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Transportation Planning

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Site Servicing and Grading

Stormwater Management

Municipal Road Design

# Functional Servicing and Storm Water Management Report

Proposed 10 Units Townhouse Development

86 Thomas Street  
Mississauga, Ontario

August 16 2020  
Project No:NT-19-013

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## 1.0 INTRODUCTION

This Functional Servicing & Stormwater Management Report has been prepared in support of the Rezoning (ZBA) and Site Plan Control Application (SPCA) for the proposed 10 units stacked townhouses development at 86 Thomas Street, in Mississauga, Peel Region.

The purpose of this report is to identify and document how the proposed development will be serviced by the City's existing municipal infrastructure (i.e. water, storm and sanitary) and the measures to be used to provide appropriate stormwater management.

## 2.0 SITE LOCATION & EXISTING CONDITIONS

The subject site is approximately 0.1643 hectares in area and is located at the northwest corner of Thomas Street and Hillside Drive, as shown in **Figure 1 after the report**.

The subject site is bounded by:

- Townhouse development on 80 Thomas St. to the north and east (Dunpar Development).
- Existing residential property to the west.
- Thomas Street to the south.

## 3.0 PROPOSED DEVELOPMENT

The proposed development consists of 10 units townhouses, as shown in the Site Plan contained in **Appendix A**.

## 4.0 MUNICIPAL SERVICING

### 4.1 WATER

#### 4.1.1 Design Criteria

|                         |                     |
|-------------------------|---------------------|
| Type of Construction    | Residential         |
| Average Day Consumption | 280 L/person/day    |
| PPU                     | 2.7 person per unit |
| Maximum Day Factor      | 2.0                 |
| Peak Hour Factor        | 3.0                 |

*Region of Peel, Watermain Design Criteria, Revised June 2010*

#### 4.1.2 Existing

As shown in the City's 'As-Built' drawings (contained in **Appendix B**), there is an existing 300 mm dia. watermain located on the northside of Thomas Street that runs along the southern frontage of the subject site.

There are 2 fire hydrants on Thomas Street. One is located in front of 80 Thomas Street, approximately 53m northeast of the subject site, and the other located in front of 96 Thomas Street, approximately 45m southwest of the subject site.

ONYX.SPRINKLER Installations Inc. performed the flow test for the development at 80 Thomas Street on November 10<sup>th</sup> 2020. Since the subject site is adjacent to 80 Thomas St. development, the flow test will be used for this project, details can be found in Appendix C.

#### 4.1.3 Proposed Water Demand

Based on the calculation in **Appendix C**, water demand and pressure as below in Table 1:

**Table 1 Water Demand & Pressure**

|                           | Water Demand | Required Pressure, kPa | Provided Pressure, kPa |
|---------------------------|--------------|------------------------|------------------------|
| Average Daily Demand, l/s | 0.09         | 275 - 690              | 550                    |
| Maximum Daily Demand, l/s | 0.18         | 275 - 690              | 550                    |
| Peak Hourly Demand, l/s   | 0.26         | 275 - 690              | 550                    |

According to our calculations, a minimum fire suppression flow of 146 l/s at 140 kPa will be required, refer to detailed calculations in **Appendix C**. ONYX flow tests show that the existing water system has 391 l/s at 140 kPa (20 psi). Based on the flow test and Table 1, there is enough pressure and flow in the existing water system to support the subject development.

#### 4.1.4 Proposed Water Servicing

An internal 150mm dia. watermain will be proposed to service the site with 25mm PVC water connections for each unit, which will connect to the existing 300 mm watermain on Thomas Street.

At this time no additional Fire Hydrants are being proposed since there are 2 existing hydrants within 75m which provides sufficient coverage for the proposed site.

### 4.2 SANITARY

#### 4.2.1 Design Criteria

|                           |                                    |
|---------------------------|------------------------------------|
| Type of Construction      | Residential                        |
| PPU                       | 2.7 people per unit                |
| Peak sanitary flow factor | Harmon Formula                     |
| Average Daily Flow        | 302.8 L/capita/day                 |
| Peak Extraneous Flow      | 0.2 L/s/ha<br>0.028 l/s/m of sewer |

*Region of Peel, Sanitary Sewer Design Criteria, Modified March 2017 REV 0.9*

#### **4.2.2 Existing Conditions**

As shown in City's 'As-Built' drawings (contained in **Appendix B**), there are two (2) existing sanitary sewers along Thomas Street. One located in the middle of Thomas Street with size of 375mm dia. at slope of 0.6%, named as EX. N. SAN in drawings. The other located in the south of Thomas Street with size of 300mm dia.

#### **4.2.3 Proposed Sanitary Flow**

During the site development, the proposed sanitary flow will be 1.85 l/s, for detailed calculation see **Appendix D**. The proposed development will add 1.4% of the existing sanitary sewer capacity, which can be considered negligible.

#### **4.2.4 Proposed Sanitary Servicing**

An internal 250mm dia. sanitary sewer will drain southernly and connect into the existing 375mm dia. sanitary sewer system on Thomas Street.

### **5.0 GRADING, DRAINAGE & STORMWATER MANAGEMENT**

#### **5.1.1 Stormwater Design Criteria**

The most current version of the following guidelines, policies and standards will apply to the design of storm drainage facilities in the City of Mississauga:

- MOECC (i.e., Stormwater Management Planning and Design Manual, March 2003)
- Wet Weather Flow Management Guidelines, WWFMG, November 2006
- Low Impact Development Stormwater Management Planning and Design Guide (TRCA, 2011)
- Development Requirements Manual, Section 2 – Design Requirements, City of Mississauga, Effective September 2016

#### **5.1.2 Stormwater Quality Control**

Under the Wet Weather Flow Management Guidelines, the site is required to provide a long-term removal of 80% of total suspended solids (TSS) on an average annual basis.

#### **5.1.3 Storm Water Quantity Control**

Provide post to pre control for 2-, 5-, 10-, 25-, 50- & 100-year storm event.

#### **5.1.4 Erosion Control**

As indicated in WWFMG, 'For small infill/redevelopment sites < 2 ha, erosion control in the form of stormwater detention is normally not required, provided the on-site minimum runoff retention from a small design rainfall event (typically 5mm) is achieved under the Water Balance Criteria.'

## 5.2 EXISTING CONDITIONS

### 5.2.1 Existing Drainage pattern

The overland flow on site generally drains southernly uncontrolled to Thomas street and finally collected by the existing storm sewer system on Thomas Street.

### 5.2.2 Existing Stormwater Service

There is an existing 1200mm dia. C.P. storm sewer located on Thomas Street, runs along the southern frontage of the subject site with a slope of 1.66%, see in **Appendix B**.

### 5.2.3 Pre-Development Target Flow

The pre-development target flow is summarized in Table 2 below, and drainage areas can be found on Drawing DAP.

**Table 2 – Pre-Development Target Peak Flow**

| On Site, Pre-development Catchment Area: A=0.1643 ha |      |                  |
|--|------|------------------|
| Return Period  | "C"  | Target Peak Flow |
| 1:2  | 0.25 | 6.8 L/s          |
| 1:5  | 0.25 | 9.2 L/s          |
| 1:10   | 0.25 | 11.3 L/s         |
| 1:25   | 0.28 | 14.3 L/s         |
| 1:50   | 0.30 | 17.4 L/s         |
| 1:100  | 0.31 | 20.1 L/s         |

## 5.3 STORMWATER QUANTITY CONTROL

The majority of stormwater from the site will be collected via catchbasins, manholes, and area drains. All of the area drains and the associated piping will be detailed by the building mechanical consultant under a separate application. A small area on the south and east of the property will drain to Thomas Street as uncontrolled flow.

The following table identifies the input post development parameters and the corresponding detailed calculations can be found in **Appendix E**.

**Table 3 – Post-Development Quantity Control Analysis**

| Return Period | Target Flow (L/s) | Uncontrolled Flow to Thomas Street (L/s) | Controlled Flow before Quantity Control (L/s) | Controlled Flow after Quantity Control (L/s) | Required Storage (m <sup>3</sup> ) |
|---------------|-------------------|--|---|--|------------------------------------|
| (1)           | (2)               | (3)                                      | (4)   | (5)  | (6)                                |
| 1:2           | 6.8               | 1.1                                      | 20.1  | 5.6  | 12.5                               |
| 1:5           | 9.2               | 1.4                                      | 27.0  | 7.7  | 16.5                               |
| 1:10          | 11.3              | 1.7                                      | 33.3  | 9.5  | 20.3                               |
| 1:25          | 14.3              | 2.2                                      | 42.0  | 11.9   | 25.8                               |
| 1:50          | 17.4              | 2.7                                      | 51.2  | 14.35  | 31.6                               |
| 1:100         | 20.1              | 3.1                                      | 59.0  | 16.8   | 36.2                               |

Total stormwater storage will be provided by an underground GreenStorm System (40.0m<sup>3</sup>) and underground pipes and MHs. The maximum outflow from the site will be controlled via an 75mm orifice tube located in upstream of STM Control MH, see Drawing of SS.

The uncontrolled flow will drain to ROW of Thomas Street and will be collected by the storm sewer system (CBs) along north side of Thomas Street.

**5.4 DOWNSTREAM STORM SEWER IMPACT ANALYSIS**

Refer to the report of “Storm Sewer Downstream Capacity Analysis”, the proposed development was over controlled and will not be affecting the existing downstream storm sewer system capacity.

**5.5 STORMWATER QUALITY CONTROL**

Under the Wet Weather Flow Management Guidelines, the site is proposed to provide a long-term removal of 80% of total suspended solids (TSS) on an average annual basis.

To address this requirement, NexTrans is proposing to provide:

- A Stormceptor EFO4 at the downstream STM MH 103.
- Enhanced landscaping features to treat runoff from the property.

Table 4 below quantitatively demonstrates how criteria targets are being addressed.

**Table 4 – TSS Removal**

| Surface         | Site Area (ha) | Fraction of Site Area | Proposed TSS Removal | TSS Removal Overall |
|-----------------|----------------|-----------------------|----------------------|---------------------|
| Controlled Area |                |                       |                      |                     |
| Impervious      | 0.1275         | 78%                   | 91%                  | 71%                 |



|                                     |               |     |     |            |
|-------------------------------------|---------------|-----|-----|------------|
| Landscape<br>(300mm absorbent soil) | 0.0242        | 15% | 95% | 14%        |
| <b>Uncontrolled Area</b>            |               |     |     |            |
| Landscape<br>(300mm absorbent soil) | 0.0077        | 4%  | 85% | 3%         |
| Impervious                          | 0.0049        | 3%  | 0   | 0          |
| <b>Total</b>                        | <b>0.1643</b> |     |     | <b>88%</b> |

## 5.6 WATER BALANCE

The water balance criteria require that 5 mm of rainfall be diverted from the storm sewer system through infiltration, evapotranspiration, or rainwater reuse. A total of 8.2 m<sup>3</sup> of water is to be retained on site (1643 m<sup>2</sup> x 5 mm).

The proposed GreenStorm system will retain 17.2 m<sup>3</sup> volume of harvested rain water to be infiltrated on site, details of the proposed GreenStorm system can be found in the shop drawing in **Appendix D**.

## 6.0 SUMMARY

**Table 5 – STM Plan Summary**

|                      | Criteria                  | Proposed   | Met the Criteria? |
|----------------------|---------------------------|--|-------------------|
| Water Balance        | 5mm                       | 5mm  | yes               |
| STM Quantity Control | Retain to pre-development | Minor System: internal pipe<br>Major System: future road | yes               |
| STM Quality Control  | 80% of TSS removal        | 80% min.   | yes               |

This Functional Servicing and Stormwater Management Report has outlined the requirements for servicing the proposed development. Reference to Table 5, these preliminary studies and general results indicate that the subject development can be serviced by existing municipal services (storm, sanitary and water) and the existing infrastructure is adequate to support the proposed development.

Report Prepared By:

Wendy Li  
P.Eng.

**NEXTRANS (CONSULTING ENGINEERS)**

Report Reviewed By:



Ghansham Ramnath  
P.Eng.



DATE: FEB 13, 2019  
 PROJECT NO:  
 NT-19-013  
 DRAWING NO.  
 FIGURE 1

PROJECT NAME:  
**86 THOMAS STREET**  
**CITY OF MISSISSAUGA**

DRAWING TITLE:  
**LOCATION PLAN**



# APPENDIX A – SITE PLAN

**SITE STATISTICS**

| ZONING REGULATIONS - From Table 4.14.1 - RM9 and RM10 Permitted Uses and Zone Regulations |  |  |  |
|---|--|--|--|
| ZONE RM-10 (BACK TO BACK AND STACKED TOWNHOUSES)  |  |  | REXTON DEVELOPMENT                     |
| 1.  | ZONING REGULATIONS   | REQUIRED                                   | PROPOSED                               |
| 2.  | MAXIMUM DWELLING HEIGHT  |  |  |
| 3.  | 5.1 Measured to the mean height level of a flat roof on top of a sloped roof.                      | 15.0 m, 3 Storeys.                         | 9.86 m, 3 Storeys.                     |
| 4.  | 6.0 MINIMUM FRONT YARD   | 7.50 m.                                    |  |
| 5.  |  |  | 3.80 m (South)                         |
| 7.  | 7.0 MINIMUM EXTERIOR SIDE YARD   | 4.5 m.                                     | N/A                                    |
| 8.  |  |  | N/A                                    |
| 9.  | 8.0 MINIMUM INTERIOR SIDE YARD   | 4.5 m.                                     | 8.78 m (West)                          |
| 10.   |  |  | 1.23 m (East)                          |
| 11.   | 12.2 MINIMUM PARKING SPACES  |  |  |
| 12.   | 2.0 spaces per 4-4 bedroom unit = 8 parking spaces.<br>1.5 spaces per 6-2 bedroom unit = 9 spaces. | 17 spaces                                  | 18 spaces                              |
| 13.   | 12.3 MINIMUM VISITOR PARKING SPACES  |  |  |
| 14.   | 0.25 spaces per 10 units = 2.5 spaces.   | 2.5 spaces                                 | 3 spaces (Includes 1 H/C space)        |
| 15.   | 13.0 PARKING AREAS SETBACKS  |  |  |
| 16.   | Minimum setback between a parking space and an interior side lot line and/or rear lot line.        | 3.0 metres                                 | 1.63 metres                            |
| 17.   | 15.0 MINIMUM AMENITY AREA AND LANDSCAPE AREA   |  |  |
| 18.   | 15.1 MINIMUM LANDSCAPE AREA  | 40 % of lot area.                          | 30.59 % (502.68 m <sup>2</sup> )       |
| 19.   | 15.2 MINIMUM REQUIRED LANDSCAPED SOFT AREA   | 50 % of landscaped area                    | 61.68 % (310.04 m <sup>2</sup> )       |
| 20.   | 15.3 MINIMUM LANDSCAPED BUFFER ABUTTING ANY SIDE AND REAR LOT LINE                                 | 3.0 metres                                 | 1.23 m East yard,<br>1.28 m West yard. |
| 21.   | 15.4 MINIMUM CONTIGUOUS AMENITY AREA   | 82.17 m <sup>2</sup> (5 % of the lot area) | 82.17 m <sup>2</sup> outdoor.          |
| 22.   | 15.7 MINIMUM CONTIGUOUS PRIVATE OUTDOOR SPACE PER UNIT   | 6.0 m <sup>2</sup>                         | 7.53 m <sup>2</sup>                    |

**LEGAL DESCRIPTION**

PART OF Lot 4  
Concession 5, West of Hurontario Street  
City of Mississauga  
Regional Municipality of Peel

**SITE STATISTICS**

**ZONING:**  
RM10 (Back to back & stacked townhouse)

**LOT AREA** 1,643.35 m<sup>2</sup> (17,689 Ft<sup>2</sup>) (0.406 ac)

**BUILDING COVERAGE:**  
PERMITTED: N/A  
PROPOSED: 877.76 m<sup>2</sup> (9,448.13 Ft<sup>2</sup>) 53.41%

**DWELLING UNIT WIDTH:**  
MINIMUM PERMITTED: 4.5 m  
PROPOSED: 5.73 m

**LOT FRONTAGE:**  
REQUIRED (MIN.): 38.0 m  
PROPOSED: 39.04 m

**BUILDING G.F.A.:**

|                   |  |
|-------------------|--|
| FIRST FLOOR AREA  | 283.18 m <sup>2</sup> (3,048.12 Ft <sup>2</sup> )    |
| SECOND FLOOR AREA | 877.76 m <sup>2</sup> (9,448.13 Ft <sup>2</sup> )    |
| THIRD FLOOR AREA  | 877.76 m <sup>2</sup> (9,448.13 Ft <sup>2</sup> )    |
| TOTAL GROSS AREA  | 2,038.70 m <sup>2</sup> (21,944.38 Ft <sup>2</sup> ) |

**SETBACKS**

|                           | REQUIRED | PROVIDED |
|---------------------------|----------|----------|
| Front Yard (South)        | 4.5 m    | 3.80 m   |
| Rear Yard (North)         | 7.5 m    | 3.54 m   |
| Interior Side Yard (East) | 2.5 m    | 1.23 m   |
| Interior Side Yard (West) | 2.5 m    | 8.78 m   |

**PARKING SETBACKS:**  
East (to a Residential Zone) 4.5 m 1.63 m

**BUILDING HEIGHT: MAXIMUM PERMITTED** 15.0 m 3 Storeys  
**PROVIDED:** 9.86 m 3 Storeys

**PARKING:**

**REQUIRED:**  
2.0 spaces per 4-4 bedroom unit = 8 parking spaces  
1.5 spaces per 6-2 bedroom unit = 9 spaces  
0.25 visitor spaces per 10 units = 2.5 spaces  
Total: 20 spaces

**PROVIDED:**  
21 spaces  
Includes 3 visitor spaces:  
1-V, 20-V and 21-V (H/C space)

**LANDSCAPE AREA**

|                  |                                  |
|------------------|----------------------------------|
| MINIMUM REQUIRED | 40 %                             |
| PROPOSED         | 30.59 % (502.68 m <sup>2</sup> ) |

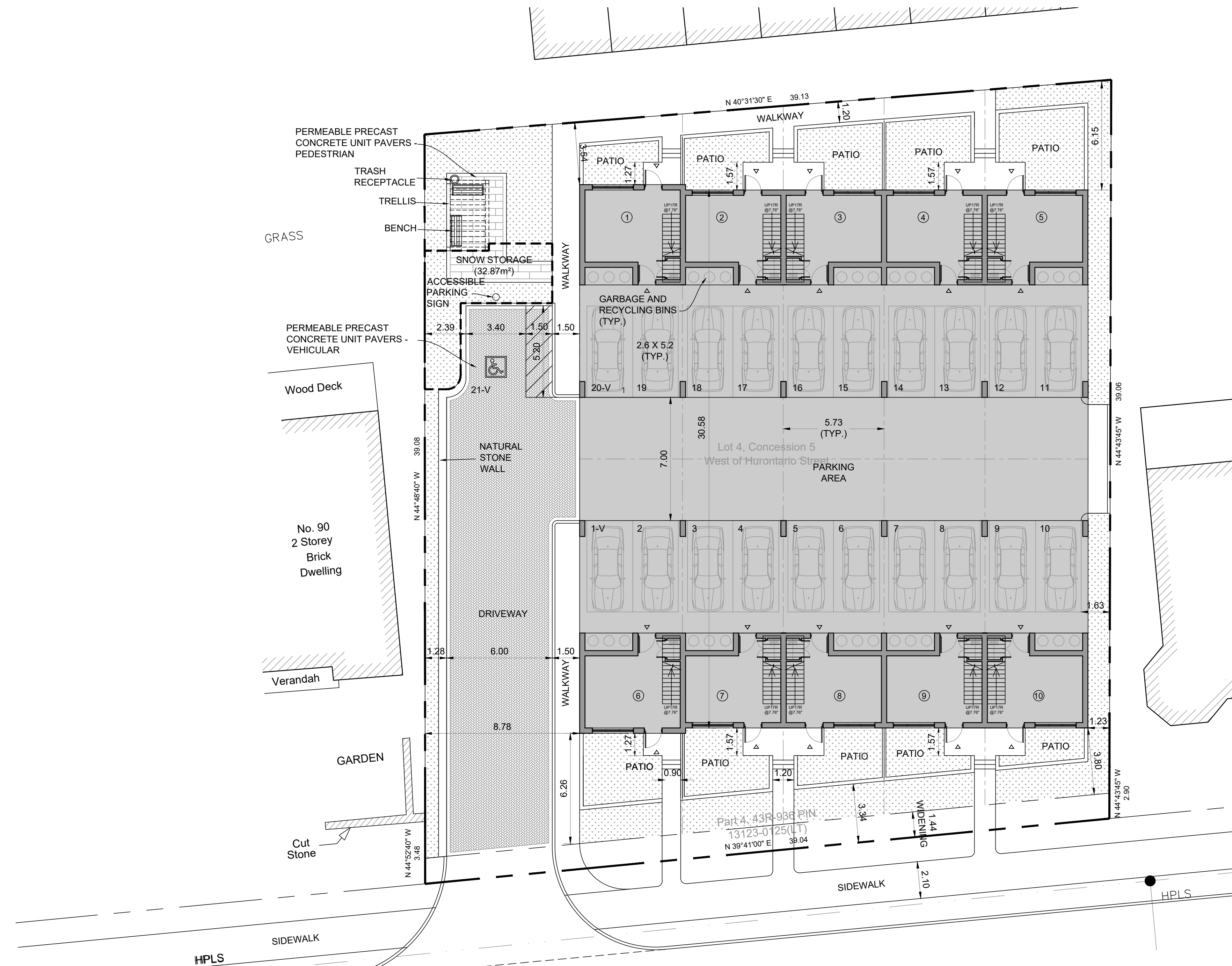
**SNOW STORAGE**

|                |   |
|----------------|---|
| REQUIRED MIN.: | 32.87 m <sup>2</sup> (2.00 % of Lot Area) |
| PROVIDED:      | 32.87 m <sup>2</sup> (2.00 % of Lot Area) |

