	(mm)=	65.59	65.59	65.59
RUNOFF COEFFICIENT	=	0.98	0.53	0.68

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0    Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB				
STANDHYD ( 0213)		Area	(ha)=	0.68
ID= 1 DT= 5.0 min		Total Imp(%)=	80.00	Dir. Conn.(%)= 80.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	0.54	0.14	
Dep. Storage	(mm)=	1.00	5.00	
Average Slope	(%)=	1.00	2.00	
Length	(m)=	67.18	40.00	
Mannings n	=	0.013	0.250	
Max.Eff.Inten.(mm/hr)=		60.35	41.96	
over (min)		5.00	10.00	
Storage Coeff. (min)=		2.46 (ii)	7.42 (ii)	
Unit Hyd. Tpeak (min)=		5.00	10.00	
Unit Hyd. peak (cms)=		0.30	0.13	
				*TOTALS*
PEAK FLOW	(cms)=	0.09	0.01	0.105 (iii)
TIME TO PEAK	(hrs)=	2.50	2.50	2.50
RUNOFF VOLUME	(mm)=	64.59	34.83	58.63
TOTAL RAINFALL	(mm)=	65.59	65.59	65.59
RUNOFF COEFFICIENT	=	0.98	0.53	0.89

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:





- CN\* = 85.0    Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD ( 0212)	Area (ha)=	0.22	
ID= 1 DT= 5.0 min	Total Imp(%)=	92.00	Dir. Conn.(%)= 92.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.20	0.02	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	38.04	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	60.35	41.96	
over (min)	5.00	10.00	
Storage Coeff. (min)=	1.75 (ii)	5.00 (ii)	
Unit Hyd. Tpeak (min)=	5.00	10.00	
Unit Hyd. peak (cms)=	0.32	0.16	
			*TOTALS*
PEAK FLOW (cms)=	0.03	0.00	0.035 (iii)
TIME TO PEAK (hrs)=	2.50	2.50	2.50
RUNOFF VOLUME (mm)=	64.59	34.83	62.19
TOTAL RAINFALL (mm)=	65.59	65.59	65.59
RUNOFF COEFFICIENT =	0.98	0.53	0.95

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0    Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD ( 2130)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 ( 0203):	0.18	0.021	2.50	44.32
+ ID2= 2 ( 0210):	0.14	0.023	2.50	62.20
=====				
ID = 3 ( 2130):	0.32	0.043	2.50	52.08

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.



-----				
ADD HYD ( 2130)				
3 + 2 = 1				
-----				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 3 ( 2130):	0.32	0.043	2.50	52.08
+ ID2= 2 ( 0211):	0.11	0.016	2.50	57.08
=====				
ID = 1 ( 2130):	0.43	0.059	2.50	53.33

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----				
ADD HYD ( 2130)				
1 + 2 = 3				
-----				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 2130):	0.43	0.059	2.50	53.33
+ ID2= 2 ( 0212):	0.22	0.035	2.50	62.19
=====				
ID = 3 ( 2130):	0.64	0.095	2.50	56.32

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----				
ADD HYD ( 2130)				
3 + 2 = 1				
-----				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 3 ( 2130):	0.64	0.095	2.50	56.32
+ ID2= 2 ( 0213):	0.68	0.105	2.50	58.63
=====				
ID = 1 ( 2130):	1.32	0.200	2.50	57.50

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----				
RESERVOIR( 21301)				
IN= 2---> OUT= 1				
DT= 5.0 min				
-----				
OVERFLOW IS OFF				
	OUTFLOW	STORAGE	OUTFLOW	STORAGE
	(cms)	(ha.m.)	(cms)	(ha.m.)
	0.0000	0.0000	0.0160	0.0793

	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 ( 2130)	1.320	0.200	2.50	57.50
OUTFLOW: ID= 1 ( 21301)	1.320	0.013	4.08	56.55

PEAK FLOW REDUCTION [Qout/Qin](%)= 6.41  
 TIME SHIFT OF PEAK FLOW (min)= 95.00  
 MAXIMUM STORAGE USED (ha.m.)= 0.0635



-----  
 -----  
 | CALIB |  
 | STANDHYD ( 2131) | Area (ha)= 0.12  
 | ID= 1 DT= 5.0 min | Total Imp(%)= 72.00 Dir. Conn.(%)= 72.00  
 -----  
 -----

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.08	0.03	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	27.69	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	60.35	41.96	
over (min)	5.00	15.00	
Storage Coeff. (min)=	1.45 (ii)	11.44 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.33	0.09	
			*TOTALS*
PEAK FLOW (cms)=	0.01	0.00	0.017 (iii)
TIME TO PEAK (hrs)=	2.42	2.58	2.50
RUNOFF VOLUME (mm)=	64.59	34.83	56.18
TOTAL RAINFALL (mm)=	65.59	65.59	65.59
RUNOFF COEFFICIENT =	0.98	0.53	0.86

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 -----  
 | ADD HYD ( 21302) |  
 | 1 + 2 = 3 |

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 ( 21301):	1.32	0.013	4.08	56.55
+ ID2= 2 ( 2131):	0.12	0.017	2.50	56.18
=====				
ID = 3 ( 21302):	1.43	0.026	2.50	56.52

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----  
 -----  
 | ADD HYD ( 0005) |  
 | 1 + 2 = 3 |

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
--	--------------	----------------	----------------	--------------



ID1= 1 ( 0006):	4.11	0.105	2.50	56.25
+ ID2= 2 ( 21302):	1.43	0.026	2.50	56.52
=====				
ID = 3 ( 0005):	5.55	0.131	2.50	56.32

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----

ADD HYD ( 0005)				
3 + 2 = 1				
-----				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 3 ( 0005):	5.55	0.131	2.50	56.32
+ ID2= 2 ( 0214):	1.03	0.101	2.50	36.35
=====				
ID = 1 ( 0005):	6.58	0.231	2.50	53.18

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----

=====

=====

```

V   V   I   SSSSS  U   U   A   L           (v 6.0.2001)
V   V   I   SS    U   U   A A  L
V   V   I   SS    U   U   AAAAA L
V   V   I   SS    U   U   A   A  L
  VV    I   SSSSS  UUUUU  A   A  LLLLLL

  000  TTTTT  TTTTT  H   H  Y   Y  M   M  000  TM
  0   0   T    T    H   H  Y   Y  MM  MM  0   0
  0   0   T    T    H   H  Y   M   M  0   0
  000  T    T    H   H  Y   M   M  000
    
```

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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

Input filename: C:\Program Files (x86)\Visual OTTHYMO 6.0\V02\voin.dat

Output filename:

C:\Users\jliang\AppData\Local\Civica\XH5\becad37f-97fe-4a15-a3fd-f87dd2156d5f\caca9c51-172f-49af-9fda-63c96d6643a8\scena

Summary filename:

C:\Users\jliang\AppData\Local\Civica\XH5\becad37f-97fe-4a15-a3fd-f87dd2156d5f\caca9c51-172f-49af-9fda-63c96d6643a8\scena



DATE: 10-27-2021

TIME: 05:35:39

USER: \_\_\_\_\_

COMMENTS: \_\_\_\_\_

\*\*\*\*\*  
 \*\* SIMULATION : Run 05 \*\*  
 \*\*\*\*\*

READ STORM	Filename: C:\Users\jliang\AppData\Local\Temp\907c1cff-ccb1-41c0-9867-a9890799f0d3\d9be6e7f
Ptotal= 73.00 mm	Comments: 50-Year 6-hour AES Storm

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.25	1.46	1.75	24.82	3.25	10.22	4.75	1.46
0.50	1.46	2.00	24.82	3.50	10.22	5.00	1.46
0.75	1.46	2.25	67.16	3.75	5.84	5.25	1.46
1.00	1.46	2.50	67.16	4.00	5.84	5.50	1.46
1.25	8.76	2.75	18.98	4.25	2.92	5.75	1.46
1.50	8.76	3.00	18.98	4.50	2.92	6.00	1.46

CALIB	Area (ha)= 0.00	Curve Number (CN)= 85.0
NASHYD ( 2002)	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
ID= 1 DT= 5.0 min	U.H. Tp(hrs)= 0.20	

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	1.46	1.583	24.82	3.083	10.22	4.58	1.46
0.167	1.46	1.667	24.82	3.167	10.22	4.67	1.46
0.250	1.46	1.750	24.82	3.250	10.22	4.75	1.46
0.333	1.46	1.833	24.82	3.333	10.22	4.83	1.46
0.417	1.46	1.917	24.82	3.417	10.22	4.92	1.46



0.500	1.46	2.000	24.82	3.500	10.22	5.00	1.46
0.583	1.46	2.083	67.16	3.583	5.84	5.08	1.46
0.667	1.46	2.167	67.16	3.667	5.84	5.17	1.46
0.750	1.46	2.250	67.16	3.750	5.84	5.25	1.46
0.833	1.46	2.333	67.16	3.833	5.84	5.33	1.46
0.917	1.46	2.417	67.16	3.917	5.84	5.42	1.46
1.000	1.46	2.500	67.16	4.000	5.84	5.50	1.46
1.083	8.76	2.583	18.98	4.083	2.92	5.58	1.46
1.167	8.76	2.667	18.98	4.167	2.92	5.67	1.46
1.250	8.76	2.750	18.98	4.250	2.92	5.75	1.46
1.333	8.76	2.833	18.98	4.333	2.92	5.83	1.46
1.417	8.76	2.917	18.98	4.417	2.92	5.92	1.46
1.500	8.76	3.000	18.98	4.500	2.92	6.00	1.46