**General Note:**

- I hereby certify that this drawing confirms in all respects to the site development plans Architect or Engineer's Signature (if applicable) and Professional seal
- The City of Mississauga requires that all working drawings submitted to the Building Division as part of an application for the issuance of a building permit shall be certified by the architect or engineer as being in conformity with the site development plan as approved by the City of Mississauga.
- All exterior lighting will be directed onto the site and will not infringe upon the adjacent properties.
- All rooftop mechanical units shall be screened from view by the applicant.
- Parking spaces reserved for people with disabilities must be identified by a sign, installed at the applicant's expense, in accordance with the By-law Requirements and Building Code Requirements.
- The applicant will be responsible for ensuring that all plans conform to Transport Canada's restrictions.
- Grades will be met with a 33% maximum slope at the property lines and within the site.
- All damaged areas are to be reinstated with topsoil and sod prior to the release of securities.
- Signage shown on the site development plans is for information purposes only. All signs will be subject to the provisions of Sign by-law 0054-2002, as amended, and a separate sign application will be required through the Building Division.
- Any fencing adjacent to municipal lands is to be located 15 cm (6.0 in.) inside the property line.
- Only "shielded" lighting fixtures are permitted for all development, except for detached and semi-detached dwellings within 60 m (196.8 ft.) of a residentially zoned property and must confirm to the Engineer Certified Lighting Plan.
- The Engineer Certified Lighting Plan must be signed by the consulting Engineer.
- The Owner covenants and agrees to construct and install "shielded" lighting fixtures on the subject lands, in conformity with the Site Plan and Engineer Certified Lighting Plan to the satisfaction of the City of Mississauga.
- The applicant will be responsible for ensuring that all plans conform to Transport Canada's restrictions.
- Where planting is to be located in landscaped areas on top of an underground parking structure, it is the responsibility of the applicant to arrange the coordination of the design of the underground parking structure with the Landscape Architect and the Consulting Engineering. Underground parking structures with landscaping area to be capable of supporting the following loads:
  - 15 cm of drainage gravel plus 40 cm topsoil for sod
  - 15 cm of drainage gravel plus 60 cm topsoil for shrubs
  - 15 cm of drainage gravel plus 90 cm for trees
 Or
  - Prefabricated sheet drain system\* with a compressive strength of 1003 Kpa plus 40 cm topsoil for sod
  - Prefabricated sheet drain system\* with a compressive strength of 1003 Kpa plus 60 cm topsoil for shrubs
  - Prefabricated sheet drain system\* with a compressive strength of 1003 Kpa plus 90 cm topsoil for trees
  - \* Terradrain 900 or approved equal
- The structural design of any retaining wall over 0.6 m in height or any retaining wall located on a property line is to be shown on the Site Grading plan for this project and is to be approved by the Consulting Engineer for the project.
- Continuous 15 cm high barrier type poured concrete curbing will be provided between all asphalt and landscaped areas throughout the site.
- All utility companies will be notified for locates prior to the installation of the hoarding that lies within the site and within the limited of the City boulevard area.

Curb & Gutter



**Thomas Street**

**NOTE**

Garbage and Recycling bins will be carried to the street individually by each tenant for municipal pick-up.

**NOTE:**

If the final course of asphalt paving is delayed, install a temporary lift of asphalt at ramps or curb cuts to provide barrier-free access.

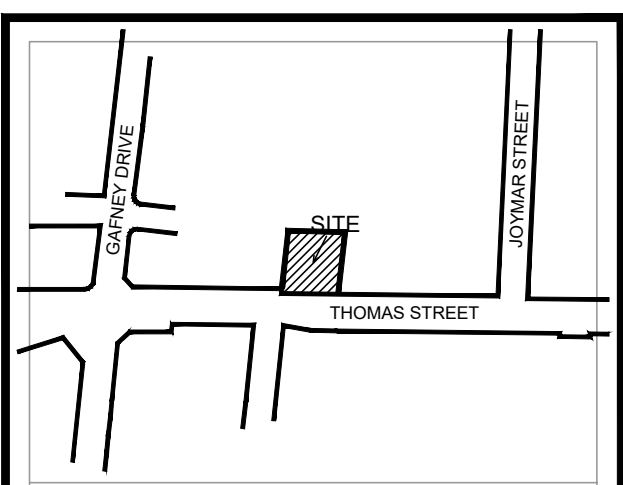
**UNIT SIZES**

| Unit  | First Floor          | Second Floor         | Third Floor          | Total                  |
|-------|----------------------|----------------------|----------------------|------------------------|
| 1     | 29.71m <sup>2</sup>  | 89.64m <sup>2</sup>  | 89.64m <sup>2</sup>  | 208.99m <sup>2</sup>   |
| 2     | 27.97m <sup>2</sup>  | 87.31m <sup>2</sup>  | 87.31m <sup>2</sup>  | 202.59m <sup>2</sup>   |
| 3     | 27.97m <sup>2</sup>  | 87.31m <sup>2</sup>  | 87.31m <sup>2</sup>  | 202.59m <sup>2</sup>   |
| 4     | 27.97m <sup>2</sup>  | 87.31m <sup>2</sup>  | 87.31m <sup>2</sup>  | 202.59m <sup>2</sup>   |
| 5     | 27.97m <sup>2</sup>  | 87.31m <sup>2</sup>  | 87.31m <sup>2</sup>  | 202.59m <sup>2</sup>   |
| 6     | 29.71m <sup>2</sup>  | 89.64m <sup>2</sup>  | 89.64m <sup>2</sup>  | 208.99m <sup>2</sup>   |
| 7     | 27.97m <sup>2</sup>  | 87.31m <sup>2</sup>  | 87.31m <sup>2</sup>  | 202.59m <sup>2</sup>   |
| 8     | 27.97m <sup>2</sup>  | 87.31m <sup>2</sup>  | 87.31m <sup>2</sup>  | 202.59m <sup>2</sup>   |
| 9     | 27.97m <sup>2</sup>  | 87.31m <sup>2</sup>  | 87.31m <sup>2</sup>  | 202.59m <sup>2</sup>   |
| 10    | 27.97m <sup>2</sup>  | 87.31m <sup>2</sup>  | 87.31m <sup>2</sup>  | 202.59m <sup>2</sup>   |
| Total | 283.18m <sup>2</sup> | 877.76m <sup>2</sup> | 877.76m <sup>2</sup> | 2,038.70m <sup>2</sup> |

**SITE PLAN**

SCALE 1:150

CONTRACTOR SHALL CHECK AND VERIFY ALL DIMENSIONS ON SITE. ALL DRAWINGS ARE THE PROPERTY OF THE ARCHITECT AND MAY NOT BE USED WITHOUT HIS PERMISSION. THIS DRAWING IS NOT TO BE USED FOR CONSTRUCTION UNTIL COUNTERSIGNED BY THE ARCHITECT. DRAWINGS ARE NOT TO BE SCALED.

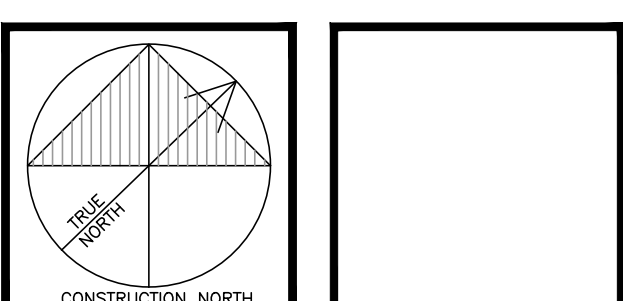


**KEY PLAN**  
N.T.S.

SITE PLAN APPLICATION NUMBER: OZ 20 11

| NO. | DATE        | REVISION/ISSUED FOR          |
|-----|-------------|------------------------------|
| 2   | JUN 03 2020 | SITE PLAN APPROVAL           |
| 1   | MAR 21 2019 | PRE-APPLICATION CONSULTATION |
| NO. | DATE        | REVISION/ISSUED FOR          |

**PROPOSED RESIDENTIAL DEVELOPMENT**  
**86 THOMAS ST.**  
MISSISSAUGA, ON



**WES SURDYKA**  
architect inc

3645 KEELE STREET, 2nd FLOOR, STE 108  
TORONTO, ONTARIO M3J 1M8  
TEL (416) 630-2254 FAX (416) 630-5741  
E-mail: surdykaarchitect@bellnet.ca

DRAWING TITLE

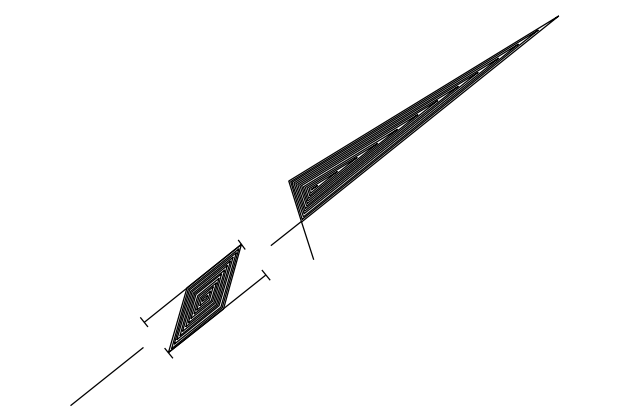
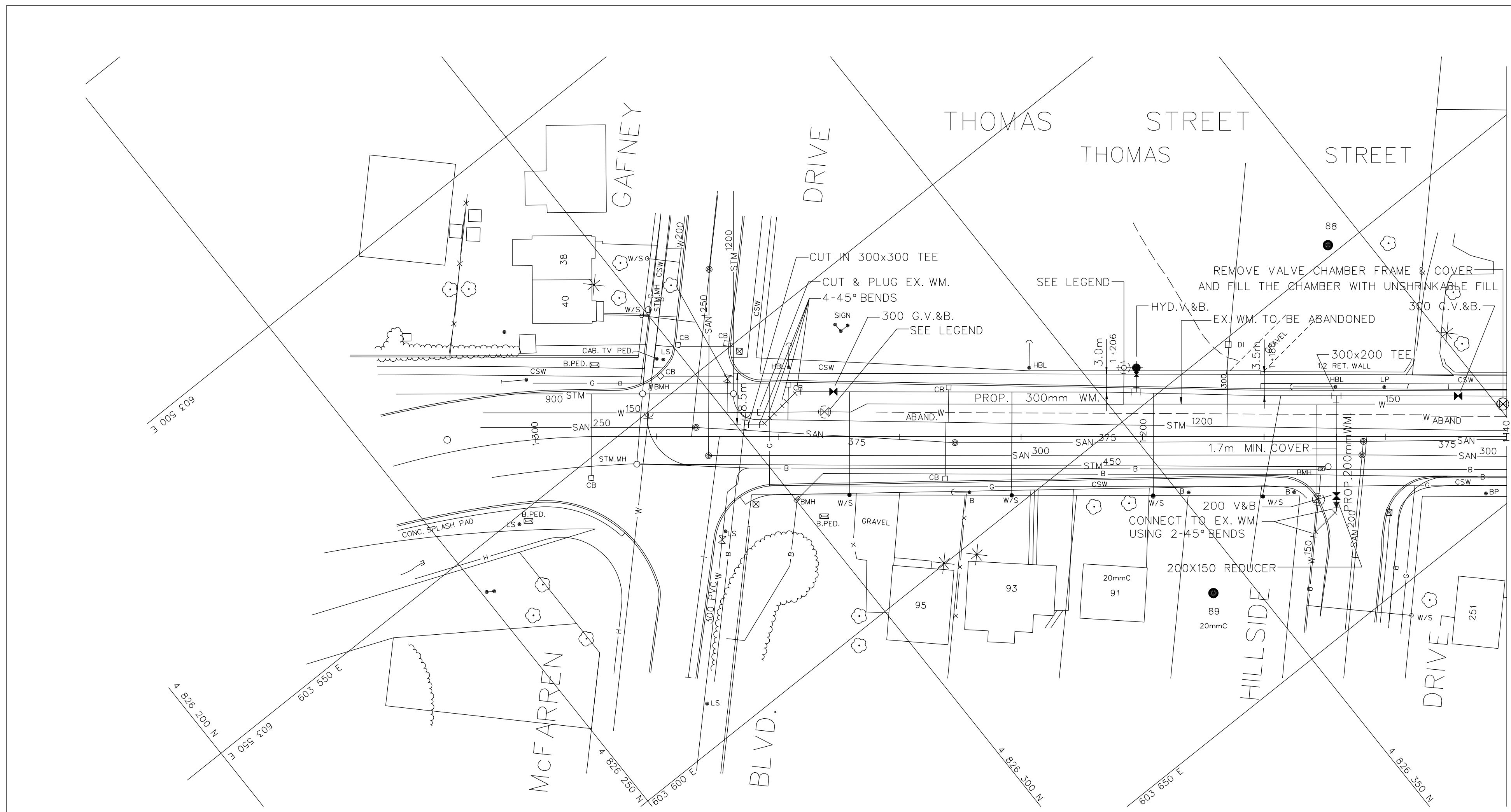
**SITE PLAN**

|             |          |               |
|-------------|----------|---------------|
| DRAWN BY    | PLOTTED  | MAR. 18, 2021 |
| SCALE       | AS SHOWN |               |
| START DATE  | MAR 2019 |               |
| PROJECT NO. | 18-12    |               |

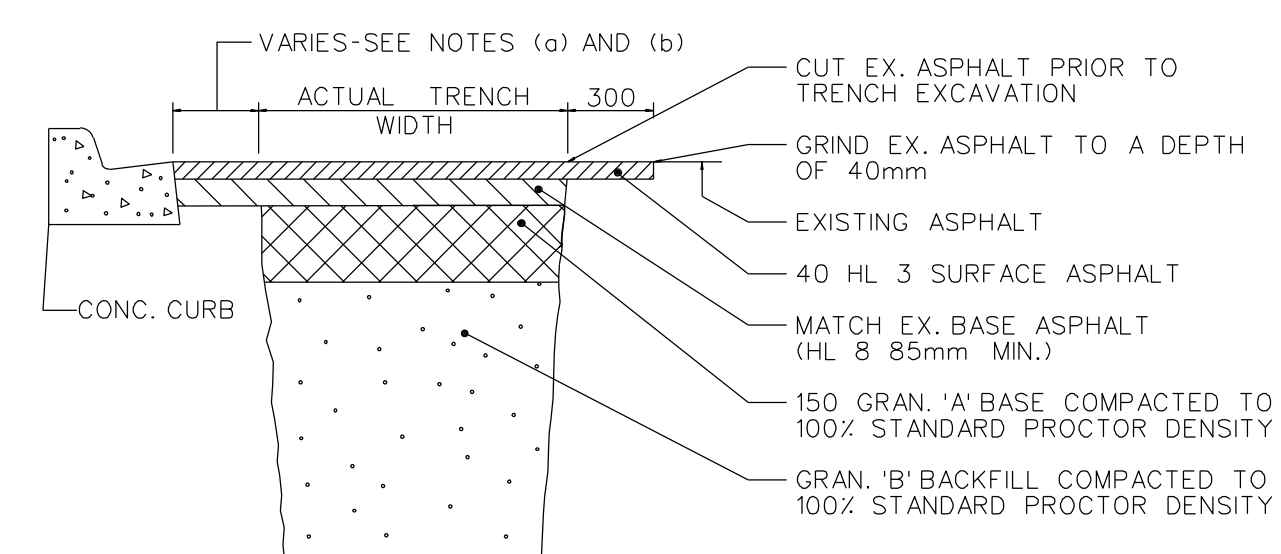
DRAWING NO.  
**A1.0**  
OF

# **APPENDIX B – AS-BUILT DRAWINGS**





**DISCLAIMER**  
 These records are based upon available and unverified information and may prove inaccurate. The Region of Peel disclaims any responsibility should these records be relied upon to the detriment of any person.



NOTES: (a). 300mmx40mm GRIND WIDE WHERE DISTANCE FROM EDGE OF TRENCH TO CURB EXCEEDS 1.0m  
 (b). FULL WIDTH TO CURB WHERE DISTANCE LESS THEN 1.0m

REINSTATEMENT DETAIL  
 (THOMAS ST. AND QUEEN ST.)  
 N.T.S.

| SERVICE DATA     |      |       |               |      |       |
|------------------|------|-------|---------------|------|-------|
| SERVICE          | DATE | INIT. | SERVICE       | DATE | INIT. |
| SAN. SEWERS      |      |       | GAS MAINS     |      |       |
| STORM SEWERS     |      |       | BELLUNG CABLE |      |       |
| WATERMANS        |      |       | HYDRO/G CABLE |      |       |
| TRANSIT          |      |       | GNT. HYDRO    |      |       |
| PARK & REC.      |      |       | CTV           |      |       |
| ONT. CLEAN WATER |      |       |               |      |       |

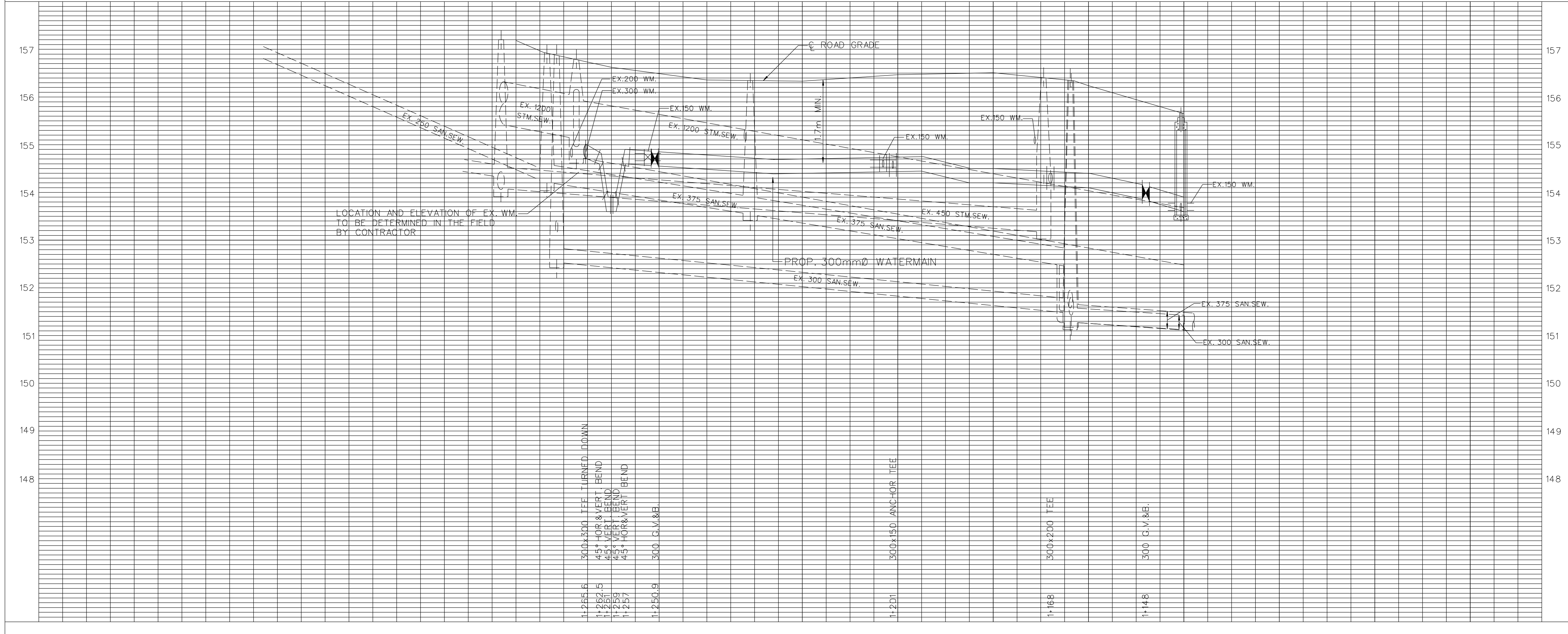
  

| REVISIONS |                |       |
|-----------|----------------|-------|
| DATE      | DETAILS        | INIT. |
| OCT. 1997 | AS CONSTRUCTED | J.P.  |

KEY PLAN  
N.T.S.

NOTES: 1. FOR GENERAL NOTES AND LEGEND SEE DWG. No. 22150-D  
 2. FOR TRENCH BEDDING DETAIL SEE DWG. No. 22570-D  
 3. REMOVE AND DISPOSE OF ABANDONED WATERMAN IF IT CONFLICTS WITH PROPOSED WATERMAN

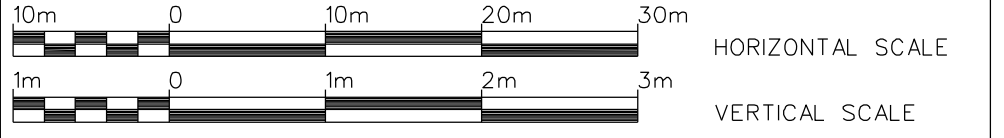


**General Notes**  
 - - All Driveways ASPHALT Unless Otherwise Noted.  
 - - All Service Locations Are Approximate And Must Be Located Accurately In The Field  
 ⊙ Denotes Building - Not Located  
 ⊞ Denotes Building Located

B.M. No. Elev.  
 The Contractor Is Responsible For Locating And Protecting All Existing Utilities Prior To And During Construction Location Of Existing Utilities Approximate Only To Be Verified In Field By Contractor.

Designed by \_\_\_\_\_ Chkd. \_\_\_\_\_  
 Approved by \_\_\_\_\_

**NOTICE TO CONTRACTOR**  
 48 HOURS PRIOR TO COMMENCING WORK NOTIFY THE FOLLOWING  
 THE REGIONAL MUNICIPALITY OF PEEL  
 CITY OF MISSISSAUGA WORKS DEPT.  
 CITY OF BRAMPTON WORKS DEPT.  
 TOWN OF CALEDON WORKS DEPT.  
 BELL TELEPHONE COMPANY  
 CONSUMERS GAS COMPANY  
 MINISTRY OF TRANSPORTATION  
 ONTARIO CLEAN WATER AGENCY  
 HYDRO ELECTRIC POWER COMM. OF ONTARIO  
 HYDRO ELECTRIC COMM. CITY OF MISSISSAUGA  
 HYDRO ELECTRIC COMM. CITY OF BRAMPTON  
 HYDRO ELECTRIC COMM. TOWN OF CALEDON  
 CABLE TELEVISION



**Region of Peel**  
**Public Works**

THOMAS STREET  
 (FROM JOYMAR DR. TO GAFNEY DR.)  
 PROP. 300mmØ WATERMAIN  
 Sta. 1+140 To Sta. 1+300

|  |               |        |             |         |        |        |       |       |            |          |      |             |         |      |               |       |        |         |
|--|---------------|--------|-------------|---------|--------|--------|-------|-------|------------|----------|------|-------------|---------|------|---------------|-------|--------|---------|
| 1-300  | 1-280         | 1-260  | 1-240       | 1-220   | 1-200  | 1-180  | 1-160 | 1-140 |            |          |      |             |         |      |               |       |        |         |
| 153.60   | 154.40        | 154.40 | 154.45      | 154.20  | 154.10 | 153.60 |       |       |            |          |      |             |         |      |               |       |        |         |
| BOT. EL. OF WM. @ RD. CHAINAGE   |               |        |             |         |        |        |       |       |            |          |      |             |         |      |               |       |        |         |
| <table border="0"> <tr> <td>Checked by</td> <td>Drawn by</td> <td>Y.C.</td> <td>Project No.</td> <td>96-1440</td> </tr> <tr> <td>Date</td> <td>AUG. 03, 1995</td> <td>Sheet</td> <td>2 of 2</td> <td>22151-D</td> </tr> </table> |               |        |             |         |        |        |       |       | Checked by | Drawn by | Y.C. | Project No. | 96-1440 | Date | AUG. 03, 1995 | Sheet | 2 of 2 | 22151-D |
| Checked by   | Drawn by      | Y.C.   | Project No. | 96-1440 |        |        |       |       |            |          |      |             |         |      |               |       |        |         |
| Date   | AUG. 03, 1995 | Sheet  | 2 of 2      | 22151-D |        |        |       |       |            |          |      |             |         |      |               |       |        |         |



# APPENDIX C – WATER DATA

## DOMESTICE WATER CALCULATION - New Building

|                             |                        |                    |
|-----------------------------|------------------------|--------------------|
| <b>86 Thomas Street</b>     |                        |                    |
| Mississauga, ON             |                        |                    |
| March 15, 2020              |                        |                    |
| File No.: NT-19-013         |                        |                    |
| <b>Nextrans Engineering</b> |                        |                    |
| Prepared by: W.L.           | <b>Type of Housing</b> | <b>Residential</b> |
| Checked by: G.R.            |                        |                    |

### Unit Quantity Determination

|                         |             |              |
|-------------------------|-------------|--------------|
| 1. Type of Construction | Residential |              |
| 2. PPU                  | 2.7         |              |
| 3. Number of Units      | 10          |              |
| 4. Maximum Day Factor   | 2.00        |              |
| 5. Peak Hour Factor     | 3.00        |              |
| 6. Average Daily Demand | 280         | L/person/day |

### Water Usage Determination

|                         |      |     |
|-------------------------|------|-----|
| 1. Average Daily Demand | 0.09 | L/s |
| 2. Maximum Daily Demand | 0.18 | L/s |
| 3. Peak Hourly Demand   | 0.26 | L/s |

| <b>FIRE WATER DEMAND CALCULATION (FUS 1999)</b> |                       |                        |                  |
|---|-----------------------|------------------------|------------------|
| <b>86 Thomas Street</b>                         |                       |                        |                  |
| Mississauga, ON                                 |                       |                        |                  |
| June 20, 2020                                   |                       |                        |                  |
| File No.: NT-19-013                             |                       |                        |                  |
| <b>Nextrans Engineering</b>                     |                       |                        |                  |
| Checked by: G.R.                                |                       | <b>Type of Housing</b> | <b>Townhouse</b> |
| Prepared by: W.L.                               |                       | <b>ID</b>              | New Building     |
| <b>Design Parameters</b>                        |                       |                        |                  |
| 1 C - Type of Construction                      | ordinary construction |                        | 1.0              |
| 2. Total Floor Area (from site plan)            | 584                   |                        | m <sup>2</sup>   |
| 3. Fire Hazard Factor                           | Combustible           |                        | 0%               |
| 4. Automatic Sprinkler Protection               | no                    |                        | 0%               |
| 5. Fully Supervised System                      | no                    |                        | 0%               |
| 6. Exposure Factor                              |                       |                        | 0.65             |
|   | East Side             | 3.1 to 10m             | 0.2              |
|   | West Side             | 3.1 to 10m             | 0.2              |
|   | South Side            | 30.1 to 45m            | 0.05             |
|   | North Side            | 3.1 to 10m             | 0.2              |
| <b>Fire Water Determination</b>                 |                       |                        |                  |
| 1. $F=220 \cdot C \cdot A^{0.5}$                | 5,316.7               |                        | l/min            |
| 2. Adjusted by Fire Hazard Factor               | 5,316.7               |                        | l/min            |
| 3. Adjusted by Automatic Sprinkler System       | 0.0                   |                        | l/min            |
| 4. Adjusted by Supervised System                | 0.0                   |                        | l/min            |
| 5. Adjusted by Exposure Factor                  | 3,455.8               |                        | l/min            |
| <b>Fire Water Demand</b>                        | <b>8,772.5</b>        |                        | <b>l/min</b>     |

146 L/s

A min. flow of 146 l/s must be available at the nearest hydrant with a minimum pressure of 140 kPa.

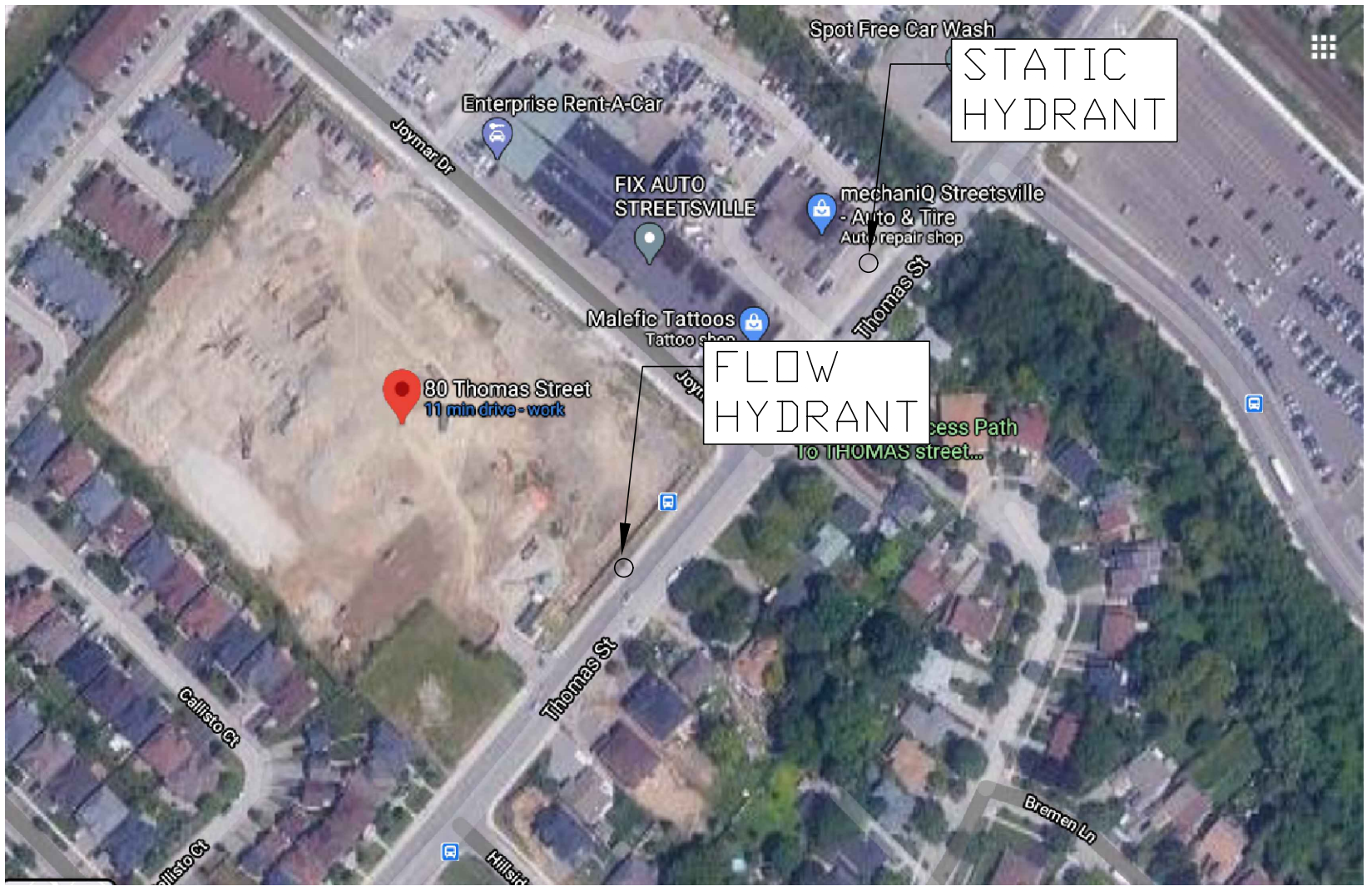
# FIRE HYDRANT FLOW TEST REPORT

## ONYX SPRINKLER

INSTALLATIONS INC.

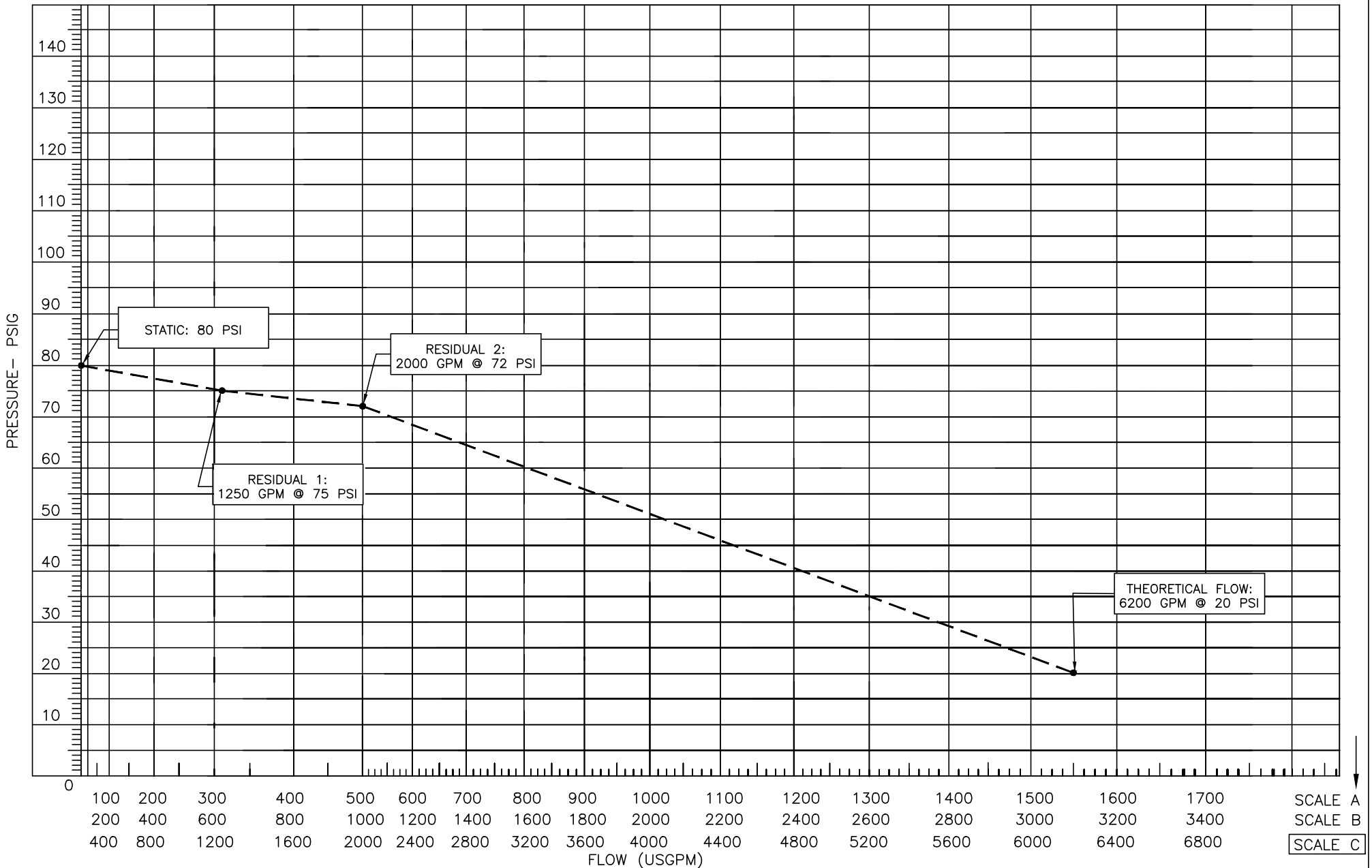
400 MATHESON BLVD W,  
MISSISSAUGA, ON  
L5R 1B8  
TEL. 416-674-5633  
FAX. 416-674-9623

|               |                                   |
|---------------|-----------------------------------|
| LOCATION:     | 80 THOMAS, MISSISSAUGA, ON        |
| TEST DATE:    | 11/10/2020                        |
| TIME:         | 08:00 AM                          |
| CONDUCTED BY: | ONYX SPRINKLER INSTALLATIONS INC. |
| WITNESSED BY: | JAKUB                             |
| W/O NO.:      | 20201103-116                      |
| SPF NO.:      | SPF3155                           |



FLOW TEST RESULT DATA

| TEST NO. | PRESSURE (PSI) | FLOW (USGPM) | # OF PORTS | PRESSURE (BAR) | FLOW (L/MIN) |
|----------|----------------|--------------|------------|----------------|--------------|
| 1        | 80             | 0            | 0          | 5.52           | 0.0          |
| 2        | 75             | 1250         | 1          | 5.17           | 4731.8       |
| 3        | 72             | 2000         | 2          | 4.96           | 7570.8       |
| *4       | 20             | 6200         | *          |                |              |



# APPENDIX D – SANITARY DATA

**Proposed Sanitary Drainage Design Sheet**

| Street Name            | Up Stream<br>MH | Down Stream<br>MH | Increment |     |           | Cumulative |           | FLOW |                 |               |                        |                  |                 |                       | PIPE             |                |        |                 |                 |            |                  |             |                  |                |
|------------------------|-----------------|-------------------|-----------|-----|-----------|------------|-----------|------|-----------------|---------------|------------------------|------------------|-----------------|-----------------------|------------------|----------------|--------|-----------------|-----------------|------------|------------------|-------------|------------------|----------------|
|                        |                 |                   | Units     | PPU | Areas, ha | P          | Areas, ha | KH   | Pop/Flow<br>l/s | A Gross<br>ha | Infilt. Flow<br>L/s.ha | Infilt. 1<br>l/s | Len. sewer<br>m | Infilt. Flow<br>L/s.m | Infilt. 2<br>l/s | Q Total<br>l/s | L<br>m | Act. Size<br>mm | Nom. Size<br>mm | Grade<br>% | Nom. Cap.<br>l/s | Vel.<br>m/s | Act. Vel.<br>m/s | % Pipe<br>Full |
| New Development        |                 |                   | 10        | 2.7 | 0.1643    | 27         | 0.1643    | 4.36 | 0.41            | 0.1643        | 0.20                   | 0.03             | 50.00           | 0.028                 | 1.40             | 1.85           | 50.00  | 250             | 250             | 1.00       | 59.5             | 1.21        | 0.55             | 3.1            |
| Sewer to Thomas Street |                 |                   |           |     |           | 27         | 0.1643    |      |                 |               |                        |                  |                 |                       | 1.85             |                | 375    | 375             | 0.60            | 135.8      | 1.23             | 0.43        | 1.4              |                |

A = area in ha  
 PPU = persons per unit  
 P = population  
 $KH = 1 + 14 / \{ 4 + (P/1000)^{1/2} \}$   
 Qaverage=302.8 L/capita/day

|                              |      |         |           |
|------------------------------|------|---------|-----------|
| <b>86 Thomas Street</b>      |      |         |           |
| <b>11 Units Townhouse</b>    |      |         |           |
| <b>Sanitary Sewer Design</b> |      |         |           |
| Design:                      | W.L. | Job No. | NT-19-013 |
| Check:                       | G.R. | Date    | Mar. 2020 |
|                              |      | Sheet   | 1 of 1    |

# APPENDIX E – STORMWATER DATA

**Pre-Development**

C

|            |           |      |                     |
|------------|-----------|------|---------------------|
| Total area | 0.1643 ha | 0.25 | Drain to Thomas St. |
|------------|-----------|------|---------------------|

**Post-Development**

C

**post-area:**

|  |                  |             |                     |
|--|------------------|-------------|---------------------|
| <b>A1 - Controlled</b>                   | <b>0.1517</b> ha | <b>0.80</b> | Drain to Stm. Sewer |
| Landscape                                | 0.0242 ha        | 0.25        |                     |
| Permeable Unit Paver                     | 0 ha             | 0.85        |                     |
| Hard Surface                             | 0.1275 ha        | 0.90        |                     |
| <b>A2 - Uncontrolled</b>                 | <b>0.0098</b> ha | <b>0.58</b> | Drain to Thomas St. |
| Landscape                                | 0.0049 ha        | 0.25        |                     |
| Hard Surface                             | 0.0049 ha        | 0.90        |                     |
| <b>A3- Uncontrolled, swale catchment</b> | <b>0.0028</b> ha | <b>0.25</b> | Drain to Thomas St. |
| Landscape                                | 0.0028 ha        | 0.25        |                     |
| Hard Surface                             | 0 ha             | 0.90        |                     |

A2+A3

0.0126

0.5028





**Modified Rational Method - Two Year Storm**  
**Site Flow and Storage Summary**  
 86 Thomas Street, Mississauga  
 File No.: NT-19-013  
 Date: March 2021



**Uncontrolled A2+A3**  
 Drainage Areas  
 Area = **0.0126** ha  
 "C" = **0.50**  
 AC1 = **0.01**  
 Tc = **15.0** min  
 Time Increment = **1.0** min

**Controlled A1**  
 Drainage Areas  
 Area = **0.1517** ha  
 "C" = **0.80**  
 AC2 = **0.12**  
 Tc = **15.0** min  
 Time Increment = **1.0** min

Allowable Rel. Rate = 6.83 L/s  
 Max. Orifice Allowed = 5.78 L/s  
 Actual Orifice Release Rate M = 5.56 L/s