Unit Hyd Qpeak (cms)= 0.001

PEAK FLOW (cms)= 0.001 (i)  
 TIME TO PEAK (hrs)= 2.500  
 RUNOFF VOLUME (mm)= 40.216  
 TOTAL RAINFALL (mm)= 73.000  
 RUNOFF COEFFICIENT = 0.551

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 -----  
 | CALIB |  
 | STANDHYD ( 0201) | Area (ha)= 0.73  
 | ID= 1 DT= 5.0 min | Total Imp(%)= 80.00 Dir. Conn.(%)= 80.00  
 -----  
 -----

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.58	0.15	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	69.71	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	67.16	48.86	
over (min)	5.00	10.00	
Storage Coeff. (min)=	2.41 (ii)	7.17 (ii)	
Unit Hyd. Tpeak (min)=	5.00	10.00	
Unit Hyd. peak (cms)=	0.30	0.14	
			*TOTALS*
PEAK FLOW (cms)=	0.11	0.02	0.127 (iii)
TIME TO PEAK (hrs)=	2.50	2.50	2.50
RUNOFF VOLUME (mm)=	72.00	40.98	65.79
TOTAL RAINFALL (mm)=	73.00	73.00	73.00
RUNOFF COEFFICIENT =	0.99	0.56	0.90

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:



- CN\* = 85.0    Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----

CALIB			
STANDHYD ( 0200)	Area (ha)=	0.46	
ID= 1 DT= 5.0 min	Total Imp(%)=	67.00	Dir. Conn.(%)= 67.00

-----

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.31	0.15	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	55.14	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	67.16	48.86	
over (min)	5.00	15.00	
Storage Coeff. (min)=	2.10 (ii)	11.49 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.31	0.09	
			*TOTALS*
PEAK FLOW (cms)=	0.06	0.02	0.073 (iii)
TIME TO PEAK (hrs)=	2.50	2.58	2.50
RUNOFF VOLUME (mm)=	72.00	40.98	61.75
TOTAL RAINFALL (mm)=	73.00	73.00	73.00
RUNOFF COEFFICIENT =	0.99	0.56	0.85

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0    Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----

ADD HYD ( 2000)				
1 + 2 = 3	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 0200):	0.46	0.073	2.50	61.75
+ ID2= 2 ( 0201):	0.73	0.127	2.50	65.79
=====				
ID = 3 ( 2000):	1.18	0.200	2.50	64.24

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----



RESERVOIR( 20011)	OVERFLOW IS OFF			
IN= 2---> OUT= 1				
DT= 5.0 min	OUTFLOW	STORAGE	OUTFLOW	STORAGE
	(cms)	(ha.m.)	(cms)	(ha.m.)
	0.0000	0.0000	0.0140	0.0709

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 ( 2000)	1.185	0.200	2.50	64.24
OUTFLOW: ID= 1 ( 20011)	1.185	0.013	4.08	63.16

PEAK FLOW REDUCTION [Qout/Qin](%)= 6.30  
 TIME SHIFT OF PEAK FLOW (min)= 95.00  
 MAXIMUM STORAGE USED (ha.m.)= 0.0638

CALIB			
STANDHYD ( 2011)	Area (ha)=	0.08	
ID= 1 DT= 5.0 min	Total Imp(%)=	73.00	Dir. Conn.(%)= 73.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	0.06	0.02
Dep. Storage (mm)=	1.00	5.00
Average Slope (%)=	1.00	2.00
Length (m)=	22.66	40.00
Mannings n =	0.013	0.250

Max.Eff.Inten.(mm/hr)=	67.16	48.86
over (min)	5.00	15.00
Storage Coeff. (min)=	1.23 (ii)	10.63 (ii)
Unit Hyd. Tpeak (min)=	5.00	15.00
Unit Hyd. peak (cms)=	0.33	0.09

			*TOTALS*
PEAK FLOW (cms)=	0.01	0.00	0.013 (iii)
TIME TO PEAK (hrs)=	2.42	2.58	2.50
RUNOFF VOLUME (mm)=	72.00	40.98	63.55
TOTAL RAINFALL (mm)=	73.00	73.00	73.00
RUNOFF COEFFICIENT =	0.99	0.56	0.87

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD ( 2012)	Area (ha)=	0.03	





| ID= 1 DT= 5.0 min | Total Imp(%)= 65.00 Dir. Conn.(%)= 65.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.02	0.01	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	14.61	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	67.16	48.86	
over (min)	5.00	15.00	
Storage Coeff. (min)=	0.94 (ii)	10.34 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.34	0.09	
			*TOTALS*
PEAK FLOW (cms)=	0.00	0.00	0.005 (iii)
TIME TO PEAK (hrs)=	2.25	2.58	2.50
RUNOFF VOLUME (mm)=	72.00	40.98	61.04
TOTAL RAINFALL (mm)=	73.00	73.00	73.00
RUNOFF COEFFICIENT =	0.99	0.56	0.84

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD ( 2001)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 2001):	1.18	0.013	4.08	63.16
+ ID2= 2 ( 2002):	0.00	0.001	2.50	40.22
=====				
ID = 3 ( 2001):	1.19	0.013	4.08	63.06

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 2001)				
3 + 2 = 1				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 3 ( 2001):	1.19	0.013	4.08	63.06
+ ID2= 2 ( 2011):	0.08	0.013	2.50	63.55
=====				
ID = 1 ( 2001):	1.27	0.022	2.50	63.09



NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 2001)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 ( 2001):	1.27	0.022	2.50	63.09
+ ID2= 2 ( 2012):	0.03	0.005	2.50	61.04
=====				
ID = 3 ( 2001):	1.30	0.027	2.50	63.04

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB STANDHYD ( 0202)	Area (ha)=	0.94
ID= 1 DT= 5.0 min	Total Imp(%)=	70.00 Dir. Conn.(%)= 70.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.66	0.28	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	79.12	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	67.16	48.86	
over (min)	5.00	15.00	
Storage Coeff. (min)=	2.60 (ii)	12.00 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.29	0.09	
			*TOTALS*
PEAK FLOW (cms)=	0.12	0.03	0.152 (iii)
TIME TO PEAK (hrs)=	2.50	2.58	2.50
RUNOFF VOLUME (mm)=	72.00	40.98	62.69
TOTAL RAINFALL (mm)=	73.00	73.00	73.00
RUNOFF COEFFICIENT =	0.99	0.56	0.86

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR( 2020)	OVERFLOW IS OFF			
IN= 2---> OUT= 1				
DT= 5.0 min	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)



	0.0000	0.0000	0.0090	0.0561
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 ( 0202)	0.939	0.152	2.50	62.69
OUTFLOW: ID= 1 ( 2020)	0.939	0.008	4.33	61.00

PEAK FLOW REDUCTION [Qout/Qin](%)= 5.31  
 TIME SHIFT OF PEAK FLOW (min)=110.00  
 MAXIMUM STORAGE USED (ha.m.)= 0.0504

-----  
 -----  
 | CALIB |  
 | STANDHYD ( 2021) | Area (ha)= 0.03  
 | ID= 1 DT= 5.0 min | Total Imp(%)= 65.00 Dir. Conn.(%)= 65.00  
 -----  
 -----

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.02	0.01	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	14.83	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	67.16	48.86	
over (min)	5.00	15.00	
Storage Coeff. (min)=	0.95 (ii)	10.35 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.34	0.09	
			*TOTALS*
PEAK FLOW (cms)=	0.00	0.00	0.005 (iii)
TIME TO PEAK (hrs)=	2.25	2.58	2.50
RUNOFF VOLUME (mm)=	72.00	40.98	61.04
TOTAL RAINFALL (mm)=	73.00	73.00	73.00
RUNOFF COEFFICIENT =	0.99	0.56	0.84

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 -----  
 | CALIB |  
 | STANDHYD ( 2022) | Area (ha)= 0.07  
 | ID= 1 DT= 5.0 min | Total Imp(%)= 99.00 Dir. Conn.(%)= 99.00  
 -----  
 -----

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	0.07	0.00



Dep. Storage	(mm)=	1.00	5.00	
Average Slope	(%)=	1.00	2.00	
Length	(m)=	22.06	40.00	
Mannings n	=	0.013	0.250	
Max.Eff.Inten.(mm/hr)=		67.16	48.86	
over (min)		5.00	5.00	
Storage Coeff. (min)=		1.21 (ii)	2.53 (ii)	
Unit Hyd. Tpeak (min)=		5.00	5.00	
Unit Hyd. peak (cms)=		0.33	0.29	
				*TOTALS*
PEAK FLOW	(cms)=	0.01	0.00	0.014 (iii)
TIME TO PEAK	(hrs)=	2.42	2.50	2.50
RUNOFF VOLUME	(mm)=	72.00	40.98	71.69
TOTAL RAINFALL	(mm)=	73.00	73.00	73.00
RUNOFF COEFFICIENT	=	0.99	0.56	0.98

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD ( 20201)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 2020):	0.94	0.008	4.33	61.00
+ ID2= 2 ( 2021):	0.03	0.005	2.50	61.04
=====				
ID = 3 ( 20201):	0.97	0.011	2.50	61.00

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 20201)				
3 + 2 = 1				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 3 ( 20201):	0.97	0.011	2.50	61.00
+ ID2= 2 ( 2022):	0.07	0.014	2.50	71.69
=====				
ID = 1 ( 20201):	1.04	0.024	2.50	61.75

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.