Max. Storage Required = 12.5 m<sup>3</sup>

|                         |                        |
|-------------------------|------------------------|
| 2-Year Return Frequency |                        |
| a=                      | 610.00                 |
| c=                      | -0.7800                |
| l =                     | A*(T+4.6) <sup>2</sup> |

| (1)<br>Time<br>(min) | (2)<br>Rainfall<br>Intensity<br>(mm/hr) | (3)<br>Storm<br>Runoff<br>(Uncon. Post)<br>(m <sup>3</sup> /s) | (4)<br>Runoff<br>Volume<br>(Uncon. Post)<br>(m <sup>3</sup> ) | (5)<br>Storm<br>Runoff<br>(Con. Post)<br>(m <sup>3</sup> /s) | (6)<br>Runoff<br>Volume<br>(Con. Post)<br>(m <sup>3</sup> ) | (7)<br>Storm<br>Actual Runoff<br>(m <sup>3</sup> /s) | (8)<br>Total Runoff<br>Volume<br>(m <sup>3</sup> ) | (9)<br>Total<br>Volume Required<br>(m <sup>3</sup> ) |
|----------------------|---|--|---|--|---|--|--|--|
| (1)                  | (2)                                     | (3) = [(2)*AC1] / 360  | (4) = (1)*(3)*60  | (5) = [(2)*AC2] / 360  | (6) = (1)*(5)*60  |  | (8) = (7)*10*60                                    | (9) = (6)-(8)  |
| 15.0                 | 59.9                                    | 0.0011   | 0.95  | 0.0201   | 18.09   | 0.0066   | 6.0  | 12.1   |
| 16.0                 | 57.6                                    | 0.0010   | 0.97  | 0.0193   | 18.56   | 0.0066   | 6.3  | 12.2   |
| 17.0                 | 55.5                                    | 0.0010   | 1.00  | 0.0186   | 19.00   | 0.0065   | 6.7  | 12.3   |
| 18.0                 | 53.6                                    | 0.0009   | 1.02  | 0.0180   | 19.42   | 0.0065   | 7.0  | 12.4   |
| 19.0                 | 51.8                                    | 0.0009   | 1.04  | 0.0174   | 19.82   | 0.0065   | 7.4  | 12.4   |
| 20.0                 | 50.2                                    | 0.0009   | 1.06  | 0.0168   | 20.20   | 0.0064   | 7.7  | 12.5   |
| 21.0                 | 48.6                                    | 0.0009   | 1.08  | 0.0163   | 20.56   | 0.0064   | 8.1  | 12.5   |
| 22.0                 | 47.2                                    | 0.0008   | 1.10  | 0.0158   | 20.91   | 0.0064   | 8.4  | 12.5   |
| 23.0                 | 45.9                                    | 0.0008   | 1.11  | 0.0154   | 21.24   | 0.0064   | 8.8  | 12.5   |
| 24.0                 | 44.6                                    | 0.0008   | 1.13  | 0.0150   | 21.55   | 0.0063   | 9.1  | 12.4   |
| 25.0                 | 43.4                                    | 0.0008   | 1.15  | 0.0146   | 21.86   | 0.0063   | 9.5  | 12.4   |
| 26.0                 | 42.3                                    | 0.0007   | 1.16  | 0.0142   | 22.15   | 0.0063   | 9.8  | 12.3   |
| 27.0                 | 41.3                                    | 0.0007   | 1.18  | 0.0138   | 22.43   | 0.0063   | 10.2   | 12.2   |
| 28.0                 | 40.3                                    | 0.0007   | 1.19  | 0.0135   | 22.70   | 0.0063   | 10.5   | 12.2   |
| 29.0                 | 39.3                                    | 0.0007   | 1.20  | 0.0132   | 22.97   | 0.0063   | 10.9   | 12.1   |
| 30.0                 | 38.4                                    | 0.0007   | 1.22  | 0.0129   | 23.22   | 0.0062   | 11.2   | 12.0   |
| 31.0                 | 37.6                                    | 0.0007   | 1.23  | 0.0126   | 23.47   | 0.0062   | 11.6   | 11.9   |
| 32.0                 | 36.8                                    | 0.0006   | 1.24  | 0.0123   | 23.71   | 0.0062   | 11.9   | 11.8   |
| 33.0                 | 36.0                                    | 0.0006   | 1.26  | 0.0121   | 23.94   | 0.0062   | 12.3   | 11.7   |
| 34.0                 | 35.3                                    | 0.0006   | 1.27  | 0.0118   | 24.16   | 0.0062   | 12.6   | 11.6   |
| 35.0                 | 34.6                                    | 0.0006   | 1.28  | 0.0116   | 24.38   | 0.0062   | 13.0   | 11.4   |
| 36.0                 | 33.9                                    | 0.0006   | 1.29  | 0.0114   | 24.60   | 0.0062   | 13.3   | 11.3   |
| 37.0                 | 33.3                                    | 0.0006   | 1.30  | 0.0112   | 24.81   | 0.0061   | 13.6   | 11.2   |
| 38.0                 | 32.7                                    | 0.0006   | 1.31  | 0.0110   | 25.01   | 0.0061   | 14.0   | 11.0   |
| 39.0                 | 32.1                                    | 0.0006   | 1.32  | 0.0108   | 25.21   | 0.0061   | 14.3   | 10.9   |
| 40.0                 | 31.5                                    | 0.0006   | 1.33  | 0.0106   | 25.40   | 0.0061   | 14.7   | 10.7   |
| 41.0                 | 31.0                                    | 0.0005   | 1.34  | 0.0104   | 25.59   | 0.0061   | 15.0   | 10.6   |
| 42.0                 | 30.5                                    | 0.0005   | 1.35  | 0.0102   | 25.77   | 0.0061   | 15.4   | 10.4   |
| 43.0                 | 30.0                                    | 0.0005   | 1.36  | 0.0101   | 25.95   | 0.0061   | 15.7   | 10.3   |
| 44.0                 | 29.5                                    | 0.0005   | 1.37  | 0.0099   | 26.13   | 0.0061   | 16.0   | 10.1   |
| 45.0                 | 29.0                                    | 0.0005   | 1.38  | 0.0097   | 26.30   | 0.0061   | 16.4   | 9.9  |
| 46.0                 | 28.6                                    | 0.0005   | 1.39  | 0.0096   | 26.47   | 0.0061   | 16.7   | 9.7  |
| 47.0                 | 28.1                                    | 0.0005   | 1.40  | 0.0094   | 26.64   | 0.0061   | 17.1   | 9.6  |
| 48.0                 | 27.7                                    | 0.0005   | 1.41  | 0.0093   | 26.80   | 0.0060   | 17.4   | 9.4  |
| 49.0                 | 27.3                                    | 0.0005   | 1.41  | 0.0092   | 26.96   | 0.0060   | 17.8   | 9.2  |
| 50.0                 | 26.9                                    | 0.0005   | 1.42  | 0.0090   | 27.11   | 0.0060   | 18.1   | 9.0  |
| 51.0                 | 26.6                                    | 0.0005   | 1.43  | 0.0089   | 27.27   | 0.0060   | 18.4   | 8.8  |
| 52.0                 | 26.2                                    | 0.0005   | 1.44  | 0.0088   | 27.42   | 0.0060   | 18.8   | 8.6  |
| 53.0                 | 25.8                                    | 0.0005   | 1.45  | 0.0087   | 27.57   | 0.0060   | 19.1   | 8.4  |
| 54.0                 | 25.5                                    | 0.0004   | 1.45  | 0.0086   | 27.71   | 0.0060   | 19.5   | 8.2  |
| 55.0                 | 25.2                                    | 0.0004   | 1.46  | 0.0084   | 27.86   | 0.0060   | 19.8   | 8.1  |
| 56.0                 | 24.8                                    | 0.0004   | 1.47  | 0.0083   | 28.00   | 0.0060   | 20.1   | 7.9  |
| 57.0                 | 24.5                                    | 0.0004   | 1.48  | 0.0082   | 28.14   | 0.0060   | 20.5   | 7.6  |
| 58.0                 | 24.2                                    | 0.0004   | 1.48  | 0.0081   | 28.27   | 0.0060   | 20.8   | 7.4  |
| 59.0                 | 23.9                                    | 0.0004   | 1.49  | 0.0080   | 28.41   | 0.0060   | 21.2   | 7.2  |
| 60.0                 | 23.6                                    | 0.0004   | 1.50  | 0.0079   | 28.54   | 0.0060   | 21.5   | 7.0  |
| 61.0                 | 23.3                                    | 0.0004   | 1.50  | 0.0078   | 28.67   | 0.0060   | 21.8   | 6.8  |
| 62.0                 | 23.1                                    | 0.0004   | 1.51  | 0.0077   | 28.80   | 0.0060   | 22.2   | 6.6  |
| 63.0                 | 22.8                                    | 0.0004   | 1.52  | 0.0077   | 28.92   | 0.0060   | 22.5   | 6.4  |
| 64.0                 | 22.5                                    | 0.0004   | 1.52  | 0.0076   | 29.05   | 0.0060   | 22.9   | 6.2  |
| 65.0                 | 22.3                                    | 0.0004   | 1.53  | 0.0075   | 29.17   | 0.0060   | 23.2   | 6.0  |
| 90.0                 | 17.5                                    | 0.0003   | 1.67  | 0.0059   | 31.79   | 0.0062   | 33.5   | 0.0  |
| 120.0                | 14.2                                    | 0.0002   | 1.79  | 0.0047   | 34.19   | 0.0050   | 36.0   | 0.0  |
| 150.0                | 12.0                                    | 0.0002   | 1.89  | 0.0040   | 36.12   | 0.0042   | 38.0   | 0.0  |
| 180.0                | 10.4                                    | 0.0002   | 1.98  | 0.0035   | 37.74   | 0.0037   | 39.7   | 0.0  |
| 210.0                | 9.3                                     | 0.0002   | 2.05  | 0.0031   | 39.16   | 0.0033   | 41.2   | 0.0  |
| 240.0                | 8.4                                     | 0.0001   | 2.12  | 0.0028   | 40.41   | 0.0030   | 42.5   | 0.0  |

**Modified Rational Method - Five Year Storm**  
**Site Flow and Storage Summary**  
 86 Thomas Street, Mississauga  
 File No.: NT-19-013  
 Date: March 2021



**Uncontrolled A2+A3**  
 Drainage Areas  
 Area = **0.0126** ha  
 "C" = **0.50**  
 AC1 = **0.01**  
 Tc = **15.0** min  
 Time Increment = **1.0** min

**Controlled A1**  
 Drainage Areas  
 Area = **0.1517** ha  
 "C" = **0.80**  
 AC2 = **0.12**  
 Tc = **15.0** min  
 Time Increment = **1.0** min

Allowable Rel. Rate = 9.19 L/s  
 Max. Orifice Allowed = 7.77 L/s  
 Actual Orifice Release Rate M = 7.70 L/s  
 Total Actual Flow = 9.11 L/s  
 Max. Storage Required = 16.5 m<sup>3</sup>

|                         |                        |
|-------------------------|------------------------|
| 5-Year Return Frequency |                        |
| a=                      | 820.00                 |
| c=                      | -0.7800                |
| l =                     | A*(T+4.6) <sup>2</sup> |

| (1)<br>Time<br>(min) | (2)<br>Rainfall<br>Intensity<br>(mm/hr) | (3)<br>Storm<br>Runoff<br>(Uncon. Post)<br>(m <sup>3</sup> /s) | (4)<br>Runoff<br>Volume<br>(Uncon. Post)<br>(m <sup>3</sup> ) | (5)<br>Storm<br>Runoff<br>(Con. Post)<br>(m <sup>3</sup> /s) | (6)<br>Runoff<br>Volume<br>(Con. Post)<br>(m <sup>3</sup> ) | (7)<br>Storm<br>Actual Runoff<br>(m <sup>3</sup> /s) | (8)<br>Total Runoff<br>Volume<br>(m <sup>3</sup> ) | (9)<br>Total<br>Volume Required<br>(m <sup>3</sup> ) |
|----------------------|---|--|---|--|---|--|--|--|
| (1)                  | (2)                                     | (3) = [(2)*AC1] / 360  | (4) = (1)*(3)*60  | (5) = [(2)*AC2] / 360  | (6) = (1)*(5)*60  |  | (8) = (7)*10*60                                    | (9) = (6)-(8)  |
| 15.0                 | 80.5                                    | 0.0014   | 1.28  | 0.0270   | 24.31   | 0.0091   | 8.2  | 16.1   |
| 16.0                 | 77.4                                    | 0.0014   | 1.31  | 0.0260   | 24.95   | 0.0091   | 8.7  | 16.3   |
| 17.0                 | 74.6                                    | 0.0013   | 1.34  | 0.0250   | 25.54   | 0.0090   | 9.2  | 16.4   |
| 18.0                 | 72.0                                    | 0.0013   | 1.37  | 0.0242   | 26.11   | 0.0090   | 9.7  | 16.4   |
| 19.0                 | 69.7                                    | 0.0012   | 1.40  | 0.0234   | 26.64   | 0.0089   | 10.2   | 16.5   |
| 20.0                 | 67.4                                    | 0.0012   | 1.42  | 0.0226   | 27.15   | 0.0089   | 10.7   | 16.5   |
| 21.0                 | 65.4                                    | 0.0012   | 1.45  | 0.0219   | 27.64   | 0.0088   | 11.1   | 16.5   |
| 22.0                 | 63.4                                    | 0.0011   | 1.47  | 0.0213   | 28.10   | 0.0088   | 11.6   | 16.5   |
| 23.0                 | 61.6                                    | 0.0011   | 1.50  | 0.0207   | 28.55   | 0.0088   | 12.1   | 16.4   |
| 24.0                 | 60.0                                    | 0.0011   | 1.52  | 0.0201   | 28.97   | 0.0088   | 12.6   | 16.4   |
| 25.0                 | 58.4                                    | 0.0010   | 1.54  | 0.0196   | 29.38   | 0.0087   | 13.1   | 16.3   |
| 26.0                 | 56.9                                    | 0.0010   | 1.56  | 0.0191   | 29.77   | 0.0087   | 13.6   | 16.2   |
| 27.0                 | 55.5                                    | 0.0010   | 1.58  | 0.0186   | 30.15   | 0.0087   | 14.0   | 16.1   |
| 28.0                 | 54.1                                    | 0.0010   | 1.60  | 0.0182   | 30.52   | 0.0086   | 14.5   | 16.0   |
| 29.0                 | 52.9                                    | 0.0009   | 1.62  | 0.0177   | 30.87   | 0.0086   | 15.0   | 15.9   |
| 30.0                 | 51.7                                    | 0.0009   | 1.64  | 0.0173   | 31.22   | 0.0086   | 15.5   | 15.7   |
| 31.0                 | 50.5                                    | 0.0009   | 1.65  | 0.0170   | 31.55   | 0.0086   | 16.0   | 15.6   |
| 32.0                 | 49.5                                    | 0.0009   | 1.67  | 0.0166   | 31.87   | 0.0086   | 16.4   | 15.4   |
| 33.0                 | 48.4                                    | 0.0009   | 1.69  | 0.0163   | 32.18   | 0.0085   | 16.9   | 15.3   |
| 34.0                 | 47.5                                    | 0.0008   | 1.70  | 0.0159   | 32.48   | 0.0085   | 17.4   | 15.1   |
| 35.0                 | 46.5                                    | 0.0008   | 1.72  | 0.0156   | 32.78   | 0.0085   | 17.9   | 14.9   |
| 36.0                 | 45.6                                    | 0.0008   | 1.73  | 0.0153   | 33.07   | 0.0085   | 18.4   | 14.7   |
| 37.0                 | 44.8                                    | 0.0008   | 1.75  | 0.0150   | 33.35   | 0.0085   | 18.8   | 14.5   |
| 38.0                 | 43.9                                    | 0.0008   | 1.76  | 0.0147   | 33.62   | 0.0085   | 19.3   | 14.3   |
| 39.0                 | 43.2                                    | 0.0008   | 1.78  | 0.0145   | 33.88   | 0.0085   | 19.8   | 14.1   |
| 40.0                 | 42.4                                    | 0.0007   | 1.79  | 0.0142   | 34.14   | 0.0084   | 20.3   | 13.9   |
| 41.0                 | 41.7                                    | 0.0007   | 1.80  | 0.0140   | 34.40   | 0.0084   | 20.7   | 13.7   |
| 42.0                 | 41.0                                    | 0.0007   | 1.82  | 0.0137   | 34.64   | 0.0084   | 21.2   | 13.4   |
| 43.0                 | 40.3                                    | 0.0007   | 1.83  | 0.0135   | 34.89   | 0.0084   | 21.7   | 13.2   |
| 44.0                 | 39.6                                    | 0.0007   | 1.84  | 0.0133   | 35.12   | 0.0084   | 22.2   | 13.0   |
| 45.0                 | 39.0                                    | 0.0007   | 1.85  | 0.0131   | 35.36   | 0.0084   | 22.6   | 12.7   |
| 46.0                 | 38.4                                    | 0.0007   | 1.87  | 0.0129   | 35.58   | 0.0084   | 23.1   | 12.5   |
| 47.0                 | 37.8                                    | 0.0007   | 1.88  | 0.0127   | 35.81   | 0.0084   | 23.6   | 12.2   |
| 48.0                 | 37.3                                    | 0.0007   | 1.89  | 0.0125   | 36.02   | 0.0084   | 24.1   | 12.0   |
| 49.0                 | 36.7                                    | 0.0006   | 1.90  | 0.0123   | 36.24   | 0.0083   | 24.5   | 11.7   |
| 50.0                 | 36.2                                    | 0.0006   | 1.91  | 0.0121   | 36.45   | 0.0083   | 25.0   | 11.5   |
| 51.0                 | 35.7                                    | 0.0006   | 1.92  | 0.0120   | 36.66   | 0.0083   | 25.5   | 11.2   |
| 52.0                 | 35.2                                    | 0.0006   | 1.93  | 0.0118   | 36.86   | 0.0083   | 25.9   | 10.9   |
| 53.0                 | 34.7                                    | 0.0006   | 1.94  | 0.0117   | 37.06   | 0.0083   | 26.4   | 10.6   |
| 54.0                 | 34.3                                    | 0.0006   | 1.95  | 0.0115   | 37.25   | 0.0083   | 26.9   | 10.4   |
| 55.0                 | 33.8                                    | 0.0006   | 1.96  | 0.0113   | 37.45   | 0.0083   | 27.4   | 10.1   |
| 56.0                 | 33.4                                    | 0.0006   | 1.97  | 0.0112   | 37.63   | 0.0083   | 27.8   | 9.8  |
| 57.0                 | 33.0                                    | 0.0006   | 1.98  | 0.0111   | 37.82   | 0.0083   | 28.3   | 9.5  |
| 58.0                 | 32.5                                    | 0.0006   | 1.99  | 0.0109   | 38.00   | 0.0083   | 28.8   | 9.2  |
| 59.0                 | 32.1                                    | 0.0006   | 2.00  | 0.0108   | 38.18   | 0.0083   | 29.2   | 8.9  |
| 60.0                 | 31.8                                    | 0.0006   | 2.01  | 0.0107   | 38.36   | 0.0083   | 29.7   | 8.6  |
| 61.0                 | 31.4                                    | 0.0006   | 2.02  | 0.0105   | 38.54   | 0.0082   | 30.2   | 8.4  |
| 62.0                 | 31.0                                    | 0.0005   | 2.03  | 0.0104   | 38.71   | 0.0082   | 30.7   | 8.1  |
| 63.0                 | 30.7                                    | 0.0005   | 2.04  | 0.0103   | 38.88   | 0.0082   | 31.1   | 7.8  |
| 64.0                 | 30.3                                    | 0.0005   | 2.05  | 0.0102   | 39.05   | 0.0082   | 31.6   | 7.4  |
| 65.0                 | 30.0                                    | 0.0005   | 2.06  | 0.0101   | 39.21   | 0.0082   | 32.1   | 7.1  |
| 90.0                 | 23.6                                    | 0.0004   | 2.24  | 0.0079   | 42.73   | 0.0083   | 45.0   | 0.0  |
| 120.0                | 19.0                                    | 0.0003   | 2.41  | 0.0064   | 45.96   | 0.0067   | 48.4   | 0.0  |
| 150.0                | 16.1                                    | 0.0003   | 2.55  | 0.0054   | 48.56   | 0.0057   | 51.1   | 0.0  |
| 180.0                | 14.0                                    | 0.0002   | 2.66  | 0.0047   | 50.74   | 0.0049   | 53.4   | 0.0  |
| 210.0                | 12.4                                    | 0.0002   | 2.76  | 0.0042   | 52.64   | 0.0044   | 55.4   | 0.0  |
| 240.0                | 11.2                                    | 0.0002   | 2.85  | 0.0038   | 54.32   | 0.0040   | 57.2   | 0.0  |

**Modified Rational Method - Ten Year Storm**

**Site Flow and Storage Summary**  
 86 Thomas Street, Mississauga  
 File No.: NT-19-013  
 Date: March 2021



**Uncontrolled A2+A3**

Drainage Areas  
 Area = **0.0126** ha  
 "C" = **0.50**  
 AC1 = **0.01**  
 Tc = **15.0** min  
 Time Increment = **1.0** min

**Controlled A1**

Drainage Areas  
 Area = **0.1517** ha  
 "C" = **0.80**  
 AC2 = **0.12**  
 Tc = **15.0** min  
 Time Increment = **1.0** min

Allowable Rel. Rate = 11.31 L/s  
 Max. Orifice Allowed = 9.56 L/s  
 Actual Orifice Release Rate M = 9.49 L/s  
 Total Actual Flow = 11.24 L/s

Max. Storage Required = **20.3** m<sup>3</sup>

|                          |                        |
|--------------------------|------------------------|
| 10-Year Return Frequency |                        |
| a =                      | 1010.00                |
| c =                      | -0.7800                |
| l =                      | A*(T+4.6) <sup>c</sup> |

| (1)<br>Time<br>(min) | (2)<br>Rainfall<br>Intensity<br>(mm/hr) | (3)<br>Storm<br>Runoff<br>(Uncon. Post)<br>(m <sup>3</sup> /s) | (4)<br>Runoff<br>Volume<br>(Uncon. Post)<br>(m <sup>3</sup> ) | (5)<br>Storm<br>Runoff<br>(Con. Post)<br>(m <sup>3</sup> /s) | (6)<br>Runoff<br>Volume<br>(Con. Post)<br>(m <sup>3</sup> ) | (7)<br>Storm<br>Actual Runoff<br>(m <sup>3</sup> /s) | (8)<br>Total Runoff<br>Volume<br>(m <sup>3</sup> ) | (9)<br>Total<br>Volume Required<br>(m <sup>3</sup> ) |  |
|----------------------|---|--|---|--|---|--|--|--|--|
| (1)                  | (2)                                     | (3) = [(2)*AC1] / 360  |   | (4) = (1)*(3)*60   |   | (5) = [(2)*AC2] / 360                                |  | (6) = (1)*(5)*60                                     |  |
|                      |   |  |   |  |   |  | (8) = (7)*10*60                                    | (9) = (6)-(8)  |  |
| 15.0                 | 99.2                                    | 0.0017   | 1.57  | 0.0333   | 29.95   | 0.0112   | 10.1   | 19.8   |  |
| 16.0                 | 95.4                                    | 0.0017   | 1.61  | 0.0320   | 30.73   | 0.0112   | 10.7   | 20.0   |  |
| 17.0                 | 91.9                                    | 0.0016   | 1.65  | 0.0308   | 31.46   | 0.0111   | 11.3   | 20.1   |  |
| 18.0                 | 88.7                                    | 0.0016   | 1.69  | 0.0298   | 32.16   | 0.0111   | 11.9   | 20.2   |  |
| 19.0                 | 85.8                                    | 0.0015   | 1.72  | 0.0288   | 32.82   | 0.0110   | 12.5   | 20.3   |  |
| 20.0                 | 83.1                                    | 0.0015   | 1.75  | 0.0279   | 33.45   | 0.0110   | 13.1   | 20.3   |  |
| 21.0                 | 80.5                                    | 0.0014   | 1.79  | 0.0270   | 34.04   | 0.0109   | 13.7   | 20.3   |  |
| 22.0                 | 78.1                                    | 0.0014   | 1.82  | 0.0262   | 34.61   | 0.0109   | 14.3   | 20.3   |  |
| 23.0                 | 75.9                                    | 0.0013   | 1.84  | 0.0255   | 35.16   | 0.0108   | 14.9   | 20.2   |  |
| 24.0                 | 73.9                                    | 0.0013   | 1.87  | 0.0248   | 35.68   | 0.0108   | 15.5   | 20.1   |  |
| 25.0                 | 71.9                                    | 0.0013   | 1.90  | 0.0241   | 36.19   | 0.0108   | 16.1   | 20.1   |  |
| 26.0                 | 70.1                                    | 0.0012   | 1.92  | 0.0235   | 36.67   | 0.0107   | 16.7   | 19.9   |  |
| 27.0                 | 68.3                                    | 0.0012   | 1.95  | 0.0229   | 37.14   | 0.0107   | 17.3   | 19.8   |  |
| 28.0                 | 66.7                                    | 0.0012   | 1.97  | 0.0224   | 37.59   | 0.0107   | 17.9   | 19.7   |  |
| 29.0                 | 65.1                                    | 0.0011   | 1.99  | 0.0219   | 38.03   | 0.0106   | 18.5   | 19.5   |  |
| 30.0                 | 63.7                                    | 0.0011   | 2.02  | 0.0214   | 38.45   | 0.0106   | 19.1   | 19.3   |  |
| 31.0                 | 62.3                                    | 0.0011   | 2.04  | 0.0209   | 38.86   | 0.0106   | 19.7   | 19.2   |  |
| 32.0                 | 60.9                                    | 0.0011   | 2.06  | 0.0204   | 39.25   | 0.0106   | 20.3   | 19.0   |  |
| 33.0                 | 59.7                                    | 0.0010   | 2.08  | 0.0200   | 39.64   | 0.0105   | 20.9   | 18.8   |  |
| 34.0                 | 58.4                                    | 0.0010   | 2.10  | 0.0196   | 40.01   | 0.0105   | 21.5   | 18.5   |  |
| 35.0                 | 57.3                                    | 0.0010   | 2.12  | 0.0192   | 40.37   | 0.0105   | 22.1   | 18.3   |  |
| 36.0                 | 56.2                                    | 0.0010   | 2.14  | 0.0189   | 40.73   | 0.0105   | 22.6   | 18.1   |  |
| 37.0                 | 55.1                                    | 0.0010   | 2.15  | 0.0185   | 41.07   | 0.0105   | 23.2   | 17.8   |  |
| 38.0                 | 54.1                                    | 0.0010   | 2.17  | 0.0182   | 41.41   | 0.0104   | 23.8   | 17.6   |  |
| 39.0                 | 53.2                                    | 0.0009   | 2.19  | 0.0178   | 41.74   | 0.0104   | 24.4   | 17.3   |  |
| 40.0                 | 52.2                                    | 0.0009   | 2.21  | 0.0175   | 42.05   | 0.0104   | 25.0   | 17.1   |  |
| 41.0                 | 51.3                                    | 0.0009   | 2.22  | 0.0172   | 42.37   | 0.0104   | 25.6   | 16.8   |  |
| 42.0                 | 50.5                                    | 0.0009   | 2.24  | 0.0169   | 42.67   | 0.0104   | 26.2   | 16.5   |  |
| 43.0                 | 49.6                                    | 0.0009   | 2.25  | 0.0167   | 42.97   | 0.0104   | 26.7   | 16.2   |  |
| 44.0                 | 48.8                                    | 0.0009   | 2.27  | 0.0164   | 43.26   | 0.0104   | 27.3   | 15.9   |  |
| 45.0                 | 48.1                                    | 0.0008   | 2.28  | 0.0161   | 43.55   | 0.0103   | 27.9   | 15.6   |  |
| 46.0                 | 47.3                                    | 0.0008   | 2.30  | 0.0159   | 43.83   | 0.0103   | 28.5   | 15.3   |  |
| 47.0                 | 46.6                                    | 0.0008   | 2.31  | 0.0156   | 44.10   | 0.0103   | 29.1   | 15.0   |  |
| 48.0                 | 45.9                                    | 0.0008   | 2.33  | 0.0154   | 44.37   | 0.0103   | 29.7   | 14.7   |  |
| 49.0                 | 45.2                                    | 0.0008   | 2.34  | 0.0152   | 44.64   | 0.0103   | 30.3   | 14.4   |  |
| 50.0                 | 44.6                                    | 0.0008   | 2.35  | 0.0150   | 44.89   | 0.0103   | 30.8   | 14.1   |  |
| 51.0                 | 44.0                                    | 0.0008   | 2.37  | 0.0148   | 45.15   | 0.0103   | 31.4   | 13.7   |  |
| 52.0                 | 43.4                                    | 0.0008   | 2.38  | 0.0146   | 45.40   | 0.0103   | 32.0   | 13.4   |  |
| 53.0                 | 42.8                                    | 0.0008   | 2.39  | 0.0144   | 45.64   | 0.0102   | 32.6   | 13.1   |  |
| 54.0                 | 42.2                                    | 0.0007   | 2.41  | 0.0142   | 45.88   | 0.0102   | 33.2   | 12.7   |  |
| 55.0                 | 41.7                                    | 0.0007   | 2.42  | 0.0140   | 46.12   | 0.0102   | 33.7   | 12.4   |  |
| 56.0                 | 41.1                                    | 0.0007   | 2.43  | 0.0138   | 46.35   | 0.0102   | 34.3   | 12.0   |  |
| 57.0                 | 40.6                                    | 0.0007   | 2.44  | 0.0136   | 46.58   | 0.0102   | 34.9   | 11.7   |  |
| 58.0                 | 40.1                                    | 0.0007   | 2.45  | 0.0135   | 46.81   | 0.0102   | 35.5   | 11.3   |  |
| 59.0                 | 39.6                                    | 0.0007   | 2.47  | 0.0133   | 47.03   | 0.0102   | 36.1   | 11.0   |  |
| 60.0                 | 39.1                                    | 0.0007   | 2.48  | 0.0131   | 47.25   | 0.0102   | 36.7   | 10.6   |  |
| 61.0                 | 38.6                                    | 0.0007   | 2.49  | 0.0130   | 47.47   | 0.0102   | 37.2   | 10.2   |  |
| 62.0                 | 38.2                                    | 0.0007   | 2.50  | 0.0128   | 47.68   | 0.0102   | 37.8   | 9.9  |  |
| 63.0                 | 37.8                                    | 0.0007   | 2.51  | 0.0127   | 47.89   | 0.0102   | 38.4   | 9.5  |  |
| 64.0                 | 37.3                                    | 0.0007   | 2.52  | 0.0125   | 48.09   | 0.0101   | 39.0   | 9.1  |  |
| 65.0                 | 36.9                                    | 0.0006   | 2.53  | 0.0124   | 48.30   | 0.0101   | 39.6   | 8.7  |  |
| 90.0                 | 29.0                                    | 0.0005   | 2.76  | 0.0097   | 52.64   | 0.0103   | 55.4   | 0.0  |  |
| 120.0                | 23.4                                    | 0.0004   | 2.97  | 0.0079   | 56.61   | 0.0083   | 59.6   | 0.0  |  |
| 150.0                | 19.8                                    | 0.0003   | 3.14  | 0.0066   | 59.81   | 0.0070   | 62.9   | 0.0  |  |
| 180.0                | 17.2                                    | 0.0003   | 3.28  | 0.0058   | 62.50   | 0.0061   | 65.8   | 0.0  |  |
| 210.0                | 15.3                                    | 0.0003   | 3.40  | 0.0051   | 64.83   | 0.0054   | 68.2   | 0.0  |  |
| 240.0                | 13.8                                    | 0.0002   | 3.51  | 0.0046   | 66.90   | 0.0049   | 70.4   | 0.0  |  |

**Modified Rational Method - Twenty-Five Year Storm**  
**Site Flow and Storage Summary**  
 86 Thomas Street, Mississauga  
 File No.: NT-19-013  
 Date: March 2021



**Uncontrolled A2+A3**

Drainage Areas  
 Area = **0.0126** ha  
 "C" = **0.55**  
 AC1 = **0.01**  
 Tc = **15.0** min  
 Time Increment = **1.0** min

**Controlled A1**

Drainage Areas  
 Area = **0.1517** ha  
 "C" = **0.88**  
 AC2 = **0.13**  
 Tc = **15.0** min  
 Time Increment = **1.0** min

Allowable Rel. Rate = 14.29 L/s  
 Max. Orifice Allowed = 12.09 L/s  
 Actual Orifice Release Rate M = 11.90 L/s  
 Total actual flow = 14.10 L/s

Max. Storage Required = **25.8** m<sup>3</sup>

|                          |                        |
|--------------------------|------------------------|
| 25-Year Return Frequency |                        |
| a =                      | 1160.00                |
| c =                      | -0.7800                |
| l =                      | A*(T+4.6) <sup>2</sup> |

| (1)<br>Time<br>(min) | (2)<br>Rainfall<br>Intensity<br>(mm/hr) | (3)<br>Storm<br>Runoff<br>(Uncon. Post)<br>(m <sup>3</sup> /s) | (4)<br>Runoff<br>Volume<br>(Uncon. Post)<br>(m <sup>3</sup> ) | (5)<br>Storm<br>Runoff<br>(Con. Post)<br>(m <sup>3</sup> /s) | (6)<br>Runoff<br>Volume<br>(Con. Post)<br>(m <sup>3</sup> ) | (7)<br>Storm<br>Actual Runoff<br>(m <sup>3</sup> /s) | (8)<br>Total Runoff<br>Volume<br>(m <sup>3</sup> ) | (9)<br>Total<br>Volume Required<br>(m <sup>3</sup> ) |  |           |  |                 |  |               |  |
|----------------------|---|--|---|--|---|--|--|--|--|-----------|--|-----------------|--|---------------|--|
| (1)                  | (2)                                     | (3) = [(2)*AC1] / 360  |   | (4) = (1)*(3)*60   |   | (5) = [(2)*AC2] / 360                                |  | (6) = (1)*(5)*60                                     |  | (7) = (3) |  | (8) = (7)*10*60 |  | (9) = (6)-(8) |  |
| 15.0                 | 113.9                                   | 0.0022   | 1.98  | 0.0420   | 37.84   | 0.0141   | 12.7   | 25.1   |  |           |  |                 |  |               |  |
| 16.0                 | 109.6                                   | 0.0021   | 2.04  | 0.0404   | 38.82   | 0.0140   | 13.5   | 25.4   |  |           |  |                 |  |               |  |
| 17.0                 | 105.6                                   | 0.0020   | 2.08  | 0.0390   | 39.75   | 0.0139   | 14.2   | 25.5   |  |           |  |                 |  |               |  |
| 18.0                 | 101.9                                   | 0.0020   | 2.13  | 0.0376   | 40.63   | 0.0139   | 15.0   | 25.6   |  |           |  |                 |  |               |  |
| 19.0                 | 98.5                                    | 0.0019   | 2.17  | 0.0364   | 41.46   | 0.0138   | 15.7   | 25.7   |  |           |  |                 |  |               |  |
| 20.0                 | 95.4                                    | 0.0018   | 2.22  | 0.0352   | 42.25   | 0.0137   | 16.5   | 25.8   |  |           |  |                 |  |               |  |
| 21.0                 | 92.5                                    | 0.0018   | 2.26  | 0.0341   | 43.01   | 0.0137   | 17.2   | 25.8   |  |           |  |                 |  |               |  |
| 22.0                 | 89.8                                    | 0.0017   | 2.29  | 0.0331   | 43.73   | 0.0136   | 18.0   | 25.7   |  |           |  |                 |  |               |  |
| 23.0                 | 87.2                                    | 0.0017   | 2.33  | 0.0322   | 44.42   | 0.0136   | 18.8   | 25.7   |  |           |  |                 |  |               |  |
| 24.0                 | 84.8                                    | 0.0016   | 2.36  | 0.0313   | 45.08   | 0.0135   | 19.5   | 25.6   |  |           |  |                 |  |               |  |
| 25.0                 | 82.6                                    | 0.0016   | 2.40  | 0.0305   | 45.72   | 0.0135   | 20.2   | 25.5   |  |           |  |                 |  |               |  |
| 26.0                 | 80.5                                    | 0.0016   | 2.43  | 0.0297   | 46.33   | 0.0135   | 21.0   | 25.3   |  |           |  |                 |  |               |  |
| 27.0                 | 78.5                                    | 0.0015   | 2.46  | 0.0290   | 46.92   | 0.0134   | 21.7   | 25.2   |  |           |  |                 |  |               |  |
| 28.0                 | 76.6                                    | 0.0015   | 2.49  | 0.0283   | 47.49   | 0.0134   | 22.5   | 25.0   |  |           |  |                 |  |               |  |
| 29.0                 | 74.8                                    | 0.0014   | 2.52  | 0.0276   | 48.04   | 0.0133   | 23.2   | 24.8   |  |           |  |                 |  |               |  |
| 30.0                 | 73.1                                    | 0.0014   | 2.55  | 0.0270   | 48.57   | 0.0133   | 24.0   | 24.6   |  |           |  |                 |  |               |  |
| 31.0                 | 71.5                                    | 0.0014   | 2.57  | 0.0264   | 49.09   | 0.0133   | 24.7   | 24.4   |  |           |  |                 |  |               |  |
| 32.0                 | 70.0                                    | 0.0014   | 2.60  | 0.0258   | 49.59   | 0.0133   | 25.4   | 24.1   |  |           |  |                 |  |               |  |
| 33.0                 | 68.5                                    | 0.0013   | 2.63  | 0.0253   | 50.08   | 0.0132   | 26.2   | 23.9   |  |           |  |                 |  |               |  |
| 34.0                 | 67.1                                    | 0.0013   | 2.65  | 0.0248   | 50.55   | 0.0132   | 26.9   | 23.6   |  |           |  |                 |  |               |  |
| 35.0                 | 65.8                                    | 0.0013   | 2.67  | 0.0243   | 51.01   | 0.0132   | 27.7   | 23.3   |  |           |  |                 |  |               |  |
| 36.0                 | 64.5                                    | 0.0012   | 2.70  | 0.0238   | 51.45   | 0.0131   | 28.4   | 23.1   |  |           |  |                 |  |               |  |
| 37.0                 | 63.3                                    | 0.0012   | 2.72  | 0.0234   | 51.89   | 0.0131   | 29.1   | 22.7   |  |           |  |                 |  |               |  |
| 38.0                 | 62.2                                    | 0.0012   | 2.74  | 0.0229   | 52.31   | 0.0131   | 29.9   | 22.4   |  |           |  |                 |  |               |  |
| 39.0                 | 61.0                                    | 0.0012   | 2.77  | 0.0225   | 52.73   | 0.0131   | 30.6   | 22.1   |  |           |  |                 |  |               |  |
| 40.0                 | 60.0                                    | 0.0012   | 2.79  | 0.0221   | 53.13   | 0.0131   | 31.3   | 21.8   |  |           |  |                 |  |               |  |
| 41.0                 | 58.9                                    | 0.0011   | 2.81  | 0.0218   | 53.53   | 0.0130   | 32.1   | 21.4   |  |           |  |                 |  |               |  |
| 42.0                 | 58.0                                    | 0.0011   | 2.83  | 0.0214   | 53.91   | 0.0130   | 32.8   | 21.1   |  |           |  |                 |  |               |  |
| 43.0                 | 57.0                                    | 0.0011   | 2.85  | 0.0210   | 54.29   | 0.0130   | 33.5   | 20.7   |  |           |  |                 |  |               |  |
| 44.0                 | 56.1                                    | 0.0011   | 2.87  | 0.0207   | 54.66   | 0.0130   | 34.3   | 20.4   |  |           |  |                 |  |               |  |
| 45.0                 | 55.2                                    | 0.0011   | 2.89  | 0.0204   | 55.02   | 0.0130   | 35.0   | 20.0   |  |           |  |                 |  |               |  |
| 46.0                 | 54.4                                    | 0.0011   | 2.90  | 0.0201   | 55.37   | 0.0130   | 35.7   | 19.6   |  |           |  |                 |  |               |  |
| 47.0                 | 53.5                                    | 0.0010   | 2.92  | 0.0198   | 55.72   | 0.0129   | 36.5   | 19.2   |  |           |  |                 |  |               |  |
| 48.0                 | 52.7                                    | 0.0010   | 2.94  | 0.0195   | 56.06   | 0.0129   | 37.2   | 18.8   |  |           |  |                 |  |               |  |
| 49.0                 | 52.0                                    | 0.0010   | 2.96  | 0.0192   | 56.39   | 0.0129   | 37.9   | 18.4   |  |           |  |                 |  |               |  |
| 50.0                 | 51.2                                    | 0.0010   | 2.97  | 0.0189   | 56.72   | 0.0129   | 38.7   | 18.0   |  |           |  |                 |  |               |  |
| 51.0                 | 50.5                                    | 0.0010   | 2.99  | 0.0186   | 57.04   | 0.0129   | 39.4   | 17.6   |  |           |  |                 |  |               |  |
| 52.0                 | 49.8                                    | 0.0010   | 3.01  | 0.0184   | 57.36   | 0.0129   | 40.1   | 17.2   |  |           |  |                 |  |               |  |
| 53.0                 | 49.1                                    | 0.0010   | 3.02  | 0.0181   | 57.67   | 0.0129   | 40.9   | 16.8   |  |           |  |                 |  |               |  |
| 54.0                 | 48.5                                    | 0.0009   | 3.04  | 0.0179   | 57.97   | 0.0128   | 41.6   | 16.4   |  |           |  |                 |  |               |  |
| 55.0                 | 47.8                                    | 0.0009   | 3.06  | 0.0177   | 58.27   | 0.0128   | 42.3   | 15.9   |  |           |  |                 |  |               |  |
| 56.0                 | 47.2                                    | 0.0009   | 3.07  | 0.0174   | 58.56   | 0.0128   | 43.1   | 15.5   |  |           |  |                 |  |               |  |
| 57.0                 | 46.6                                    | 0.0009   | 3.09  | 0.0172   | 58.85   | 0.0128   | 43.8   | 15.1   |  |           |  |                 |  |               |  |
| 58.0                 | 46.0                                    | 0.0009   | 3.10  | 0.0170   | 59.14   | 0.0128   | 44.5   | 14.6   |  |           |  |                 |  |               |  |
| 59.0                 | 45.5                                    | 0.0009   | 3.12  | 0.0168   | 59.42   | 0.0128   | 45.2   | 14.2   |  |           |  |                 |  |               |  |
| 60.0                 | 44.9                                    | 0.0009   | 3.13  | 0.0166   | 59.69   | 0.0128   | 46.0   | 13.7   |  |           |  |                 |  |               |  |
| 61.0                 | 44.4                                    | 0.0009   | 3.14  | 0.0164   | 59.97   | 0.0128   | 46.7   | 13.3   |  |           |  |                 |  |               |  |
| 62.0                 | 43.9                                    | 0.0008   | 3.16  | 0.0162   | 60.23   | 0.0127   | 47.4   | 12.8   |  |           |  |                 |  |               |  |
| 63.0                 | 43.4                                    | 0.0008   | 3.17  | 0.0160   | 60.50   | 0.0127   | 48.2   | 12.3   |  |           |  |                 |  |               |  |
| 64.0                 | 42.9                                    | 0.0008   | 3.19  | 0.0158   | 60.76   | 0.0127   | 48.9   | 11.9   |  |           |  |                 |  |               |  |
| 65.0                 | 42.4                                    | 0.0008   | 3.20  | 0.0156   | 61.02   | 0.0127   | 49.6   | 11.4   |  |           |  |                 |  |               |  |
| 90.0                 | 33.4                                    | 0.0006   | 3.49  | 0.0123   | 66.50   | 0.0130   | 70.0   | 0.0  |  |           |  |                 |  |               |  |
| 120.0                | 26.9                                    | 0.0005   | 3.75  | 0.0099   | 71.52   | 0.0105   | 75.3   | 0.0  |  |           |  |                 |  |               |  |
| 150.0                | 22.7                                    | 0.0004   | 3.96  | 0.0084   | 75.56   | 0.0088   | 79.5   | 0.0  |  |           |  |                 |  |               |  |
| 180.0                | 19.8                                    | 0.0004   | 4.14  | 0.0073   | 78.95   | 0.0077   | 83.1   | 0.0  |  |           |  |                 |  |               |  |
| 210.0                | 17.6                                    | 0.0003   | 4.30  | 0.0065   | 81.91   | 0.0068   | 86.2   | 0.0  |  |           |  |                 |  |               |  |
| 240.0                | 15.9                                    | 0.0003   | 4.43  | 0.0059   | 84.52   | 0.0062   | 89.0   | 0.0  |  |           |  |                 |  |               |  |