ADD HYD ( 0002)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 2001):	1.30	0.027	2.50	63.04
+ ID2= 2 ( 20201):	1.04	0.024	2.50	61.75
=====				
ID = 3 ( 0002):	2.34	0.051	2.50	62.46

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB	Area (ha)=	0.07
STANDHYD ( 2071)	Total Imp(%)=	74.00
ID= 1 DT= 5.0 min	Dir. Conn.(%)=	74.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.05	0.02	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	21.29	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	67.16	48.86	
over (min)	5.00	15.00	
Storage Coeff. (min)=	1.18 (ii)	10.58 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.33	0.09	
			*TOTALS*
PEAK FLOW (cms)=	0.01	0.00	0.011 (iii)
TIME TO PEAK (hrs)=	2.42	2.58	2.50
RUNOFF VOLUME (mm)=	72.00	40.98	63.86
TOTAL RAINFALL (mm)=	73.00	73.00	73.00
RUNOFF COEFFICIENT =	0.99	0.56	0.87

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	Area (ha)=	0.56
STANDHYD ( 0207)	Total Imp(%)=	63.00
ID= 1 DT= 5.0 min	Dir. Conn.(%)=	63.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	0.35	0.21
Dep. Storage (mm)=	1.00	5.00
Average Slope (%)=	1.00	2.00



Length	(m)=	61.05	40.00	
Mannings n	=	0.013	0.250	
Max.Eff.Inten.(mm/hr)=		67.16	48.86	
over (min)		5.00	15.00	
Storage Coeff. (min)=		2.23 (ii)	11.63 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		0.30	0.09	
				*TOTALS*
PEAK FLOW (cms)=		0.07	0.02	0.088 (iii)
TIME TO PEAK (hrs)=		2.50	2.58	2.50
RUNOFF VOLUME (mm)=		72.00	40.98	60.51
TOTAL RAINFALL (mm)=		73.00	73.00	73.00
RUNOFF COEFFICIENT =		0.99	0.56	0.83

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----						
RESERVOIR( 2070)		OVERFLOW IS OFF				
IN= 2---> OUT= 1						
DT= 5.0 min						
-----		OUTFLOW	STORAGE		OUTFLOW	STORAGE
		(cms)	(ha.m.)		(cms)	(ha.m.)
		0.0000	0.0000		0.0060	0.0318

	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 ( 0207)	0.559	0.088	2.50	60.51
OUTFLOW: ID= 1 ( 2070)	0.559	0.005	4.17	58.11

PEAK FLOW REDUCTION [Qout/Qin](%)= 6.12  
 TIME SHIFT OF PEAK FLOW (min)=100.00  
 MAXIMUM STORAGE USED (ha.m.)= 0.0284

-----					
ADD HYD ( 20701)					
1 + 2 = 3					
-----		AREA	QPEAK	TPEAK	R.V.
		(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 2070):		0.56	0.005	4.17	58.11
+ ID2= 2 ( 2071):		0.07	0.011	2.50	63.86
=====					
ID = 3 ( 20701):		0.63	0.015	2.50	58.73

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.



-----  
 -----  
 | CALIB |  
 | STANDHYD ( 0204) | Area (ha)= 0.13  
 | ID= 1 DT= 5.0 min | Total Imp(%)= 75.00 Dir. Conn.(%)= 75.00  
 -----  
 -----

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.10	0.03	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	29.10	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	67.16	48.86	
over (min)	5.00	15.00	
Storage Coeff. (min)=	1.43 (ii)	10.83 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.33	0.09	
			*TOTALS*
PEAK FLOW (cms)=	0.02	0.00	0.021 (iii)
TIME TO PEAK (hrs)=	2.42	2.58	2.50
RUNOFF VOLUME (mm)=	72.00	40.98	64.20
TOTAL RAINFALL (mm)=	73.00	73.00	73.00
RUNOFF COEFFICIENT =	0.99	0.56	0.88

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 -----  
 | CALIB |  
 | STANDHYD ( 0208) | Area (ha)= 0.04  
 | ID= 1 DT= 5.0 min | Total Imp(%)= 75.00 Dir. Conn.(%)= 75.00  
 -----  
 -----

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.03	0.01	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	16.93	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	67.16	48.86	
over (min)	5.00	15.00	
Storage Coeff. (min)=	1.03 (ii)	10.43 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.34	0.09	
			*TOTALS*



PEAK FLOW	(cms)=	0.01	0.00	0.007 (iii)
TIME TO PEAK	(hrs)=	2.25	2.58	2.50
RUNOFF VOLUME	(mm)=	72.00	40.98	64.17
TOTAL RAINFALL	(mm)=	73.00	73.00	73.00
RUNOFF COEFFICIENT	=	0.99	0.56	0.88

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD ( 0205)	Area (ha)=	0.22	
ID= 1 DT= 5.0 min	Total Imp(%)=	99.00	Dir. Conn.(%)= 99.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.22	0.00	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	38.38	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	67.16	48.86	
over (min)	5.00	5.00	
Storage Coeff. (min)=	1.69 (ii)	3.00 (ii)	
Unit Hyd. Tpeak (min)=	5.00	5.00	
Unit Hyd. peak (cms)=	0.32	0.28	
			*TOTALS*
PEAK FLOW (cms)=	0.04	0.00	0.041 (iii)
TIME TO PEAK (hrs)=	2.42	2.50	2.50
RUNOFF VOLUME (mm)=	72.00	40.98	71.68
TOTAL RAINFALL (mm)=	73.00	73.00	73.00
RUNOFF COEFFICIENT =	0.99	0.56	0.98

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD ( 0206)	Area (ha)=	0.51	
ID= 1 DT= 5.0 min	Total Imp(%)=	88.00	Dir. Conn.(%)= 88.00

IMPERVIOUS PERVIOUS (i)





Surface Area	(ha)=	0.45	0.06	
Dep. Storage	(mm)=	1.00	5.00	
Average Slope	(%)=	1.00	2.00	
Length	(m)=	58.54	40.00	
Mannings n	=	0.013	0.250	
Max.Eff.Inten.(mm/hr)=		67.16	48.86	
over (min)		5.00	10.00	
Storage Coeff. (min)=		2.17 (ii)	5.90 (ii)	
Unit Hyd. Tpeak (min)=		5.00	10.00	
Unit Hyd. peak (cms)=		0.31	0.15	
				*TOTALS*
PEAK FLOW	(cms)=	0.08	0.01	0.092 (iii)
TIME TO PEAK	(hrs)=	2.50	2.50	2.50
RUNOFF VOLUME	(mm)=	72.00	40.98	68.27
TOTAL RAINFALL	(mm)=	73.00	73.00	73.00
RUNOFF COEFFICIENT	=	0.99	0.56	0.94

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0    Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----				
ADD HYD ( 2060)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 0204):	0.13	0.021	2.50	64.20
+ ID2= 2 ( 0205):	0.22	0.041	2.50	71.68
=====				
ID = 3 ( 2060):	0.35	0.062	2.50	68.95

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----				
ADD HYD ( 2060)				
3 + 2 = 1				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 3 ( 2060):	0.35	0.062	2.50	68.95
+ ID2= 2 ( 0206):	0.51	0.092	2.50	68.27
=====				
ID = 1 ( 2060):	0.86	0.155	2.50	68.54

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.



ADD HYD ( 2060)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 ( 2060):	0.86	0.155	2.50	68.54
+ ID2= 2 ( 0208):	0.04	0.007	2.50	64.17
=====				
ID = 3 ( 2060):	0.90	0.162	2.50	68.34

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR( 20601)	OVERFLOW IS OFF			
IN= 2---> OUT= 1	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
DT= 5.0 min	0.0000	0.0000	0.0120	0.0571

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 ( 2060)	0.905	0.162	2.50	68.34
OUTFLOW: ID= 1 ( 20601)	0.905	0.011	4.08	67.00

PEAK FLOW REDUCTION [Qout/Qin](%)= 6.70  
 TIME SHIFT OF PEAK FLOW (min)= 95.00  
 MAXIMUM STORAGE USED (ha.m.)= 0.0516

CALIB	Area (ha)=	0.05
STANDHYD ( 2061)	Total Imp(%)=	82.00
ID= 1 DT= 5.0 min	Dir. Conn.(%)=	82.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.04	0.01	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	17.32	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	67.16	48.86	
over (min)	5.00	10.00	
Storage Coeff. (min)=	1.05 (ii)	5.56 (ii)	
Unit Hyd. Tpeak (min)=	5.00	10.00	
Unit Hyd. peak (cms)=	0.34	0.16	
			*TOTALS*
PEAK FLOW (cms)=	0.01	0.00	0.008 (iii)
TIME TO PEAK (hrs)=	2.25	2.50	2.50
RUNOFF VOLUME (mm)=	72.00	40.98	66.39
TOTAL RAINFALL (mm)=	73.00	73.00	73.00



RUNOFF COEFFICIENT = 0.99 0.56 0.91

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| ADD HYD ( 20602) |
| 1 + 2 = 3      |
-----
          AREA    QPEAK    TPEAK    R.V.
          (ha)    (cms)    (hrs)    (mm)
ID1= 1 ( 20601):  0.90  0.011  4.08  67.00
+ ID2= 2 ( 2061):  0.05  0.008  2.50  66.39
=====
ID = 3 ( 20602):  0.95  0.016  2.50  66.97
  