**Modified Rational Method - Fifty Year Storm**  
**Site Flow and Storage Summary**  
 86 Thomas Street, Mississauga  
 File No.: NT-19-013  
 Date: March 2021



**Uncontrolled A2+A3**  
 Drainage Areas  
 Area = **0.0126** ha  
 "C" = **0.60**  
 AC1 = **0.01**  
 Tc = **15.0** min  
 Time Increment = **1.0** min

**Controlled A1**  
 Drainage Areas  
 Area = **0.1517** ha  
 "C" = **0.96**  
 AC2 = **0.14**  
 Tc = **15.0** min  
 Time Increment = **1.0** min

Allowable Rel. Rate = 17.41 L/s  
 Max. Orifice Allowed = 14.73 L/s  
 Actual Orifice Release Rate M = 14.35 L/s  
 Total actual flow = 17.04 L/s  
 Max. Storage Required = **31.6** m<sup>3</sup>

|                          |                        |
|--------------------------|------------------------|
| 50-Year Return Frequency |                        |
| a =                      | 1300.00                |
| c =                      | -0.7800                |
| l =                      | A*(T+4.7) <sup>2</sup> |

| (1)<br>Time<br>(min) | (2)<br>Rainfall<br>Intensity<br>(mm/hr) | (3)<br>Storm<br>Runoff<br>(Uncon. Post)<br>(m <sup>3</sup> /s) | (4)<br>Runoff<br>Volume<br>(Uncon. Post)<br>(m <sup>3</sup> ) | (5)<br>Storm<br>Runoff<br>(Con. Post)<br>(m <sup>3</sup> /s) | (6)<br>Runoff<br>Volume<br>(Con. Post)<br>(m <sup>3</sup> ) | (7)<br>Storm<br>Actual Runoff<br>(m <sup>3</sup> /s) | (8)<br>Total Runoff<br>Volume<br>(m <sup>3</sup> ) | (9)<br>Total<br>Volume Required<br>(m <sup>3</sup> ) |
|----------------------|---|--|---|--|---|--|--|--|
| (1)                  | (2)                                     | (3) = [(2)*AC1] / 360  | (4) = (1)*(3)*60  | (5) = [(2)*AC2] / 360  | (6) = (1)*(5)*60  |  | (8) = (7)*10*60                                    | (9) = (6)-(8)  |
| 15.0                 | 127.1                                   | 0.0027   | 2.42  | 0.0512   | 46.07   | 0.0170   | 15.3   | 30.7   |
| 16.0                 | 122.3                                   | 0.0026   | 2.48  | 0.0493   | 47.28   | 0.0169   | 16.3   | 31.0   |
| 17.0                 | 117.9                                   | 0.0025   | 2.54  | 0.0475   | 48.42   | 0.0168   | 17.2   | 31.2   |
| 18.0                 | 113.8                                   | 0.0024   | 2.60  | 0.0458   | 49.50   | 0.0168   | 18.1   | 31.4   |
| 19.0                 | 110.1                                   | 0.0023   | 2.65  | 0.0443   | 50.52   | 0.0167   | 19.0   | 31.5   |
| 20.0                 | 106.6                                   | 0.0023   | 2.70  | 0.0429   | 51.50   | 0.0166   | 19.9   | 31.6   |
| 21.0                 | 103.3                                   | 0.0022   | 2.75  | 0.0416   | 52.42   | 0.0165   | 20.8   | 31.6   |
| 22.0                 | 100.3                                   | 0.0021   | 2.80  | 0.0404   | 53.31   | 0.0165   | 21.7   | 31.6   |
| 23.0                 | 97.5                                    | 0.0021   | 2.84  | 0.0392   | 54.15   | 0.0164   | 22.6   | 31.5   |
| 24.0                 | 94.8                                    | 0.0020   | 2.88  | 0.0382   | 54.97   | 0.0164   | 23.5   | 31.4   |
| 25.0                 | 92.3                                    | 0.0019   | 2.92  | 0.0372   | 55.75   | 0.0163   | 24.5   | 31.3   |
| 26.0                 | 89.9                                    | 0.0019   | 2.96  | 0.0362   | 56.50   | 0.0163   | 25.4   | 31.1   |
| 27.0                 | 87.7                                    | 0.0019   | 3.00  | 0.0353   | 57.22   | 0.0162   | 26.3   | 31.0   |
| 28.0                 | 85.6                                    | 0.0018   | 3.04  | 0.0345   | 57.92   | 0.0162   | 27.1   | 30.8   |
| 29.0                 | 83.6                                    | 0.0018   | 3.07  | 0.0337   | 58.60   | 0.0161   | 28.0   | 30.6   |
| 30.0                 | 81.7                                    | 0.0017   | 3.11  | 0.0329   | 59.25   | 0.0161   | 28.9   | 30.3   |
| 31.0                 | 80.0                                    | 0.0017   | 3.14  | 0.0322   | 59.89   | 0.0160   | 29.8   | 30.0   |
| 32.0                 | 78.3                                    | 0.0017   | 3.17  | 0.0315   | 60.50   | 0.0160   | 30.7   | 29.8   |
| 33.0                 | 76.6                                    | 0.0016   | 3.20  | 0.0309   | 61.10   | 0.0160   | 31.6   | 29.5   |
| 34.0                 | 75.1                                    | 0.0016   | 3.23  | 0.0302   | 61.67   | 0.0159   | 32.5   | 29.2   |
| 35.0                 | 73.6                                    | 0.0016   | 3.26  | 0.0296   | 62.24   | 0.0159   | 33.4   | 28.8   |
| 36.0                 | 72.2                                    | 0.0015   | 3.29  | 0.0291   | 62.79   | 0.0159   | 34.3   | 28.5   |
| 37.0                 | 70.8                                    | 0.0015   | 3.32  | 0.0285   | 63.32   | 0.0158   | 35.2   | 28.1   |
| 38.0                 | 69.5                                    | 0.0015   | 3.35  | 0.0280   | 63.84   | 0.0158   | 36.1   | 27.8   |
| 39.0                 | 68.3                                    | 0.0014   | 3.37  | 0.0275   | 64.35   | 0.0158   | 37.0   | 27.4   |
| 40.0                 | 67.1                                    | 0.0014   | 3.40  | 0.0270   | 64.84   | 0.0158   | 37.8   | 27.0   |
| 41.0                 | 65.9                                    | 0.0014   | 3.43  | 0.0266   | 65.33   | 0.0157   | 38.7   | 26.6   |
| 42.0                 | 64.8                                    | 0.0014   | 3.45  | 0.0261   | 65.80   | 0.0157   | 39.6   | 26.2   |
| 43.0                 | 63.8                                    | 0.0013   | 3.47  | 0.0257   | 66.26   | 0.0157   | 40.5   | 25.8   |
| 44.0                 | 62.8                                    | 0.0013   | 3.50  | 0.0253   | 66.71   | 0.0157   | 41.4   | 25.3   |
| 45.0                 | 61.8                                    | 0.0013   | 3.52  | 0.0249   | 67.16   | 0.0157   | 42.3   | 24.9   |
| 46.0                 | 60.8                                    | 0.0013   | 3.54  | 0.0245   | 67.59   | 0.0156   | 43.2   | 24.4   |
| 47.0                 | 59.9                                    | 0.0013   | 3.57  | 0.0241   | 68.02   | 0.0156   | 44.0   | 24.0   |
| 48.0                 | 59.0                                    | 0.0012   | 3.59  | 0.0238   | 68.43   | 0.0156   | 44.9   | 23.5   |
| 49.0                 | 58.2                                    | 0.0012   | 3.61  | 0.0234   | 68.84   | 0.0156   | 45.8   | 23.0   |
| 50.0                 | 57.3                                    | 0.0012   | 3.63  | 0.0231   | 69.24   | 0.0156   | 46.7   | 22.6   |
| 51.0                 | 56.5                                    | 0.0012   | 3.65  | 0.0228   | 69.64   | 0.0155   | 47.6   | 22.1   |
| 52.0                 | 55.7                                    | 0.0012   | 3.67  | 0.0224   | 70.02   | 0.0155   | 48.5   | 21.6   |
| 53.0                 | 55.0                                    | 0.0012   | 3.69  | 0.0221   | 70.40   | 0.0155   | 49.3   | 21.1   |
| 54.0                 | 54.3                                    | 0.0011   | 3.71  | 0.0218   | 70.78   | 0.0155   | 50.2   | 20.6   |
| 55.0                 | 53.5                                    | 0.0011   | 3.73  | 0.0216   | 71.14   | 0.0155   | 51.1   | 20.1   |
| 56.0                 | 52.9                                    | 0.0011   | 3.75  | 0.0213   | 71.51   | 0.0155   | 52.0   | 19.5   |
| 57.0                 | 52.2                                    | 0.0011   | 3.77  | 0.0210   | 71.86   | 0.0155   | 52.9   | 19.0   |
| 58.0                 | 51.5                                    | 0.0011   | 3.79  | 0.0208   | 72.21   | 0.0154   | 53.7   | 18.5   |
| 59.0                 | 50.9                                    | 0.0011   | 3.80  | 0.0205   | 72.55   | 0.0154   | 54.6   | 17.9   |
| 60.0                 | 50.3                                    | 0.0011   | 3.82  | 0.0202   | 72.89   | 0.0154   | 55.5   | 17.4   |
| 61.0                 | 49.7                                    | 0.0010   | 3.84  | 0.0200   | 73.23   | 0.0154   | 56.4   | 16.9   |
| 62.0                 | 49.1                                    | 0.0010   | 3.86  | 0.0198   | 73.56   | 0.0154   | 57.2   | 16.3   |
| 63.0                 | 48.5                                    | 0.0010   | 3.87  | 0.0195   | 73.88   | 0.0154   | 58.1   | 15.8   |
| 64.0                 | 48.0                                    | 0.0010   | 3.89  | 0.0193   | 74.20   | 0.0154   | 59.0   | 15.2   |
| 65.0                 | 47.4                                    | 0.0010   | 3.91  | 0.0191   | 74.51   | 0.0154   | 59.9   | 14.6   |
| 90.0                 | 37.4                                    | 0.0008   | 4.26  | 0.0150   | 81.23   | 0.0158   | 85.5   | 0.0  |
| 120.0                | 30.1                                    | 0.0006   | 4.58  | 0.0121   | 87.39   | 0.0128   | 92.0   | 0.0  |
| 150.0                | 25.5                                    | 0.0005   | 4.84  | 0.0103   | 92.33   | 0.0108   | 97.2   | 0.0  |
| 180.0                | 22.2                                    | 0.0005   | 5.06  | 0.0089   | 96.49   | 0.0094   | 101.5  | 0.0  |
| 210.0                | 19.7                                    | 0.0004   | 5.25  | 0.0079   | 100.10  | 0.0084   | 105.3  | 0.0  |
| 240.0                | 17.8                                    | 0.0004   | 5.42  | 0.0072   | 103.30  | 0.0076   | 108.7  | 0.0  |

**Modified Rational Method - One Hundred Year Storm**  
**Site Flow and Storage Summary**  
 86 Thomas Street, Mississauga  
 File No.: NT-19-013  
 Date: March 2021



**Uncontrolled A2+A3**  
 Drainage Areas  
 Area = **0.0126** ha  
 "C" = **0.63**  
 AC1 = **0.01**  
 Tc = **15.0** min  
 Time Increment = **1.0** min

**Controlled A1**  
 Drainage Areas  
 Area = **0.1517** ha  
 "C" = **1.00**  
 AC2 = **0.15**  
 Tc = **15.0** min  
 Time Increment = **1.0** min

Allowable Rel. Rate = 20.07 L/s  
 Max. Orifice Allowed = 16.98 L/s  
 Actual Orifice Release Rate M = 16.83 L/s  
 Total actual flow = 19.92 L/s  
 Max. Storage Required = 36.2 m<sup>3</sup>

|                           |                        |
|---------------------------|------------------------|
| 100-Year Return Frequency |                        |
| a =                       | 1450.00                |
| c =                       | -0.7800                |
| l =                       | A*(T+4.9) <sup>2</sup> |

| (1)<br>Time<br>(min) | (2)<br>Rainfall<br>Intensity<br>(mm/hr) | (3)<br>Storm<br>Runoff<br>(Uncon. Post)<br>(m <sup>3</sup> /s) | (4)<br>Runoff<br>Volume<br>(Uncon. Post)<br>(m <sup>3</sup> ) | (5)<br>Storm<br>Runoff<br>(Con. Post)<br>(m <sup>3</sup> /s) | (6)<br>Runoff<br>Volume<br>(Con. Post)<br>(m <sup>3</sup> ) | (7)<br>Storm<br>Actual Runoff<br>(m <sup>3</sup> /s) | (8)<br>Total Runoff<br>Volume<br>(m <sup>3</sup> ) | (9)<br>Total<br>Volume Required<br>(m <sup>3</sup> ) |
|----------------------|---|--|---|--|---|--|--|--|
| (1)                  | (2)                                     | (3) = [(2)*AC1] / 360  | (4) = (1)*(3)*60  | (5) = [(2)*AC2] / 360  | (6) = (1)*(5)*60  |  | (8) = (7)*10*60                                    | (9) = (6)-(8)  |
| 15.0                 | 140.7                                   | 0.0031   | 2.79  | 0.0590   | 53.11   | 0.0199   | 17.9   | 35.2   |
| 16.0                 | 135.4                                   | 0.0030   | 2.86  | 0.0568   | 54.53   | 0.0198   | 19.0   | 35.5   |
| 17.0                 | 130.6                                   | 0.0029   | 2.93  | 0.0548   | 55.86   | 0.0197   | 20.1   | 35.8   |
| 18.0                 | 126.1                                   | 0.0028   | 3.00  | 0.0529   | 57.12   | 0.0196   | 21.2   | 35.9   |
| 19.0                 | 122.0                                   | 0.0027   | 3.06  | 0.0512   | 58.32   | 0.0195   | 22.2   | 36.1   |
| 20.0                 | 118.1                                   | 0.0026   | 3.12  | 0.0495   | 59.45   | 0.0194   | 23.3   | 36.1   |
| 21.0                 | 114.5                                   | 0.0025   | 3.17  | 0.0480   | 60.54   | 0.0193   | 24.4   | 36.2   |
| 22.0                 | 111.2                                   | 0.0024   | 3.23  | 0.0466   | 61.58   | 0.0193   | 25.4   | 36.1   |
| 23.0                 | 108.1                                   | 0.0024   | 3.28  | 0.0453   | 62.57   | 0.0192   | 26.5   | 36.1   |
| 24.0                 | 105.2                                   | 0.0023   | 3.33  | 0.0441   | 63.52   | 0.0191   | 27.6   | 36.0   |
| 25.0                 | 102.4                                   | 0.0023   | 3.38  | 0.0430   | 64.43   | 0.0191   | 28.6   | 35.8   |
| 26.0                 | 99.8                                    | 0.0022   | 3.43  | 0.0419   | 65.31   | 0.0190   | 29.7   | 35.6   |
| 27.0                 | 97.4                                    | 0.0021   | 3.47  | 0.0408   | 66.16   | 0.0190   | 30.7   | 35.4   |
| 28.0                 | 95.1                                    | 0.0021   | 3.51  | 0.0399   | 66.98   | 0.0189   | 31.8   | 35.2   |
| 29.0                 | 92.9                                    | 0.0020   | 3.55  | 0.0389   | 67.77   | 0.0189   | 32.8   | 34.9   |
| 30.0                 | 90.8                                    | 0.0020   | 3.59  | 0.0381   | 68.53   | 0.0188   | 33.9   | 34.6   |
| 31.0                 | 88.8                                    | 0.0020   | 3.63  | 0.0372   | 69.28   | 0.0188   | 34.9   | 34.3   |
| 32.0                 | 86.9                                    | 0.0019   | 3.67  | 0.0365   | 69.99   | 0.0187   | 36.0   | 34.0   |
| 33.0                 | 85.1                                    | 0.0019   | 3.71  | 0.0357   | 70.69   | 0.0187   | 37.0   | 33.7   |
| 34.0                 | 83.4                                    | 0.0018   | 3.74  | 0.0350   | 71.37   | 0.0187   | 38.1   | 33.3   |
| 35.0                 | 81.8                                    | 0.0018   | 3.78  | 0.0343   | 72.03   | 0.0186   | 39.1   | 32.9   |
| 36.0                 | 80.2                                    | 0.0018   | 3.81  | 0.0336   | 72.67   | 0.0186   | 40.2   | 32.5   |
| 37.0                 | 78.7                                    | 0.0017   | 3.84  | 0.0330   | 73.29   | 0.0186   | 41.2   | 32.1   |
| 38.0                 | 77.3                                    | 0.0017   | 3.88  | 0.0324   | 73.90   | 0.0185   | 42.2   | 31.7   |
| 39.0                 | 75.9                                    | 0.0017   | 3.91  | 0.0318   | 74.50   | 0.0185   | 43.3   | 31.2   |
| 40.0                 | 74.6                                    | 0.0016   | 3.94  | 0.0313   | 75.08   | 0.0185   | 44.3   | 30.7   |
| 41.0                 | 73.3                                    | 0.0016   | 3.97  | 0.0307   | 75.64   | 0.0184   | 45.4   | 30.3   |
| 42.0                 | 72.1                                    | 0.0016   | 4.00  | 0.0302   | 76.20   | 0.0184   | 46.4   | 29.8   |
| 43.0                 | 70.9                                    | 0.0016   | 4.02  | 0.0297   | 76.74   | 0.0184   | 47.4   | 29.3   |
| 44.0                 | 69.8                                    | 0.0015   | 4.05  | 0.0293   | 77.27   | 0.0184   | 48.5   | 28.8   |
| 45.0                 | 68.7                                    | 0.0015   | 4.08  | 0.0288   | 77.78   | 0.0183   | 49.5   | 28.3   |
| 46.0                 | 67.6                                    | 0.0015   | 4.11  | 0.0284   | 78.29   | 0.0183   | 50.6   | 27.7   |
| 47.0                 | 66.6                                    | 0.0015   | 4.13  | 0.0279   | 78.79   | 0.0183   | 51.6   | 27.2   |
| 48.0                 | 65.6                                    | 0.0014   | 4.16  | 0.0275   | 79.28   | 0.0183   | 52.6   | 26.6   |
| 49.0                 | 64.7                                    | 0.0014   | 4.18  | 0.0271   | 79.75   | 0.0183   | 53.7   | 26.1   |
| 50.0                 | 63.8                                    | 0.0014   | 4.21  | 0.0267   | 80.22   | 0.0182   | 54.7   | 25.5   |
| 51.0                 | 62.9                                    | 0.0014   | 4.23  | 0.0264   | 80.68   | 0.0182   | 55.7   | 25.0   |
| 52.0                 | 62.0                                    | 0.0014   | 4.25  | 0.0260   | 81.14   | 0.0182   | 56.8   | 24.4   |
| 53.0                 | 61.2                                    | 0.0013   | 4.28  | 0.0257   | 81.58   | 0.0182   | 57.8   | 23.8   |
| 54.0                 | 60.4                                    | 0.0013   | 4.30  | 0.0253   | 82.02   | 0.0182   | 58.8   | 23.2   |
| 55.0                 | 59.6                                    | 0.0013   | 4.32  | 0.0250   | 82.44   | 0.0181   | 59.9   | 22.6   |
| 56.0                 | 58.8                                    | 0.0013   | 4.35  | 0.0247   | 82.87   | 0.0181   | 60.9   | 22.0   |
| 57.0                 | 58.1                                    | 0.0013   | 4.37  | 0.0244   | 83.28   | 0.0181   | 61.9   | 21.4   |
| 58.0                 | 57.3                                    | 0.0013   | 4.39  | 0.0240   | 83.69   | 0.0181   | 63.0   | 20.7   |
| 59.0                 | 56.6                                    | 0.0012   | 4.41  | 0.0238   | 84.09   | 0.0181   | 64.0   | 20.1   |
| 60.0                 | 56.0                                    | 0.0012   | 4.43  | 0.0235   | 84.49   | 0.0181   | 65.0   | 19.5   |
| 61.0                 | 55.3                                    | 0.0012   | 4.45  | 0.0232   | 84.88   | 0.0180   | 66.0   | 18.8   |
| 62.0                 | 54.6                                    | 0.0012   | 4.47  | 0.0229   | 85.26   | 0.0180   | 67.1   | 18.2   |
| 63.0                 | 54.0                                    | 0.0012   | 4.49  | 0.0227   | 85.64   | 0.0180   | 68.1   | 17.5   |
| 64.0                 | 53.4                                    | 0.0012   | 4.51  | 0.0224   | 86.01   | 0.0180   | 69.1   | 16.9   |
| 65.0                 | 52.8                                    | 0.0012   | 4.53  | 0.0221   | 86.38   | 0.0180   | 70.2   | 16.2   |
| 90.0                 | 41.6                                    | 0.0009   | 4.94  | 0.0174   | 94.23   | 0.0184   | 99.2   | 0.0  |
| 120.0                | 33.6                                    | 0.0007   | 5.32  | 0.0141   | 101.40  | 0.0148   | 106.7  | 0.0  |
| 150.0                | 28.4                                    | 0.0006   | 5.62  | 0.0119   | 107.16  | 0.0125   | 112.8  | 0.0  |
| 180.0                | 24.7                                    | 0.0005   | 5.87  | 0.0104   | 112.01  | 0.0109   | 117.9  | 0.0  |
| 210.0                | 22.0                                    | 0.0005   | 6.09  | 0.0092   | 116.22  | 0.0097   | 122.3  | 0.0  |
| 240.0                | 19.9                                    | 0.0004   | 6.29  | 0.0083   | 119.95  | 0.0088   | 126.2  | 0.0  |