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| ADD HYD ( 0003) |
| 1 + 2 = 3      |
-----
          AREA    QPEAK    TPEAK    R.V.
          (ha)    (cms)    (hrs)    (mm)
ID1= 1 ( 0002):  2.34  0.051  2.50  62.46
+ ID2= 2 ( 20602):  0.95  0.016  2.50  66.97
=====
ID = 3 ( 0003):  3.29  0.067  2.50  63.76
  
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| ADD HYD ( 0003) |
| 3 + 2 = 1      |
-----
          AREA    QPEAK    TPEAK    R.V.
          (ha)    (cms)    (hrs)    (mm)
ID1= 3 ( 0003):  3.29  0.067  2.50  63.76
+ ID2= 2 ( 20701):  0.63  0.015  2.50  58.73
=====
ID = 1 ( 0003):  3.92  0.082  2.50  62.96
  
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| CALIB          |
| STANDHYD ( 2201) | Area (ha)= 0.19
| ID= 1 DT= 5.0 min | Total Imp(%)= 99.00 Dir. Conn.(%)= 99.00
-----
  
```



	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.19	0.00	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	35.50	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	67.16	48.86	
over (min)	5.00	5.00	
Storage Coeff. (min)=	1.61 (ii)	2.93 (ii)	
Unit Hyd. Tpeak (min)=	5.00	5.00	
Unit Hyd. peak (cms)=	0.32	0.28	
			*TOTALS*
PEAK FLOW (cms)=	0.03	0.00	0.035 (iii)
TIME TO PEAK (hrs)=	2.50	2.50	2.50
RUNOFF VOLUME (mm)=	72.00	40.98	71.68
TOTAL RAINFALL (mm)=	73.00	73.00	73.00
RUNOFF COEFFICIENT =	0.99	0.56	0.98

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0    Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD ( 0006)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 0003):	3.92	0.082	2.50	62.96
+ ID2= 2 ( 2201):	0.19	0.035	2.50	71.68
=====				
ID = 3 ( 0006):	4.11	0.117	2.50	63.36

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB				
NASHYD ( 2141)				
ID= 1 DT= 5.0 min				
-----				
Area	(ha)=	0.67	Curve Number	(CN)= 85.0
Ia	(mm)=	5.00	# of Linear Res.(N)=	3.00
U.H. Tp	(hrs)=	0.20		

Unit Hyd Qpeak (cms)= 0.128

PEAK FLOW (cms)= 0.075 (i)

TIME TO PEAK (hrs)= 2.500

RUNOFF VOLUME (mm)= 40.906

TOTAL RAINFALL (mm)= 73.000



RUNOFF COEFFICIENT = 0.560

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB |
| STANDHYD ( 2142) | Area (ha)= 0.36
| ID= 1 DT= 5.0 min | Total Imp(%)= 20.00 Dir. Conn.(%)= 5.00
-----

```

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.07	0.29	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	49.14	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	67.16	61.81	
over (min)	5.00	15.00	
Storage Coeff. (min)=	1.96 (ii)	10.51 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.31	0.09	
			*TOTALS*
PEAK FLOW (cms)=	0.00	0.04	0.044 (iii)
TIME TO PEAK (hrs)=	2.50	2.58	2.50
RUNOFF VOLUME (mm)=	72.00	44.42	45.78
TOTAL RAINFALL (mm)=	73.00	73.00	73.00
RUNOFF COEFFICIENT =	0.99	0.61	0.63

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:

CN\* = 85.0 Ia = Dep. Storage (Above)

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| ADD HYD ( 0214) |
| 1 + 2 = 3 | AREA QPEAK TPEAK R.V.
|-----| (ha) (cms) (hrs) (mm)
ID1= 1 ( 2141): 0.67 0.075 2.50 40.91
+ ID2= 2 ( 2142): 0.36 0.044 2.50 45.78
=====
ID = 3 ( 0214): 1.03 0.119 2.50 42.61
-----

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| CALIB |

```



STANDHYD ( 0210)	Area (ha)= 0.14		
ID= 1 DT= 5.0 min	Total Imp(%)= 92.00	Dir. Conn.(%)= 92.00	

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.13	0.01	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	30.44	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	67.16	48.86	
over (min)	5.00	5.00	
Storage Coeff. (min)=	1.47 (ii)	4.58 (ii)	
Unit Hyd. Tpeak (min)=	5.00	5.00	
Unit Hyd. peak (cms)=	0.33	0.23	
			*TOTALS*
PEAK FLOW (cms)=	0.02	0.00	0.025 (iii)
TIME TO PEAK (hrs)=	2.50	2.50	2.50
RUNOFF VOLUME (mm)=	72.00	40.98	69.51
TOTAL RAINFALL (mm)=	73.00	73.00	73.00
RUNOFF COEFFICIENT =	0.99	0.56	0.95

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD ( 0211)	Area (ha)= 0.11		
ID= 1 DT= 5.0 min	Total Imp(%)= 75.00	Dir. Conn.(%)= 75.00	

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.08	0.03	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	26.58	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	67.16	48.86	
over (min)	5.00	15.00	
Storage Coeff. (min)=	1.35 (ii)	10.75 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.33	0.09	
			*TOTALS*
PEAK FLOW (cms)=	0.01	0.00	0.018 (iii)
TIME TO PEAK (hrs)=	2.50	2.58	2.50
RUNOFF VOLUME (mm)=	72.00	40.98	64.17



TOTAL RAINFALL (mm)=	73.00	73.00	73.00
RUNOFF COEFFICIENT =	0.99	0.56	0.88

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	Area (ha)=	0.18	
STANDHYD ( 0203)	Total Imp(%)=	32.00	Dir. Conn.(%)= 32.00
ID= 1 DT= 5.0 min			

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.06	0.12	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	34.74	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	67.16	48.86	
over (min)	5.00	15.00	
Storage Coeff. (min)=	1.59 (ii)	10.99 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.33	0.09	
			*TOTALS*
PEAK FLOW (cms)=	0.01	0.01	0.024 (iii)
TIME TO PEAK (hrs)=	2.42	2.58	2.50
RUNOFF VOLUME (mm)=	72.00	40.98	50.87
TOTAL RAINFALL (mm)=	73.00	73.00	73.00
RUNOFF COEFFICIENT =	0.99	0.56	0.70

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	Area (ha)=	0.68	
STANDHYD ( 0213)	Total Imp(%)=	80.00	Dir. Conn.(%)= 80.00
ID= 1 DT= 5.0 min			

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	0.54	0.14
Dep. Storage (mm)=	1.00	5.00
Average Slope (%)=	1.00	2.00



Length	(m)=	67.18	40.00	
Mannings n	=	0.013	0.250	
Max.Eff.Inten.(mm/hr)=		67.16	48.86	
over (min)		5.00	10.00	
Storage Coeff. (min)=		2.36 (ii)	7.11 (ii)	
Unit Hyd. Tpeak (min)=		5.00	10.00	
Unit Hyd. peak (cms)=		0.30	0.14	
				*TOTALS*
PEAK FLOW	(cms)=	0.10	0.02	0.118 (iii)
TIME TO PEAK	(hrs)=	2.50	2.50	2.50
RUNOFF VOLUME	(mm)=	72.00	40.98	65.79
TOTAL RAINFALL	(mm)=	73.00	73.00	73.00
RUNOFF COEFFICIENT	=	0.99	0.56	0.90

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB				
STANDHYD ( 0212)	Area	(ha)=	0.22	
ID= 1 DT= 5.0 min	Total Imp(%)=	92.00	Dir. Conn.(%)=	92.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	0.20	0.02	
Dep. Storage	(mm)=	1.00	5.00	
Average Slope	(%)=	1.00	2.00	
Length	(m)=	38.04	40.00	
Mannings n	=	0.013	0.250	
Max.Eff.Inten.(mm/hr)=		67.16	48.86	
over (min)		5.00	5.00	
Storage Coeff. (min)=		1.68 (ii)	4.79 (ii)	
Unit Hyd. Tpeak (min)=		5.00	5.00	
Unit Hyd. peak (cms)=		0.32	0.22	
				*TOTALS*
PEAK FLOW	(cms)=	0.04	0.00	0.040 (iii)
TIME TO PEAK	(hrs)=	2.50	2.50	2.50
RUNOFF VOLUME	(mm)=	72.00	40.98	69.51
TOTAL RAINFALL	(mm)=	73.00	73.00	73.00
RUNOFF COEFFICIENT	=	0.99	0.56	0.95

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.





(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD ( 2130)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 0203):	0.18	0.024	2.50	50.87
+ ID2= 2 ( 0210):	0.14	0.025	2.50	69.51
=====				
ID = 3 ( 2130):	0.32	0.049	2.50	58.97

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 2130)	AREA	QPEAK	TPEAK	R.V.
3 + 2 = 1	(ha)	(cms)	(hrs)	(mm)
ID1= 3 ( 2130):	0.32	0.049	2.50	58.97
+ ID2= 2 ( 0211):	0.11	0.018	2.50	64.17
=====				
ID = 1 ( 2130):	0.43	0.067	2.50	60.26

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 2130)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 2130):	0.43	0.067	2.50	60.26
+ ID2= 2 ( 0212):	0.22	0.040	2.50	69.51
=====				
ID = 3 ( 2130):	0.64	0.107	2.50	63.38

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 2130)	AREA	QPEAK	TPEAK	R.V.
3 + 2 = 1	(ha)	(cms)	(hrs)	(mm)
ID1= 3 ( 2130):	0.64	0.107	2.50	63.38
+ ID2= 2 ( 0213):	0.68	0.118	2.50	65.79
=====				
ID = 1 ( 2130):	1.32	0.225	2.50	64.62

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.



-----  
 -----  
 | RESERVOIR( 21301) | OVERFLOW IS OFF  
 | IN= 2---> OUT= 1 |  
DT= 5.0 min

	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	0.0000	0.0000	0.0160	0.0793

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 ( 2130)	1.320	0.225	2.50	64.62
OUTFLOW: ID= 1 ( 21301)	1.320	0.014	4.08	63.66

PEAK FLOW REDUCTION [Qout/Qin](%)= 6.41  
 TIME SHIFT OF PEAK FLOW (min)= 95.00  
 MAXIMUM STORAGE USED (ha.m.)= 0.0714

-----  
 -----  
 | CALIB |  
 | STANDHYD ( 2131) | Area (ha)= 0.12  
 | ID= 1 DT= 5.0 min | Total Imp(%)= 72.00 Dir. Conn.(%)= 72.00  
 -----

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.08	0.03	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	27.69	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	67.16	48.86	
over (min)	5.00	15.00	
Storage Coeff. (min)=	1.39 (ii)	10.79 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.33	0.09	
			*TOTALS*
PEAK FLOW (cms)=	0.02	0.00	0.019 (iii)
TIME TO PEAK (hrs)=	2.42	2.58	2.50
RUNOFF VOLUME (mm)=	72.00	40.98	63.26
TOTAL RAINFALL (mm)=	73.00	73.00	73.00
RUNOFF COEFFICIENT =	0.99	0.56	0.87

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.



```

-----
| ADD HYD ( 21302) |
| 1 + 2 = 3 |
-----

```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 ( 21301):	1.32	0.014	4.08	63.66
+ ID2= 2 ( 2131):	0.12	0.019	2.50	63.26
=====				
ID = 3 ( 21302):	1.43	0.029	2.50	63.63

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| ADD HYD ( 0005) |
| 1 + 2 = 3 |
-----

```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 ( 0006):	4.11	0.117	2.50	63.36
+ ID2= 2 ( 21302):	1.43	0.029	2.50	63.63
=====				
ID = 3 ( 0005):	5.55	0.147	2.50	63.43

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| ADD HYD ( 0005) |
| 3 + 2 = 1 |
-----

```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 3 ( 0005):	5.55	0.147	2.50	63.43
+ ID2= 2 ( 0214):	1.03	0.119	2.50	42.61
=====				
ID = 1 ( 0005):	6.58	0.266	2.50	60.16

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

V V I SSSSS U U A L (v 6.0.2001)
V V I SS U U A A L
V V I SS U U AAAAA L
V V I SS U U A A L
VV I SSSSS UUUUU A A LLLLL

000 TTTTT TTTTT H H Y Y M M 000 TM
0 0 T T H H Y Y MM MM 0 0
0 0 T T H H Y M M 0 0
000 T T H H Y M M 000

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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

Input filename: C:\Program Files (x86)\Visual OTTHYMO 6.0\V02\voin.dat

Output filename:

C:\Users\jliang\AppData\Local\Civica\XH5\becad37f-97fe-4a15-a3fd-f87dd2156d5f\3e3933d6-7cd9-46fb-9044-dbc5d1faba55\scena

Summary filename:

C:\Users\jliang\AppData\Local\Civica\XH5\becad37f-97fe-4a15-a3fd-f87dd2156d5f\3e3933d6-7cd9-46fb-9044-dbc5d1faba55\scena

DATE: 10-27-2021

TIME: 05:35:38

USER:

COMMENTS: \_\_\_\_\_

-----  
 -----  
 \*\*\*\*\*  
 \*\* SIMULATION : Run 06 \*\*  
 \*\*\*\*\*

READ STORM	Filename: C:\Users\jliang\AppData\Local\Temp\907c1cff-ccb1-41c0-9867-a9890799f0d3\40ddf276
Ptotal= 80.31 mm	Comments: 100-Year 6-hour AES Storm

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.25	1.61	1.75	27.30	3.25	11.24	4.75	1.61
0.50	1.61	2.00	27.30	3.50	11.24	5.00	1.61
0.75	1.61	2.25	73.88	3.75	6.42	5.25	1.61
1.00	1.61	2.50	73.88	4.00	6.42	5.50	1.61
1.25	9.64	2.75	20.88	4.25	3.21	5.75	1.61
1.50	9.64	3.00	20.88	4.50	3.21	6.00	1.61



CALIB			
NASHYD ( 2002)	Area (ha)=	0.00	Curve Number (CN)= 85.0
ID= 1 DT= 5.0 min	Ia (mm)=	5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)=	0.20	

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

---- TRANSFORMED HYETOGRAPH ----

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.083	1.61	1.583	27.30	3.083	11.24	4.58	1.61
0.167	1.61	1.667	27.30	3.167	11.24	4.67	1.61
0.250	1.61	1.750	27.30	3.250	11.24	4.75	1.61
0.333	1.61	1.833	27.30	3.333	11.24	4.83	1.61
0.417	1.61	1.917	27.30	3.417	11.24	4.92	1.61
0.500	1.61	2.000	27.30	3.500	11.24	5.00	1.61
0.583	1.61	2.083	73.88	3.583	6.42	5.08	1.61
0.667	1.61	2.167	73.88	3.667	6.42	5.17	1.61
0.750	1.61	2.250	73.88	3.750	6.42	5.25	1.61
0.833	1.61	2.333	73.88	3.833	6.42	5.33	1.61
0.917	1.61	2.417	73.88	3.917	6.42	5.42	1.61
1.000	1.61	2.500	73.88	4.000	6.42	5.50	1.61
1.083	9.64	2.583	20.88	4.083	3.21	5.58	1.61
1.167	9.64	2.667	20.88	4.167	3.21	5.67	1.61
1.250	9.64	2.750	20.88	4.250	3.21	5.75	1.61
1.333	9.64	2.833	20.88	4.333	3.21	5.83	1.61
1.417	9.64	2.917	20.88	4.417	3.21	5.92	1.61
1.500	9.64	3.000	20.88	4.500	3.21	6.00	1.61

Unit Hyd Qpeak (cms)= 0.001

PEAK FLOW (cms)= 0.001 (i)

TIME TO PEAK (hrs)= 2.500

RUNOFF VOLUME (mm)= 46.329

TOTAL RAINFALL (mm)= 80.310

RUNOFF COEFFICIENT = 0.577

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD ( 0201)	Area (ha)=	0.73	
ID= 1 DT= 5.0 min	Total Imp(%)=	80.00	Dir. Conn.(%)= 80.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	0.58	0.15
Dep. Storage (mm)=	1.00	5.00
Average Slope (%)=	1.00	2.00



Length	(m)=	69.71	40.00	
Mannings n	=	0.013	0.250	
Max.Eff.Inten.(mm/hr)=		73.88	55.75	
over (min)		5.00	10.00	
Storage Coeff. (min)=		2.32 (ii)	6.90 (ii)	
Unit Hyd. Tpeak (min)=		5.00	10.00	
Unit Hyd. peak (cms)=		0.30	0.14	
				*TOTALS*
PEAK FLOW (cms)=		0.12	0.02	0.141 (iii)
TIME TO PEAK (hrs)=		2.50	2.50	2.50
RUNOFF VOLUME (mm)=		79.31	47.21	72.89
TOTAL RAINFALL (mm)=		80.31	80.31	80.31
RUNOFF COEFFICIENT =		0.99	0.59	0.91

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB				
STANDHYD ( 0200)	Area (ha)=	0.46		
ID= 1 DT= 5.0 min	Total Imp(%)=	67.00	Dir. Conn.(%)=	67.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	0.31	0.15	
Dep. Storage	(mm)=	1.00	5.00	
Average Slope	(%)=	1.00	2.00	
Length	(m)=	55.14	40.00	
Mannings n	=	0.013	0.250	
Max.Eff.Inten.(mm/hr)=		73.88	55.75	
over (min)		5.00	15.00	
Storage Coeff. (min)=		2.02 (ii)	10.93 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		0.31	0.09	
				*TOTALS*
PEAK FLOW (cms)=		0.06	0.02	0.081 (iii)
TIME TO PEAK (hrs)=		2.50	2.58	2.50
RUNOFF VOLUME (mm)=		79.31	47.21	68.71
TOTAL RAINFALL (mm)=		80.31	80.31	80.31
RUNOFF COEFFICIENT =		0.99	0.59	0.86

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.



(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD ( 2000)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 ( 0200):	0.46	0.081	2.50	68.71
+ ID2= 2 ( 0201):	0.73	0.141	2.50	72.89
=====				
ID = 3 ( 2000):	1.18	0.222	2.50	71.28

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR( 20011)	OVERFLOW IS OFF			
IN= 2---> OUT= 1	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
DT= 5.0 min	0.0000	0.0000	0.0140	0.0709

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 ( 2000)	1.185	0.222	2.50	71.28
OUTFLOW: ID= 1 ( 20011)	1.185	0.014	4.08	70.19

PEAK FLOW REDUCTION [Qout/Qin](%)= 6.29  
 TIME SHIFT OF PEAK FLOW (min)= 95.00  
 MAXIMUM STORAGE USED (ha.m.)= 0.0708

CALIB	Area (ha)=	PERVIOUS (i)
STANDHYD ( 2011)	0.08	
ID= 1 DT= 5.0 min	Total Imp(%)= 73.00	Dir. Conn.(%)= 73.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	0.06	0.02
Dep. Storage (mm)=	1.00	5.00
Average Slope (%)=	1.00	2.00
Length (m)=	22.66	40.00
Mannings n =	0.013	0.250
Max.Eff.Inten.(mm/hr)=	73.88	55.75
over (min)	5.00	15.00
Storage Coeff. (min)=	1.18 (ii)	10.10 (ii)
Unit Hyd. Tpeak (min)=	5.00	15.00
Unit Hyd. peak (cms)=	0.33	0.10

\*TOTALS\*



PEAK FLOW	(cms)=	0.01	0.00	0.014 (iii)
TIME TO PEAK	(hrs)=	2.50	2.58	2.50
RUNOFF VOLUME	(mm)=	79.31	47.21	70.56
TOTAL RAINFALL	(mm)=	80.31	80.31	80.31
RUNOFF COEFFICIENT	=	0.99	0.59	0.88

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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CALIB				
STANDHYD ( 2012)		Area (ha)=	0.03	
ID= 1 DT= 5.0 min		Total Imp(%)=	65.00	Dir. Conn.(%)= 65.00
-----				

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	0.02	0.01	
Dep. Storage	(mm)=	1.00	5.00	
Average Slope	(%)=	1.00	2.00	
Length	(m)=	14.61	40.00	
Mannings n	=	0.013	0.250	
Max.Eff.Inten.(mm/hr)=		73.88	55.75	