**Area Drain Orifice Calculation  
Stormwater Storage**

86 Thomas Street, Mississauga  
File No.: NT-19-013  
Date: March 2021

**Orifice Equation**

Orifice Tube = 0.82  
Orifice Tube Elevation = 153.41

| Storm Event | Orifice Coefficient | Head at Centroid (m) | Head Surface Ponding (m) | Total Head (m) | Diameter of Orifice (mm) | Maximum Area of Orifice (m <sup>2</sup> ) | Release Rate (L/s) |
|-------------|---------------------|----------------------|--------------------------|----------------|--------------------------|---|--------------------|
| 2 year      | 0.82                | 0.12                 | 0.00                     | 0.12           | 75.0                     | 0.004                                     | 5.56               |
| 5 year      | 0.82                | 0.23                 | 0.00                     | 0.23           | 75.0                     | 0.004                                     | 7.70               |
| 10 year     | 0.82                | 0.35                 | 0.00                     | 0.35           | 75.0                     | 0.004                                     | 9.49               |
| 25 year     | 0.82                | 0.55                 | 0.00                     | 0.55           | 75.0                     | 0.004                                     | 11.90              |
| 50 year     | 0.82                | 0.80                 | 0.00                     | 0.80           | 75.0                     | 0.004                                     | 14.35              |
| 100 year    | 0.82                | 1.10                 | 0.00                     | 1.10           | 75.0                     | 0.004                                     | 16.83              |





**Provided Storage**

86 Thomas St.  
 File No. NT-19-013  
 Date: July 2021

| 100 year       |        |                    |             |        |                |                        |      |
|----------------|--------|--------------------|-------------|--------|----------------|------------------------|------|
| Orifice Invert | 153.41 | Head from Centroid |             | 1.10   |                | Required               | 36.2 |
|                |        | Invert             | Depth       | Volume | Total Provided | 44.56                  |      |
| Dia            | Length | Volume             |             |        |                | Underground Pipe + MHs | 4.56 |
| 0.3            | 62.7   | 2.21               | STM MH 101  | 154.5  | 0.147          | Tank Provided          | 40   |
| 0.25           | 23.5   | 0.58               | STM MH 102  | 154.3  | 0.347          |                        |      |
|                |        |                    | STM CBMH101 | 153.61 | 1.037          |                        |      |
|                |        |                    | CB 101      | 154.56 | 0.087          |                        |      |
|                |        |                    | DCB 101     | 153.86 | 0.787          |                        |      |
|                |        |                    | DCB 102     | 153.52 | 1.127          |                        |      |

## LID - INFILTRATION FACILITY CALCULATION

|                             |                            |                    |
|-----------------------------|----------------------------|--------------------|
| <b>86 Thomas Street</b>     | $D = \frac{PT}{1000}$      |                    |
| Mississauga, ON             |                            |                    |
| August 9, 2021              |                            |                    |
| File # NT-19-013            |                            |                    |
| <b>Nextrans Engineering</b> |                            |                    |
| Prepared by: W.L.           | <b>Type of Development</b> | <b>Residential</b> |
| Checked by: G.R.            |                            |                    |

### Unit Quantity Determination

|                              |       |                |
|------------------------------|-------|----------------|
| 1. Volume within GreenStorm  | 8.2   | m <sup>3</sup> |
| 2. Percolation Rate *        | 7.5   | mm/hr          |
| 3. Depth of Infiltration Bed | 320.0 | mm             |

### Infiltration Facility Determination

|                       |      |     |
|-----------------------|------|-----|
| 1. Time to Infiltrate | 42.7 | hrs |
|-----------------------|------|-----|

\* Percolation Rate from test on 80 Thomas St provided by Soils Engineers Ltd.

## Stormceptor® EF Sizing Report

### ESTIMATED NET ANNUAL SEDIMENT (TSS) LOAD REDUCTION STORMCEPTOR®

Date: 8/26/2019

*Green cells require user input*  
*Grey cells indicate optional user input*  
*Blue cells indicate sizing results*

|                             |       |
|-----------------------------|-------|
| Drainage Area (ha):         | 0.164 |
| % Imperviousness:           | 84    |
| Runoff Coefficient 'c': 0.8 |       |
| Particle Size Distribution: | FINE  |
| Target TSS Removal (%):     | 80    |

|                             |   |                         |  |
|-----------------------------|---|-------------------------|--|
| Project Name: 80 Thomas St. |   | Project Number:         |  |
| User Contact Information    |   | EOR Contact Information |  |
| Name:                       | Brandon O'Leary   | Name:                   | Wendy Li, P.Eng  |
| Company:                    | Forterra  | Company:                | NexTrans Consulting Engineers                              |
| Email / Phone:              | <a href="mailto:Brandon.Oleary@forterra.com">Brandon.Oleary@forterra.com</a> / 905-630-0359 | Email / Phone:          | <a href="mailto:wendyl@nextrans.ca">wendyl@nextrans.ca</a> |

|                           |                 |
|---------------------------|-----------------|
| Province:                 | Ontario         |
| City:                     | Mississauga     |
| Nearest Rainfall Station: | TORONTO CENTRAL |
| NCDC Rainfall Station ID: | ON100           |
| Years of Rainfall Data:   | 18              |

|   |     |
|---|-----|
| Require Hydrocarbon Spill Capture?                | Yes |
| Upstream Flow Control?                            | No  |
| Required Water Quality Runoff Volume Capture (%): | 90  |
| Estimated Water Quality Flow Rate (L/s):          | 2.1 |
| Peak Conveyance (maximum) Flow Rate (L/s):        |     |
| Site Sediment Transport Rate (kg/ha/yr):          |     |

| Net Annual Sediment (TSS) Load Reduction Sizing Summary |                          |
|---|--------------------------|
| Stormceptor Model                                       | TSS Removal Provided (%) |
| EFO4  | 91                       |
| EFO6  | 92                       |
| EFO8  | 93                       |
| EFO10   | 93                       |
| EFO12   | 93                       |

**Recommended Stormceptor EFO Model: EFO4**  
**Estimated Net Annual Sediment (TSS) Load Reduction (%): 91**  
**Water Quality Runoff Volume Capture (%): > 90**

### THIRD-PARTY TESTING AND VERIFICATION

► Stormceptor® EF and Stormceptor® EFO are the latest evolutions in the Stormceptor® oil-grit separator (OGS) technology series, and are designed to remove a wide variety of pollutants from stormwater and snowmelt runoff. These technologies have been third-party tested in accordance with the Canadian ETV Procedure for Laboratory Testing of Oil-Grit Separators and performance has been third-party verified in accordance with the ISO 14034 Environmental Technology Verification (ETV) protocol.

### PERFORMANCE

► Stormceptor® EF and EFO remove stormwater pollutants through gravity separation and floatation, and feature a patent-pending design that generates positive removal of total suspended solids (TSS) throughout each storm event, including high-intensity storms. Captured pollutants include sediment, free oils, and sediment-bound pollutants such as nutrients, heavy metals, and petroleum hydrocarbons. Stormceptor is sized to remove a high level of TSS from the frequent rainfall events that contribute the vast majority of annual runoff volume and pollutant load. The technology incorporates an internal bypass to convey excessive stormwater flows from high-intensity storms through the device without resuspension and washout (scour) of previously captured pollutants. Proper routine maintenance ensures high pollutant removal performance and protection of downstream waterways.

### PARTICLE SIZE DISTRIBUTION (PSD)

► The Canadian ETV PSD shown in the table below, or particle fractions within this PSD, were used for this sizing. This is the identical PSD that is referenced in the Canadian ETV Procedure for Laboratory Testing of Oil-Grit Separators for both sediment removal testing and scour testing. The Canadian ETV PSD contains a wide range of particle sizes in the sand and silt fractions, and is considered reasonably representative of the particle size fractions found in typical urban stormwater runoff.

| Particle Size (µm) | Percent Less Than | Particle Size Fraction (µm) | Percent |
|--------------------|-------------------|-----------------------------|---------|
| 1000               | 100               | 500-1000                    | 5       |
| 500                | 95                | 250-500                     | 5       |
| 250                | 90                | 150-250                     | 15      |
| 150                | 75                | 100-150                     | 15      |
| 100                | 60                | 75-100                      | 10      |
| 75                 | 50                | 50-75                       | 5       |
| 50                 | 45                | 20-50                       | 10      |
| 20                 | 35                | 8-20                        | 15      |
| 8                  | 20                | 5-8                         | 10      |
| 5                  | 10                | 2-5                         | 5       |
| 2                  | 5                 | <2                          | 5       |



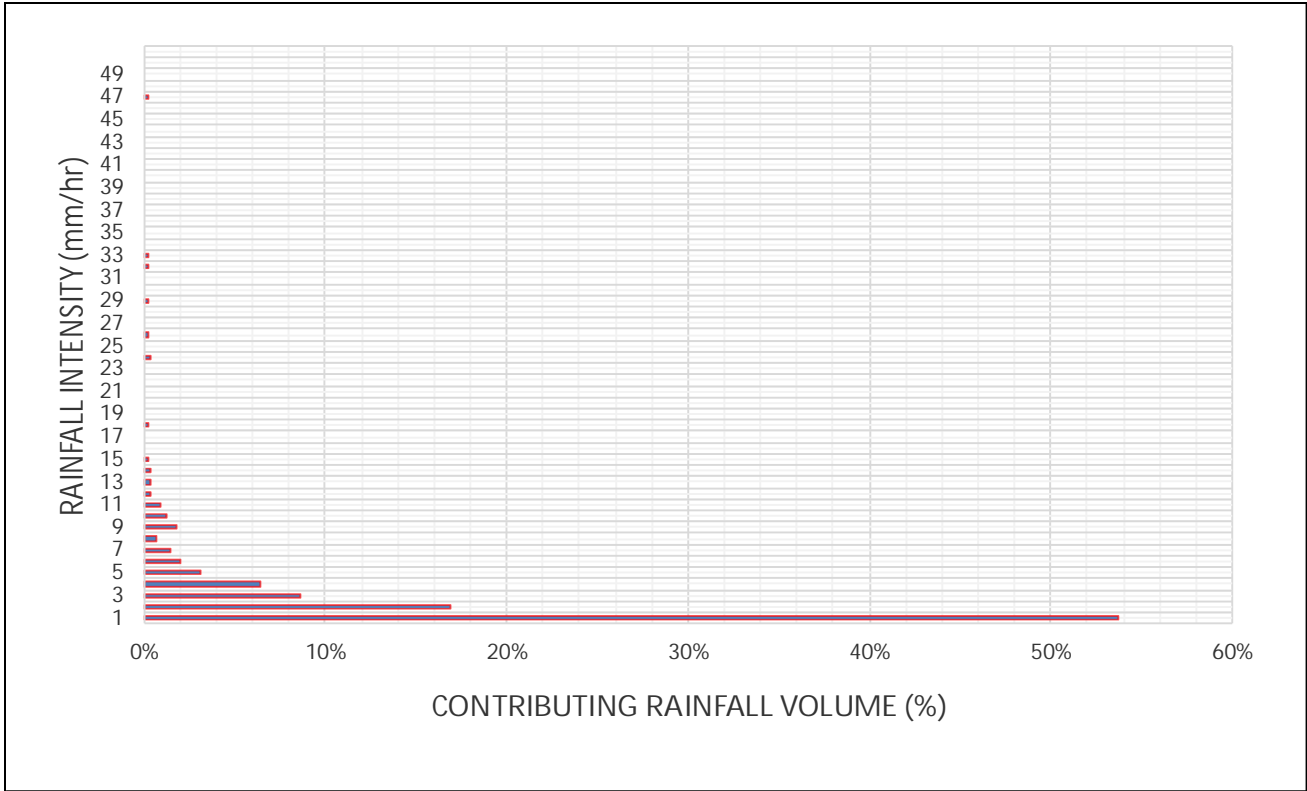
**Stormceptor®EF Sizing Report**

| <u>Rainfall Intensity (mm/hr)</u> | <u>Percent Rainfall Volume</u> | <u>Cumulative Rainfall Volume</u> | <u>Flow Rate (L/s)</u> | <u>Flow Rate (L/min)</u> | <u>Surface Loading Rate (L/min/m<sup>2</sup>)</u> | <u>Removal Efficiency (%)</u> | <u>Incremental Removal (%)</u> | <u>Cumulative Removal (%)</u> |
|-----------------------------------|--------------------------------|-----------------------------------|------------------------|--------------------------|---|-------------------------------|--------------------------------|-------------------------------|
| 1.0                               | 53.7%                          | 53.7%                             | 0.37                   | 22.0                     | 18.3  | 93                            | 49.9                           | 49.9                          |
| 2.0                               | 16.9%                          | 70.6%                             | 0.73                   | 44.0                     | 36.7  | 93                            | 15.7                           | 65.7                          |
| 3.0                               | 8.6%                           | 79.2%                             | 1.10                   | 66.0                     | 55.0  | 92                            | 7.9                            | 73.6                          |
| 4.0                               | 6.4%                           | 85.6%                             | 1.47                   | 88.0                     | 73.3  | 90                            | 5.8                            | 79.3                          |
| 5.0                               | 3.1%                           | 88.7%                             | 1.83                   | 110.0                    | 91.6  | 88                            | 2.7                            | 82.1                          |
| 6.0                               | 2.0%                           | 90.7%                             | 2.20                   | 132.0                    | 110.0   | 86                            | 1.7                            | 83.8                          |
| 7.0                               | 1.5%                           | 92.2%                             | 2.57                   | 154.0                    | 128.3   | 85                            | 1.3                            | 85.0                          |
| 8.0                               | 0.7%                           | 92.9%                             | 2.93                   | 175.9                    | 146.6   | 83                            | 0.6                            | 85.6                          |
| 9.0                               | 1.8%                           | 94.7%                             | 3.30                   | 197.9                    | 165.0   | 80                            | 1.4                            | 87.1                          |
| 10.0                              | 1.3%                           | 96.0%                             | 3.67                   | 219.9                    | 183.3   | 78                            | 1.0                            | 88.1                          |
| 11.0                              | 0.9%                           | 96.9%                             | 4.03                   | 241.9                    | 201.6   | 76                            | 0.7                            | 88.8                          |
| 12.0                              | 0.4%                           | 97.3%                             | 4.40                   | 263.9                    | 219.9   | 74                            | 0.3                            | 89.1                          |
| 13.0                              | 0.4%                           | 97.7%                             | 4.77                   | 285.9                    | 238.3   | 73                            | 0.3                            | 89.4                          |
| 14.0                              | 0.4%                           | 98.1%                             | 5.13                   | 307.9                    | 256.6   | 72                            | 0.3                            | 89.6                          |
| 15.0                              | 0.2%                           | 98.3%                             | 5.50                   | 329.9                    | 274.9   | 70                            | 0.1                            | 89.8                          |
| 16.0                              | 0.0%                           | 98.3%                             | 5.86                   | 351.9                    | 293.2   | 68                            | 0.0                            | 89.8                          |
| 17.0                              | 0.0%                           | 98.3%                             | 6.23                   | 373.9                    | 311.6   | 66                            | 0.0                            | 89.8                          |
| 18.0                              | 0.2%                           | 98.5%                             | 6.60                   | 395.9                    | 329.9   | 64                            | 0.1                            | 89.9                          |
| 19.0                              | 0.0%                           | 98.5%                             | 6.96                   | 417.9                    | 348.2   | 63                            | 0.0                            | 89.9                          |
| 20.0                              | 0.0%                           | 98.5%                             | 7.33                   | 439.9                    | 366.6   | 62                            | 0.0                            | 89.9                          |
| 21.0                              | 0.0%                           | 98.5%                             | 7.70                   | 461.9                    | 384.9   | 60                            | 0.0                            | 89.9                          |
| 22.0                              | 0.0%                           | 98.5%                             | 8.06                   | 483.9                    | 403.2   | 58                            | 0.0                            | 89.9                          |
| 23.0                              | 0.0%                           | 98.5%                             | 8.43                   | 505.9                    | 421.5   | 57                            | 0.0                            | 89.9                          |
| 24.0                              | 0.4%                           | 98.9%                             | 8.80                   | 527.8                    | 439.9   | 57                            | 0.2                            | 90.1                          |
| 25.0                              | 0.0%                           | 98.9%                             | 9.16                   | 549.8                    | 458.2   | 57                            | 0.0                            | 90.1                          |
| 26.0                              | 0.2%                           | 99.1%                             | 9.53                   | 571.8                    | 476.5   | 56                            | 0.1                            | 90.2                          |
| 27.0                              | 0.0%                           | 99.1%                             | 9.90                   | 593.8                    | 494.9   | 55                            | 0.0                            | 90.2                          |
| 28.0                              | 0.0%                           | 99.1%                             | 10.26                  | 615.8                    | 513.2   | 55                            | 0.0                            | 90.2                          |
| 29.0                              | 0.2%                           | 99.3%                             | 10.63                  | 637.8                    | 531.5   | 54                            | 0.1                            | 90.4                          |
| 30.0                              | 0.0%                           | 99.3%                             | 11.00                  | 659.8                    | 549.8   | 54                            | 0.0                            | 90.4                          |
| 31.0                              | 0.0%                           | 99.3%                             | 11.36                  | 681.8                    | 568.2   | 53                            | 0.0                            | 90.4                          |
| 32.0                              | 0.2%                           | 99.5%                             | 11.73                  | 703.8                    | 586.5   | 53                            | 0.1                            | 90.5                          |
| 33.0                              | 0.2%                           | 99.7%                             | 12.10                  | 725.8                    | 604.8   | 52                            | 0.1                            | 90.6                          |
| 34.0                              | 0.0%                           | 99.7%                             | 12.46                  | 747.8                    | 623.2   | 52                            | 0.0                            | 90.6                          |
| 35.0                              | 0.0%                           | 99.7%                             | 12.83                  | 769.8                    | 641.5   | 52                            | 0.0                            | 90.6                          |
| 36.0                              | 0.0%                           | 99.7%                             | 13.20                  | 791.8                    | 659.8   | 52                            | 0.0                            | 90.6                          |
| 37.0                              | 0.0%                           | 99.7%                             | 13.56                  | 813.8                    | 678.1   | 52                            | 0.0                            | 90.6                          |
| 38.0                              | 0.0%                           | 99.7%                             | 13.93                  | 835.8                    | 696.5   | 52                            | 0.0                            | 90.6                          |
| 39.0                              | 0.0%                           | 99.7%                             | 14.30                  | 857.7                    | 714.8   | 51                            | 0.0                            | 90.6                          |
| 40.0                              | 0.0%                           | 99.7%                             | 14.66                  | 879.7                    | 733.1   | 51                            | 0.0                            | 90.6                          |
| 41.0                              | 0.0%                           | 99.7%                             | 15.03                  | 901.7                    | 751.4   | 51                            | 0.0                            | 90.6                          |
| 42.0                              | 0.0%                           | 99.7%                             | 15.40                  | 923.7                    | 769.8   | 51                            | 0.0                            | 90.6                          |
| 43.0                              | 0.0%                           | 99.7%                             | 15.76                  | 945.7                    | 788.1   | 51                            | 0.0                            | 90.6                          |
| 44.0                              | 0.0%                           | 99.7%                             | 16.13                  | 967.7                    | 806.4   | 51                            | 0.0                            | 90.6                          |
| 45.0                              | 0.0%                           | 99.7%                             | 16.50                  | 989.7                    | 824.8   | 51                            | 0.0                            | 90.6                          |
| 46.0                              | 0.0%                           | 99.7%                             | 16.86                  | 1011.7                   | 843.1   | 51                            | 0.0                            | 90.6                          |
| 47.0                              | 0.2%                           | 99.9%                             | 17.23                  | 1033.7                   | 861.4   | 51                            | 0.1                            | 90.7                          |
| 48.0                              | 0.0%                           | 99.9%                             | 17.59                  | 1055.7                   | 879.7   | 51                            | 0.0                            | 90.7                          |
| 49.0                              | 0.0%                           | 99.9%                             | 17.96                  | 1077.7                   | 898.1   | 51                            | 0.0                            | 90.7                          |
| 50.0                              | 0.0%                           | 99.9%                             | 18.33                  | 1099.7                   | 916.4   | 50                            | 0.0                            | 90.7                          |