over (min)		5.00	10.00	
Storage Coeff. (min)=		0.91 (ii)	9.83 (ii)	
Unit Hyd. Tpeak (min)=		5.00	10.00	
Unit Hyd. peak (cms)=		0.34	0.11	
				*TOTALS*
PEAK FLOW	(cms)=	0.00	0.00	0.006 (iii)
TIME TO PEAK	(hrs)=	2.25	2.50	2.50
RUNOFF VOLUME	(mm)=	79.31	47.21	67.99
TOTAL RAINFALL	(mm)=	80.31	80.31	80.31
RUNOFF COEFFICIENT	=	0.99	0.59	0.85

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----				
-----				
ADD HYD ( 2001)				
1 + 2 = 3		AREA	QPEAK	TPEAK
		(ha)	(cms)	(hrs)
				R.V.
				(mm)
ID1= 1 ( 20011):		1.18	0.014	4.08
				70.19
-----				





+ ID2= 2 ( 2002):	0.00	0.001	2.50	46.33
=====				
ID = 3 ( 2001):	1.19	0.014	4.08	70.09

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----

ADD HYD ( 2001)				
3 + 2 = 1	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 3 ( 2001):	1.19	0.014	4.08	70.09
+ ID2= 2 ( 2011):	0.08	0.014	2.50	70.56
=====				
ID = 1 ( 2001):	1.27	0.025	2.50	70.12

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----

ADD HYD ( 2001)				
1 + 2 = 3	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 2001):	1.27	0.025	2.50	70.12
+ ID2= 2 ( 2012):	0.03	0.006	2.50	67.99
=====				
ID = 3 ( 2001):	1.30	0.030	2.50	70.07

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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CALIB			
STANDHYD ( 0202)	Area (ha)=	0.94	
ID= 1 DT= 5.0 min	Total Imp(%)=	70.00	Dir. Conn.(%)= 70.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	0.66	0.28	
Dep. Storage	(mm)=	1.00	5.00	
Average Slope	(%)=	1.00	2.00	
Length	(m)=	79.12	40.00	
Mannings n	=	0.013	0.250	
Max.Eff.Inten.(mm/hr)=		73.88	55.75	
over (min)		5.00	15.00	
Storage Coeff. (min)=		2.51 (ii)	11.42 (ii)	
Unit Hyd. Tpeak (min)=		5.00	15.00	
Unit Hyd. peak (cms)=		0.29	0.09	
				*TOTALS*
PEAK FLOW	(cms)=	0.13	0.04	0.170 (iii)
TIME TO PEAK	(hrs)=	2.50	2.58	2.50



RUNOFF VOLUME (mm)=	79.31	47.21	69.67
TOTAL RAINFALL (mm)=	80.31	80.31	80.31
RUNOFF COEFFICIENT =	0.99	0.59	0.87

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR( 2020)		OVERFLOW IS OFF			
IN= 2---> OUT= 1		OUTFLOW		STORAGE	
DT= 5.0 min		(cms)	(ha.m.)	(cms)	(ha.m.)
		0.0000	0.0000	0.0090	0.0561
		AREA	QPEAK	TPEAK	R.V.
		(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 ( 0202)		0.939	0.170	2.50	69.67
OUTFLOW: ID= 1 ( 2020)		0.939	0.009	4.25	67.99
PEAK FLOW REDUCTION [Qout/Qin](%)=		5.30			
TIME SHIFT OF PEAK FLOW (min)=		105.00			
MAXIMUM STORAGE USED (ha.m.)=		0.0560			

CALIB		STANDHYD ( 2021)		
ID= 1 DT= 5.0 min		Area (ha)=	Total Imp(%)=	Dir. Conn.(%)=
		0.03	65.00	65.00
		IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=		0.02	0.01	
Dep. Storage (mm)=		1.00	5.00	
Average Slope (%)=		1.00	2.00	
Length (m)=		14.83	40.00	
Mannings n =		0.013	0.250	
Max.Eff.Inten.(mm/hr)=		73.88	55.75	
over (min)		5.00	10.00	
Storage Coeff. (min)=		0.92 (ii)	9.83 (ii)	
Unit Hyd. Tpeak (min)=		5.00	10.00	
Unit Hyd. peak (cms)=		0.34	0.11	
*TOTALS*				
PEAK FLOW (cms)=		0.00	0.00	0.006 (iii)
TIME TO PEAK (hrs)=		2.25	2.50	2.50
RUNOFF VOLUME (mm)=		79.31	47.21	67.99
TOTAL RAINFALL (mm)=		80.31	80.31	80.31



RUNOFF COEFFICIENT = 0.99 0.59 0.85

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | CALIB |  
 | STANDHYD ( 2022) | Area (ha)= 0.07  
 | ID= 1 DT= 5.0 min | Total Imp(%)= 99.00 Dir. Conn.(%)= 99.00  
 -----

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.07	0.00	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	22.06	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	73.88	55.75	
over (min)	5.00	5.00	
Storage Coeff. (min)=	1.16 (ii)	2.43 (ii)	
Unit Hyd. Tpeak (min)=	5.00	5.00	
Unit Hyd. peak (cms)=	0.34	0.30	
			*TOTALS*
PEAK FLOW (cms)=	0.01	0.00	0.015 (iii)
TIME TO PEAK (hrs)=	2.42	2.50	2.50
RUNOFF VOLUME (mm)=	79.31	47.21	78.99
TOTAL RAINFALL (mm)=	80.31	80.31	80.31
RUNOFF COEFFICIENT =	0.99	0.59	0.98

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 | ADD HYD ( 20201) |  
 | 1 + 2 = 3 | AREA QPEAK TPEAK R.V.  
 | | (ha) (cms) (hrs) (mm)  
 ID1= 1 ( 2020): 0.94 0.009 4.25 67.99  
 + ID2= 2 ( 2021): 0.03 0.006 2.50 67.99  
 =====  
 ID = 3 ( 20201): 0.97 0.012 2.50 67.99  
 -----



NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 20201)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
3 + 2 = 1				
ID1= 3 ( 20201):	0.97	0.012	2.50	67.99
+ ID2= 2 ( 2022):	0.07	0.015	2.50	78.99
=====				
ID = 1 ( 20201):	1.04	0.027	2.50	68.76

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 0002)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 ( 2001):	1.30	0.030	2.50	70.07
+ ID2= 2 ( 20201):	1.04	0.027	2.50	68.76
=====				
ID = 3 ( 0002):	2.34	0.057	2.50	69.48

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB	Area (ha)=	Imp(%)=	Dir. Conn.(%)=
STANDHYD ( 2071)	0.07		
ID= 1 DT= 5.0 min		74.00	74.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.05	0.02	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	21.29	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	73.88	55.75	
over (min)	5.00	15.00	
Storage Coeff. (min)=	1.14 (ii)	10.06 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.34	0.10	
			*TOTALS*
PEAK FLOW (cms)=	0.01	0.00	0.013 (iii)
TIME TO PEAK (hrs)=	2.42	2.58	2.50
RUNOFF VOLUME (mm)=	79.31	47.21	70.88
TOTAL RAINFALL (mm)=	80.31	80.31	80.31
RUNOFF COEFFICIENT =	0.99	0.59	0.88



- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD ( 0207)	Area (ha)=	0.56	
ID= 1 DT= 5.0 min	Total Imp(%)=	63.00	Dir. Conn.(%)= 63.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.35	0.21	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	61.05	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	73.88	55.75	
over (min)	5.00	15.00	
Storage Coeff. (min)=	2.14 (ii)	11.06 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.31	0.09	
			*TOTALS*
PEAK FLOW (cms)=	0.07	0.03	0.098 (iii)
TIME TO PEAK (hrs)=	2.50	2.58	2.50
RUNOFF VOLUME (mm)=	79.31	47.21	67.42
TOTAL RAINFALL (mm)=	80.31	80.31	80.31
RUNOFF COEFFICIENT =	0.99	0.59	0.84

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR( 2070)	OVERFLOW IS OFF			
IN= 2---> OUT= 1				
DT= 5.0 min	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	0.0000	0.0000	0.0060	0.0318

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 ( 0207)	0.559	0.098	2.50	67.42
OUTFLOW: ID= 1 ( 2070)	0.559	0.006	4.17	65.02



PEAK FLOW REDUCTION [Qout/Qin](%)= 6.10  
 TIME SHIFT OF PEAK FLOW (min)=100.00  
 MAXIMUM STORAGE USED (ha.m.)= 0.0317

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 -----  
 | ADD HYD ( 20701) |  
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 ( 2070):	0.56	0.006	4.17	65.02
+ ID2= 2 ( 2071):	0.07	0.013	2.50	70.88
=====				
ID = 3 ( 20701):	0.63	0.016	2.50	65.65

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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 -----  
 | CALIB |  
 | STANDHYD ( 0204) |  
ID= 1 DT= 5.0 min

Area (ha)=	0.13		
Total Imp(%)=	75.00	Dir. Conn.(%)=	75.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.10	0.03	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	29.10	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	73.88	55.75	
over (min)	5.00	15.00	
Storage Coeff. (min)=	1.37 (ii)	10.29 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.33	0.09	
			*TOTALS*
PEAK FLOW (cms)=	0.02	0.00	0.024 (iii)
TIME TO PEAK (hrs)=	2.42	2.58	2.50
RUNOFF VOLUME (mm)=	79.31	47.21	71.23
TOTAL RAINFALL (mm)=	80.31	80.31	80.31
RUNOFF COEFFICIENT =	0.99	0.59	0.89

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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 -----  
CALIB



STANDHYD ( 0208)	Area (ha)= 0.04		
ID= 1 DT= 5.0 min	Total Imp(%)= 75.00	Dir. Conn.(%)= 75.00	

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.03	0.01	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	16.93	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	73.88	55.75	
over (min)	5.00	10.00	
Storage Coeff. (min)=	0.99 (ii)	9.91 (ii)	
Unit Hyd. Tpeak (min)=	5.00	10.00	
Unit Hyd. peak (cms)=	0.34	0.11	
			*TOTALS*
PEAK FLOW (cms)=	0.01	0.00	0.008 (iii)
TIME TO PEAK (hrs)=	2.25	2.50	2.50
RUNOFF VOLUME (mm)=	79.31	47.21	71.22
TOTAL RAINFALL (mm)=	80.31	80.31	80.31
RUNOFF COEFFICIENT =	0.99	0.59	0.89

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0    Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB			
STANDHYD ( 0205)	Area (ha)= 0.22		
ID= 1 DT= 5.0 min	Total Imp(%)= 99.00	Dir. Conn.(%)= 99.00	

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.22	0.00	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	38.38	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	73.88	55.75	
over (min)	5.00	5.00	
Storage Coeff. (min)=	1.62 (ii)	2.89 (ii)	
Unit Hyd. Tpeak (min)=	5.00	5.00	
Unit Hyd. peak (cms)=	0.32	0.28	
			*TOTALS*
PEAK FLOW (cms)=	0.04	0.00	0.045 (iii)
TIME TO PEAK (hrs)=	2.50	2.50	2.50
RUNOFF VOLUME (mm)=	79.31	47.21	78.98



TOTAL RAINFALL (mm)=	80.31	80.31	80.31
RUNOFF COEFFICIENT =	0.99	0.59	0.98

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	Area (ha)=	0.51		
STANDHYD ( 0206)	Total Imp(%)=	88.00	Dir. Conn.(%)=	88.00
ID= 1 DT= 5.0 min				

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.45	0.06	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	58.54	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	73.88	55.75	
over (min)	5.00	10.00	
Storage Coeff. (min)=	2.09 (ii)	5.68 (ii)	
Unit Hyd. Tpeak (min)=	5.00	10.00	
Unit Hyd. peak (cms)=	0.31	0.15	
			*TOTALS*
PEAK FLOW (cms)=	0.09	0.01	0.102 (iii)
TIME TO PEAK (hrs)=	2.50	2.50	2.50
RUNOFF VOLUME (mm)=	79.31	47.21	75.45
TOTAL RAINFALL (mm)=	80.31	80.31	80.31
RUNOFF COEFFICIENT =	0.99	0.59	0.94

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD ( 2060)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 0204):	0.13	0.024	2.50	71.23
+ ID2= 2 ( 0205):	0.22	0.045	2.50	78.98
=====				
ID = 3 ( 2060):	0.35	0.069	2.50	76.15





NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 2060)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
3 + 2 = 1				
ID1= 3 ( 2060):	0.35	0.069	2.50	76.15
+ ID2= 2 ( 0206):	0.51	0.102	2.50	75.45
ID = 1 ( 2060):	0.86	0.171	2.50	75.73

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 2060)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 ( 2060):	0.86	0.171	2.50	75.73
+ ID2= 2 ( 0208):	0.04	0.008	2.50	71.22
ID = 3 ( 2060):	0.90	0.179	2.50	75.52

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR( 20601)	OVERFLOW IS OFF			
IN= 2---> OUT= 1	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
DT= 5.0 min	0.0000	0.0000	0.0120	0.0571

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 2 ( 2060)	0.905	0.179	2.50	75.52
OUTFLOW: ID= 1 ( 20601)	0.905	0.012	4.08	74.19

PEAK FLOW REDUCTION [Qout/Qin](%)= 6.70  
 TIME SHIFT OF PEAK FLOW (min)= 95.00  
 MAXIMUM STORAGE USED (ha.m.)= 0.0570

CALIB	Area (ha)=	Dir. Conn.(%)=
STANDHYD ( 2061)	0.05	82.00
ID= 1 DT= 5.0 min	Total Imp(%)= 82.00	Dir. Conn.(%)= 82.00

IMPERVIOUS PERVIOUS (i)



Surface Area	(ha)=	0.04	0.01	
Dep. Storage	(mm)=	1.00	5.00	
Average Slope	(%)=	1.00	2.00	
Length	(m)=	17.32	40.00	
Mannings n	=	0.013	0.250	
Max.Eff.Inten.(mm/hr)=		73.88	55.75	
over (min)		5.00	10.00	
Storage Coeff. (min)=		1.01 (ii)	5.35 (ii)	
Unit Hyd. Tpeak (min)=		5.00	10.00	
Unit Hyd. peak (cms)=		0.34	0.16	
				*TOTALS*
PEAK FLOW	(cms)=	0.01	0.00	0.009 (iii)
TIME TO PEAK	(hrs)=	2.25	2.50	2.50
RUNOFF VOLUME	(mm)=	79.31	47.21	73.51
TOTAL RAINFALL	(mm)=	80.31	80.31	80.31
RUNOFF COEFFICIENT	=	0.99	0.59	0.92

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD ( 20602)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 20601):	0.90	0.012	4.08	74.19
+ ID2= 2 ( 2061):	0.05	0.009	2.50	73.51
=====				
ID = 3 ( 20602):	0.95	0.018	2.50	74.15

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD ( 0003)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 0002):	2.34	0.057	2.50	69.48
+ ID2= 2 ( 20602):	0.95	0.018	2.50	74.15
=====				
ID = 3 ( 0003):	3.29	0.075	2.50	70.83

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.



ADD HYD ( 0003)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
3 + 2 = 1				
ID1= 3 ( 0003):	3.29	0.075	2.50	70.83
+ ID2= 2 ( 20701):	0.63	0.016	2.50	65.65
=====				
ID = 1 ( 0003):	3.92	0.091	2.50	70.00

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB	Area (ha)=	Dir. Conn.(%)=
STANDHYD ( 2201)	0.19	
ID= 1 DT= 5.0 min	Total Imp(%)= 99.00	99.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.19	0.00	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	35.50	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	73.88	55.75	
over (min)	5.00	5.00	
Storage Coeff. (min)=	1.55 (ii)	2.82 (ii)	
Unit Hyd. Tpeak (min)=	5.00	5.00	
Unit Hyd. peak (cms)=	0.33	0.28	
			*TOTALS*
PEAK FLOW (cms)=	0.04	0.00	0.039 (iii)
TIME TO PEAK (hrs)=	2.42	2.50	2.50
RUNOFF VOLUME (mm)=	79.31	47.21	78.98
TOTAL RAINFALL (mm)=	80.31	80.31	80.31
RUNOFF COEFFICIENT =	0.99	0.59	0.98

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD ( 0006)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 ( 0003):	3.92	0.091	2.50	70.00
+ ID2= 2 ( 2201):	0.19	0.039	2.50	78.98
=====				



ID = 3 ( 0006): 4.11 0.130 2.50 70.41

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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-----
| CALIB |
| NASHYD ( 2141) | Area (ha)= 0.67 Curve Number (CN)= 85.0
| ID= 1 DT= 5.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00
-----
| U.H. Tp(hrs)= 0.20

```

Unit Hyd Qpeak (cms)= 0.128

PEAK FLOW (cms)= 0.086 (i)  
 TIME TO PEAK (hrs)= 2.500  
 RUNOFF VOLUME (mm)= 47.120  
 TOTAL RAINFALL (mm)= 80.310  
 RUNOFF COEFFICIENT = 0.587

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
| CALIB |
| STANDHYD ( 2142) | Area (ha)= 0.36
| ID= 1 DT= 5.0 min | Total Imp(%)= 20.00 Dir. Conn.(%)= 5.00
-----

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	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.07	0.29	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	49.14	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	73.88	70.09	
over (min)	5.00	15.00	
Storage Coeff. (min)=	1.88 (ii)	10.02 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.32	0.10	
			*TOTALS*
PEAK FLOW (cms)=	0.00	0.05	0.051 (iii)
TIME TO PEAK (hrs)=	2.42	2.50	2.50
RUNOFF VOLUME (mm)=	79.31	50.87	52.27
TOTAL RAINFALL (mm)=	80.31	80.31	80.31
RUNOFF COEFFICIENT =	0.99	0.63	0.65

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:

CN\* = 85.0 Ia = Dep. Storage (Above)

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.



ADD HYD ( 0214)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 2141):	0.67	0.086	2.50	47.12
+ ID2= 2 ( 2142):	0.36	0.051	2.50	52.27
=====				
ID = 3 ( 0214):	1.03	0.137	2.50	48.92

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB	Area	(ha)=	0.14
STANDHYD ( 0210)	Total Imp(%)=	92.00	Dir. Conn.(%)= 92.00
ID= 1 DT= 5.0 min			

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.13	0.01	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	30.44	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	73.88	55.75	
over (min)	5.00	5.00	
Storage Coeff. (min)=	1.41 (ii)	4.41 (ii)	
Unit Hyd. Tpeak (min)=	5.00	5.00	
Unit Hyd. peak (cms)=	0.33	0.23	
			*TOTALS*
PEAK FLOW (cms)=	0.03	0.00	0.028 (iii)
TIME TO PEAK (hrs)=	2.42	2.50	2.50
RUNOFF VOLUME (mm)=	79.31	47.21	76.73
TOTAL RAINFALL (mm)=	80.31	80.31	80.31
RUNOFF COEFFICIENT =	0.99	0.59	0.96

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	Area	(ha)=	0.11
STANDHYD ( 0211)	Total Imp(%)=	75.00	Dir. Conn.(%)= 75.00
ID= 1 DT= 5.0 min			



	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.08	0.03	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	26.58	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	73.88	55.75	
over (min)	5.00	15.00	
Storage Coeff. (min)=	1.30 (ii)	10.22 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.33	0.09	
			*TOTALS*
PEAK FLOW (cms)=	0.02	0.00	0.020 (iii)
TIME TO PEAK (hrs)=	2.42	2.58	2.50
RUNOFF VOLUME (mm)=	79.31	47.21	71.23
TOTAL RAINFALL (mm)=	80.31	80.31	80.31
RUNOFF COEFFICIENT =	0.99	0.59	0.89

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0    Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB		Area (ha)= 0.18	
STANDHYD ( 0203)		Total Imp(%)= 32.00	Dir. Conn.(%)= 32.00
ID= 1 DT= 5.0 min			

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.06	0.12	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	34.74	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	73.88	55.75	
over (min)	5.00	15.00	
Storage Coeff. (min)=	1.53 (ii)	10.45 (ii)	
Unit Hyd. Tpeak (min)=	5.00	15.00	
Unit Hyd. peak (cms)=	0.33	0.09	
			*TOTALS*
PEAK FLOW (cms)=	0.01	0.02	0.027 (iii)
TIME TO PEAK (hrs)=	2.50	2.58	2.50
RUNOFF VOLUME (mm)=	79.31	47.21	57.45
TOTAL RAINFALL (mm)=	80.31	80.31	80.31
RUNOFF COEFFICIENT =	0.99	0.59	0.72



- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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 -----  

CALIB			
STANDHYD ( 0213)	Area (ha)=	0.68	
ID= 1 DT= 5.0 min	Total Imp(%)=	80.00	Dir. Conn.(%)= 80.00

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 -----

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.54	0.14	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	67.18	40.00	
Mannings n =	0.013	0.250	
Max.Eff.Inten.(mm/hr)=	73.88	55.75	
over (min)	5.00	10.00	
Storage Coeff. (min)=	2.27 (ii)	6.85 (ii)	
Unit Hyd. Tpeak (min)=	5.00	10.00	
Unit Hyd. peak (cms)=	0.30	0.14	
			*TOTALS*
PEAK FLOW (cms)=	0.11	0.02	0.131 (iii)
TIME TO PEAK (hrs)=	2.50	2.50	2.50
RUNOFF VOLUME (mm)=	79.31	47.21	72.88
TOTAL RAINFALL (mm)=	80.31	80.31	80.31
RUNOFF COEFFICIENT =	0.99	0.59	0.91

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0 Ia = Dep. Storage (Above)  
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.  
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 -----  

CALIB			
STANDHYD ( 0212)	Area (ha)=	0.22	
ID= 1 DT= 5.0 min	Total Imp(%)=	92.00	Dir. Conn.(%)= 92.00

 -----  
 -----

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	0.20	0.02	
Dep. Storage (mm)=	1.00	5.00	
Average Slope (%)=	1.00	2.00	
Length (m)=	38.04	40.00	
Mannings n =	0.013	0.250	



Max.Eff.Inten.(mm/hr)=	73.88	55.75	
over (min)	5.00	5.00	
Storage Coeff. (min)=	1.61 (ii)	4.61 (ii)	
Unit Hyd. Tpeak (min)=	5.00	5.00	
Unit Hyd. peak (cms)=	0.32	0.22	
			*TOTALS*
PEAK FLOW (cms)=	0.04	0.00	0.044 (iii)
TIME TO PEAK (hrs)=	2.42	2.50	2.50
RUNOFF VOLUME (mm)=	79.31	47.21	76.73
TOTAL RAINFALL (mm)=	80.31	80.31	80.31
RUNOFF COEFFICIENT =	0.99	0.59	0.96

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
 CN\* = 85.0    Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| ADD HYD ( 2130) |
| 1 + 2 = 3 |
-----

```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 ( 0203):	0.18	0.027	2.50	57.45
+ ID2= 2 ( 0210):	0.14	0.028	2.50	76.73
=====				
ID = 3 ( 2130):	0.32	0.055	2.50	65.82

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| ADD HYD ( 2130) |
| 3 + 2 = 1 |
-----

```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 3 ( 2130):	0.32	0.055	2.50	65.82
+ ID2= 2 ( 0211):	0.11	0.020	2.50	71.23
=====				
ID = 1 ( 2130):	0.43	0.075	2.50	67.17

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
| ADD HYD ( 2130) |
| 1 + 2 = 3 |
-----

```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 ( 2130):	0.43	0.075	2.50	67.17
+ ID2= 2 ( 0212):	0.22	0.044	2.50	76.73





```
=====
ID = 3 ( 2130):    0.64    0.119    2.50    70.40
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```
-----
| ADD HYD ( 2130) |
| 3 + 2 = 1 |
-----
          AREA    QPEAK    TPEAK    R.V.
          (ha)    (cms)    (hrs)    (mm)
ID1= 3 ( 2130):    0.64    0.119    2.50    70.40
+ ID2= 2 ( 0213):    0.68    0.131    2.50    72.88
=====
ID = 1 ( 2130):    1.32    0.249    2.50    71.67
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```
-----
| RESERVOIR( 21301) | OVERFLOW IS OFF
| IN= 2---> OUT= 1 |
| DT= 5.0 min |
-----
          OUTFLOW    STORAGE    |    OUTFLOW    STORAGE
          (cms)    (ha.m.)    |    (cms)    (ha.m.)
          0.0000    0.0000    |    0.0160    0.0793
```

```

          AREA    QPEAK    TPEAK    R.V.
          (ha)    (cms)    (hrs)    (mm)
INFLOW : ID= 2 ( 2130)    1.320    0.249    2.50    71.67
OUTFLOW: ID= 1 ( 21301)    1.320    0.016    4.08    70.72
```

```

PEAK FLOW REDUCTION [Qout/Qin](%)= 6.40
TIME SHIFT OF PEAK FLOW (min)= 95.00
MAXIMUM STORAGE USED (ha.m.)= 0.0792
```

```
-----
| CALIB |
| STANDHYD ( 2131) | Area (ha)= 0.12
| ID= 1 DT= 5.0 min | Total Imp(%)= 72.00 Dir. Conn.(%)= 72.00
-----
```

```

          IMPERVIOUS    PERVIOUS (i)
Surface Area (ha)=    0.08    0.03
Dep. Storage (mm)=    1.00    5.00
Average Slope (%)=    1.00    2.00
Length (m)=    27.69    40.00
Mannings n =    0.013    0.250

Max.Eff.Inten.(mm/hr)=    73.88    55.75
over (min)    5.00    15.00
Storage Coeff. (min)=    1.33 (ii)    10.25 (ii)
Unit Hyd. Tpeak (min)=    5.00    15.00
```



Unit Hyd. peak (cms)=	0.33	0.09	
			*TOTALS*
PEAK FLOW (cms)=	0.02	0.00	0.021 (iii)
TIME TO PEAK (hrs)=	2.42	2.58	2.50
RUNOFF VOLUME (mm)=	79.31	47.21	70.26
TOTAL RAINFALL (mm)=	80.31	80.31	80.31
RUNOFF COEFFICIENT =	0.99	0.59	0.87

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 85.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----				
ADD HYD ( 21302)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 21301):	1.32	0.016	4.08	70.72
+ ID2= 2 ( 2131):	0.12	0.021	2.50	70.26
=====				
ID = 3 ( 21302):	1.43	0.032	2.50	70.68

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----				
ADD HYD ( 0005)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 ( 0006):	4.11	0.130	2.50	70.41
+ ID2= 2 ( 21302):	1.43	0.032	2.50	70.68
=====				
ID = 3 ( 0005):	5.55	0.163	2.50	70.48

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----				
ADD HYD ( 0005)				
3 + 2 = 1				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 3 ( 0005):	5.55	0.163	2.50	70.48
+ ID2= 2 ( 0214):	1.03	0.137	2.50	48.92
=====				
ID = 1 ( 0005):	6.58	0.300	2.50	67.09

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.