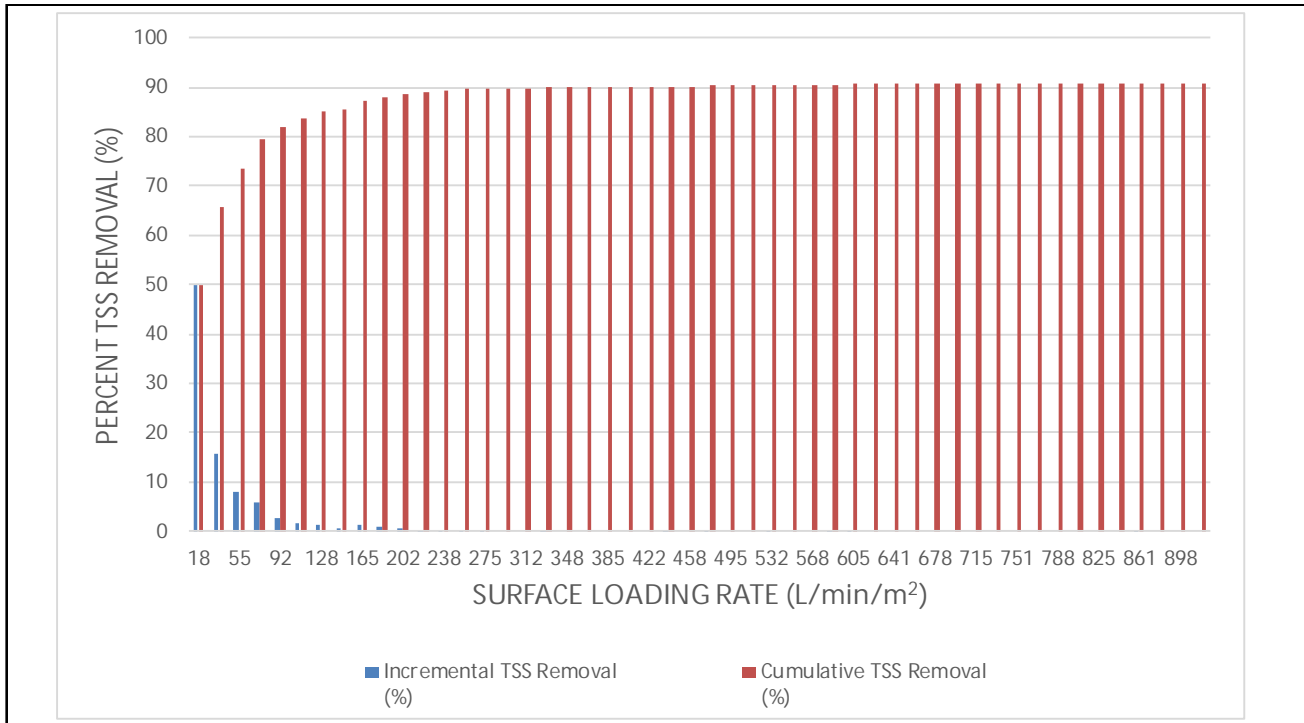
**Estimated Net Annual Sediment (TSS) Load Reduction = 91%**

## Stormceptor®EF Sizing Report

### RAINFALL DATA FROM THE TORONTO CENTRAL RAINFALL STATION



### INCREMENTAL AND CUMULATIVE TSS REMOVAL FOR THE RECOMMENDED STORMCEPTOR® MODEL



## Stormceptor® EF Sizing Report

**Table 1.1**  
Maximum Pipe Diameter / Peak Conveyance

| Stormceptor EF / EFO | Model Diameter |      | Minimum Angle Inlet / Outlet Pipes | Maximum Inlet Pipe Diameter |      | Maximum Outlet Pipe Diameter |      | Peak Conveyance Flow Rate |       |
|----------------------|----------------|------|------------------------------------|-----------------------------|------|------------------------------|------|---------------------------|-------|
|                      | (m)            | (ft) |                                    | (mm)                        | (in) | (mm)                         | (in) | (L/s)                     | (cfs) |
| EF4 / EFO4           | 1.2            | 4    | 90°                                | 609                         | 24   | 609                          | 24   | 425                       | 15    |
| EF6 / EFO6           | 1.8            | 6    | 90°                                | 914                         | 36   | 914                          | 36   | 990                       | 35    |
| EF8 / EFO8           | 2.4            | 8    | 90°                                | 1,219                       | 48   | 1,219                        | 48   | 1,700                     | 60    |
| EF10 / EFO10         | 3.0            | 10   | 90°                                | 1,828                       | 72   | 1,828                        | 72   | 2,830                     | 100   |
| EF12 / EFO12         | 3.6            | 12   | 90°                                | 1,828                       | 72   | 1,828                        | 72   | 2,830                     | 100   |

### SCOUR PREVENTION AND ONLINE CONFIGURATION

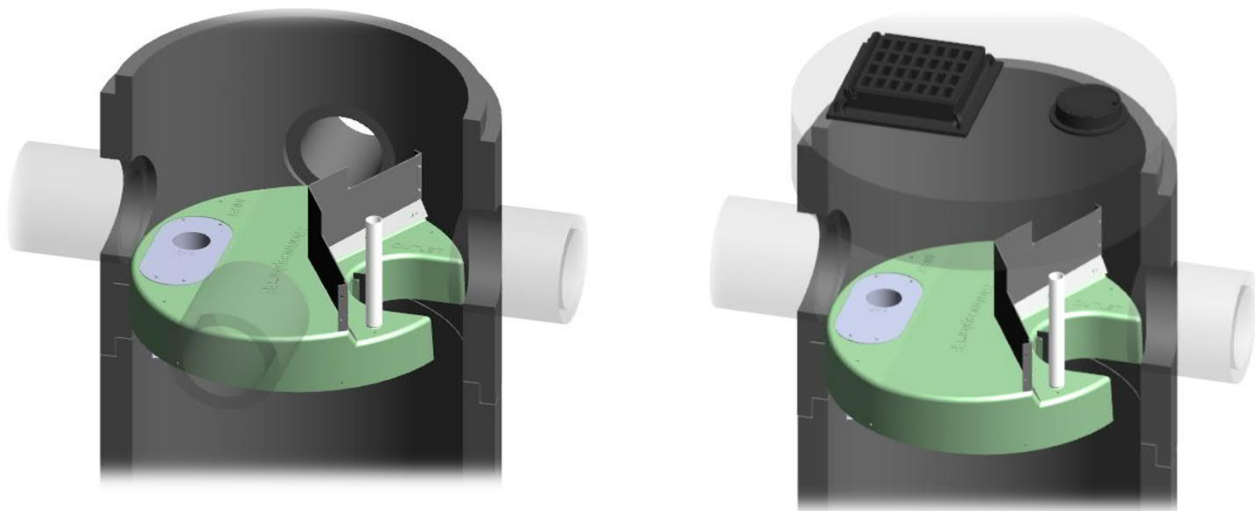
► Stormceptor® EF and EFO feature an internal bypass and superior scour prevention technology that have been demonstrated in third-party testing according to the scour testing provisions of the Canadian ETV Procedure for Laboratory Testing of Oil-Grit Separators, and the exceptional scour test performance has been third-party verified in accordance with the ISO 14034 ETV protocol. As a result, Stormceptor EF and EFO are approved for online installation, eliminating the need for costly additional bypass structures, piping, and installation expense.

### DESIGN FLEXIBILITY

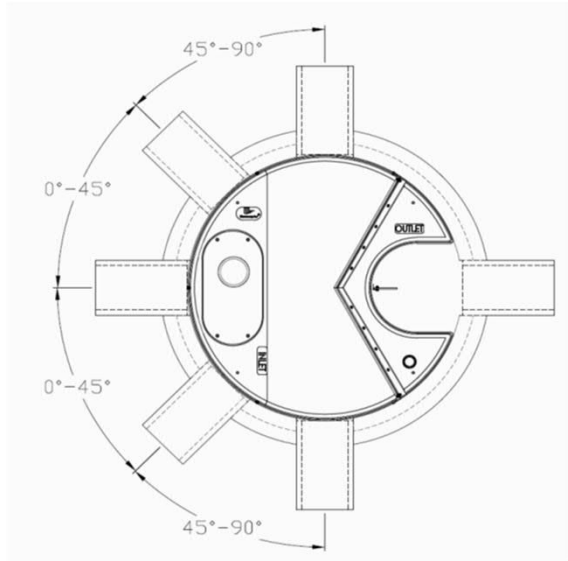
► Stormceptor® EF and EFO offers design flexibility in one simplified platform, accepting stormwater flow from a single inlet pipe or multiple inlet pipes, and/or surface runoff through an inlet grate. The device can also serve as a junction structure, accommodate a 90-degree inlet-to-outlet bend angle, and can be modified to ensure performance in submerged conditions.

### OIL CAPTURE AND RETENTION

► While Stormceptor® EF will capture and retain oil from dry weather spills and low intensity runoff, Stormceptor® EFO has demonstrated superior oil capture and greater than 99% oil retention in third-party testing according to the light liquid re-entrainment testing provisions of the Canadian ETV Procedure for Laboratory Testing of Oil-Grit Separators. Stormceptor EFO is recommended for sites where oil capture and retention is a requirement.



## Stormceptor®EF Sizing Report



**INLET-TO-OUTLET DROP** – Elevation differential between inlet and outlet pipe inverts is dictated by the angle at which the inlet pipe(s) enters the unit.  
 0° – 45°: The inlet pipe is 1-inch (25mm) higher than the outlet pipe.  
 45° – 90°: The inlet pipe is 2-inches (50mm) higher than the outlet pipe.

### HEAD LOSS

The head loss through Stormceptor EF is similar to that of a 60-degree bend structure. The applicable K value for calculating minor losses through the unit is 1.1. For submerged conditions the applicable K value is 3.0.

**Table 1.2**  
Pollutant Capacity

| Stormceptor EF / EFO | Model Diameter |      | Depth (Outlet Pipe Invert to Sump Floor) |      | Oil Volume |       | Recommended Sediment Maintenance Depth * |      | Maximum Sediment Volume * |       | Maximum Sediment Mass ** |         |
|----------------------|----------------|------|--|------|------------|-------|--|------|---------------------------|-------|--------------------------|---------|
|                      | (m)            | (ft) | (m)                                      | (ft) | (L)        | (Gal) | (mm)                                     | (in) | (L)                       | (ft³) | (kg)                     | (lb)    |
| EF4 / EFO4           | 1.2            | 4    | 1.52                                     | 5.0  | 197        | 52    | 203                                      | 8    | 1,190                     | 42    | 1,904                    | 5,250   |
| EF6 / EFO6           | 1.8            | 6    | 1.93                                     | 6.3  | 348        | 92    | 305                                      | 12   | 3,470                     | 123   | 5,552                    | 15,375  |
| EF8 / EFO8           | 2.4            | 8    | 2.59                                     | 8.5  | 545        | 144   | 610                                      | 24   | 8,780                     | 310   | 14,048                   | 38,750  |
| EF10 / EFO10         | 3.0            | 10   | 3.25                                     | 10.7 | 874        | 231   | 610                                      | 24   | 17,790                    | 628   | 28,464                   | 78,500  |
| EF12 / EFO12         | 3.6            | 12   | 3.89                                     | 12.8 | 1,219      | 322   | 610                                      | 24   | 31,220                    | 1,103 | 49,952                   | 137,875 |

\* Increased sump depth may be added to increase sediment storage capacity

\*\* Average density of wet packed sediment in sump = 1.6 kg/L (100 lb/ft³)

| Feature   | Benefit   | Feature Appeals To                                  |
|---|---|---|
| Patent-pending enhanced flow treatment and scour prevention technology  | Superior, verified third-party performance        | Regulator, Specifying & Design Engineer             |
| Third-party verified light liquid capture and retention for EFO version | Proven performance for fuel/oil hotspot locations | Regulator, Specifying & Design Engineer, Site Owner |
| Functions as bend, junction or inlet structure                          | Design flexibility                                | Specifying & Design Engineer                        |
| Minimal drop between inlet and outlet                                   | Site installation ease                            | Contractor  |
| Large diameter outlet riser for inspection and maintenance              | Easy maintenance access from grade                | Maintenance Contractor & Site Owner                 |

### STANDARD STORMCEPTOR EF/EFO DRAWINGS

For standard details, please visit <http://www.imbriumsystems.com/stormwater-treatment-solutions/stormceptor-ef>

### STANDARD STORMCEPTOR EF/EFO SPECIFICATION

For specifications, please visit <http://www.imbriumsystems.com/stormwater-treatment-solutions/stormceptor-ef>



**Stormceptor® EF Sizing Report**



# 86 THOMAS STREET, MISSISSAUGA

## DRAWING INDEX

| TITLE                    | SHEET NO |
|--------------------------|----------|
| COVER SHEET              | 1 OF 5   |
| SYSTEM LAYOUT SHEET      | 2 OF 5   |
| SYSTEM CALCULATION SHEET | 3 OF 5   |
| SYSTEM OVERLAY SHEET     | 4 OF 5   |
| DETAIL SHEET             | 5 OF 5   |

| PROJECT INFORMATION             |                 |              |                       |    |
|---------------------------------|-----------------|--------------|-----------------------|----|
| SITE CONTACT                    | PHIL ALLEN      | 416-286-5990 | PHILALLEN@STORMCON.CA |    |
| ENGINEER / TECHNICAL SPECIALIST | PARTH PUSHKARNA | 647-278-7339 | PARTHP@STORMCON.CA    |    |
| SALES REP:                      | GREG DZIEWIECKI | 437-231-6080 | GREGD@STORMCON.CA     |    |
|                                 | PARTH PUSHKARNA | 647-278-7339 | PARTHP@STORMCON.CA    |    |
| PROJECT NO:                     | 21-114.00       |              |                       |    |
| COMMENTS:                       | REVISION        | DATE         | COMMENT               | BY |
|                                 |                 |              |                       |    |
|                                 |                 |              |                       |    |
|                                 |                 |              |                       |    |
|                                 |                 |              |                       |    |

### GENERAL NOTES

- COORDINATE WITH MANUFACTURER'S REPRESENTATIVE/DISTRIBUTOR FOR PRE-CONSTRUCTION MEETING AND SITE INSPECTION DURING INSTALLATION.
- ENGINEERING DRAWINGS SUPERSEDE ALL PROVIDED DOCUMENTATION. REFER TO SITE ENGINEERS FOR ADDITIONAL INSTRUCTIONS.
- COORDINATE GREENSTORM INSTALLATION ACTIVITIES WITH OTHER SITE ACTIVITIES
- ALL DIMENSIONS ARE IN METERS UNLESS NOTED OTHERWISE
- THE SUB-GRADE AND SIDE BACKFILL TO BE COMPACTED TO 95% SPD OR AS DIRECTED BY THE QUALIFIED ENGINEER.
- CONFIRM GEOTECHNICAL SOIL EVALUATION BY A QUALIFIED ENGINEER TO DETERMINE SUITABILITY OF STRUCTURAL INSTALLATION
- CONFIRM FOR BURIED UNDERGROUND UTILITIES INCLUDING GAS, ELECTRICAL, PIPELINES OR CONDUITS
- WHEN INSTALLED IN CONFORMANCE TO THE INSTALLATION GUIDELINES, GREENSTORM-ST CAN HANDLE STANDARD CL-625 TRUCK LOADING. FOR NON-STANDARD LOADS CONTACT MANUFACTURER'S REPRESENTATIVE/DISTRIBUTOR
- PROTECT THE INSTALLATION AGAINST DAMAGE WITH CONSTRUCTION TAPE, FENCING OR OTHER MEANS TILL THE CONSTRUCTION IS COMPLETE.
- ENSURE THAT CONSTRUCTION FOLLOWS APPLICABLE FEDERAL, PROVINCIAL, LOCAL, MUNICIPAL AND LOCAL LAWS, ORDNANCES, REGULATIONS AND SAFETY REQUIREMENTS.
- VEHICULAR LOADING IS PROHIBITED UNTIL BACKFILLED AS PER MANUFACTURER'S INSTALLATION GUIDELINES. THE USE OF EQUIPMENT OVER GREENSTORM CHAMBERS IS LIMITED:
  - NO EQUIPMENT IS ALLOWED ON BARE CHAMBERS.
  - NO RUBBER TIRED LOADER, DUMP TRUCK, OR EXCAVATORS ARE ALLOWED UNTIL PROPER FILL DEPTHS ARE REACHED IN ACCORDANCE WITH THE CONSTRUCTION GUIDE.
  - WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT CAN BE FOUND IN THE CONSTRUCTION GUIDE.
  - FULL 900 mm (36") OF STABILIZED COVER MATERIALS OVER THE CHAMBERS IS REQUIRED FOR DUMP TRUCK TRAVEL OR DUMPING.

### CHECK - REQUIRED MATERIALS AND EQUIPMENT

- ALL GREENSTORM CHAMBERS AND ACCESSORIES AS SPECIFIED IN THE ENGINEER'S PLANS INCLUDING NON-WOVEN GEOTEXTILE, CONNECTORS, QUADS, SIDEWALLSADAPTER, RISER AND LINER WHERE APPLICABLE.
- RECIPROCATING SAW OR ROUTER
- TRANSIT OR LASER LEVEL MEASURING DEVICE
- COMPACTION EQUIPMENT WITH MAXIMUM GROSS VEHICLE WEIGHT OF 12,000 LBS (5,440 KGS).
- ACCEPTABLE FILL MATERIAL AS SHOWN IN INSTALLATION INSTRUCTIONS.
- QUANTITIES FOR GEOSYNTHETIC ARE APPROXIMATE AND MAY VARY BASED ON OVERLAP, WASTAGE.
- CHECK GREENSTORM CHAMBERS FOR DAMAGE PRIOR TO INSTALLATION. DO NOT USE DAMAGED CHAMBERS, CONTACT YOUR SUPPLIER IMMEDIATELY TO REPORT DAMAGE OR PACKING-LIST DISCREPANCIES.**

### NOTES FOR BIDDING AND INSTALLATIONS

- CONTRACTORS ARE EXPECTED TO COMPREHEND AND USE THE MOST CURRENT INSTALLATION INSTRUCTIONS PRIOR TO BEGINNING A SYSTEM INSTALLATION. FOR THE MOST CURRENT INSTRUCTIONS, CONTACT STORMCON AT (647) 463-9803 OR VISIT WWW.STORMCON.CA.
- CONTACT STORMCON AT LEAST TWO WEEKS PRIOR TO SYSTEM INSTALLATION TO ARRANGE FOR A PRE-CONSTRUCTION MEETING.
- USE GREENSTORM INSTALLATION INSTRUCTIONS AS A GUIDELINE ONLY FOR MINIMUM/MAXIMUM REQUIREMENTS. ACTUAL DESIGN MAY VARY. REFER TO APPROVED CONSTRUCTION DRAWINGS FOR JOB-SPECIFIC DETAILS. ENGINEERING DRAWINGS SUPERSEDE ALL PROVIDED DOCUMENTATION.
- THE FOUNDATION STONE SHALL BE LEVEL AND COMPACTED PRIOR TO CHAMBER INSTALLATION.
- ANY DISCREPANCIES WITH THE SYSTEM SUB-GRADE SOIL'S BEARING CAPACITY MUST BE REPORTED TO THE GEOTECHNICAL ENGINEER.
- CONTRACTOR TO REFER TO GREENSTORM INSTALLATION INSTRUCTIONS CONCERNING VEHICULAR TRAFFIC. RESPONSIBILITY FOR PREVENTING VEHICLES THAT EXCEED REQUIREMENTS SPECIFIED FROM TRAVELING ACROSS OR PARKING OVER THE CHAMBER SYSTEM LIES SOLELY WITH THE CONTRACTOR THROUGHOUT THE ENTIRE SITE CONSTRUCTION PROCESS. THE PLACEMENT OF WARNING TAPE, TEMPORARY FENCING, AND/OR APPROPRIATELY LOCATED SIGNS IS HIGHLY RECOMMENDED.
- TRAFFIC OF INSTALLATION EQUIPMENT OR OTHER VEHICULAR TRAFFIC OVER TOP OF THE GREENSTORM STORMWATER SYSTEM IS STRICTLY RESTRICTED AND PROHIBITED UNTIL SATISFACTORY COVER AND COMPACTION IS ACHIEVED ACCORDING TO MANUFACTURER'S INSTALLATION INSTRUCTIONS.
- EROSION AND SEDIMENT-CONTROL MEASURES MUST MEET LOCAL CODES AND THE DESIGN ENGINEER'S SPECIFICATIONS THROUGHOUT THE ENTIRE SITE CONSTRUCTION PROCESS.
- GREENSTORM SYSTEMS MUST BE DESIGNED AND INSTALLED IN ACCORDANCE WITH STORMCON'S MINIMUM REQUIREMENTS. FAILURE TO DO SO WILL VOID THE LIMITED WARRANTY.

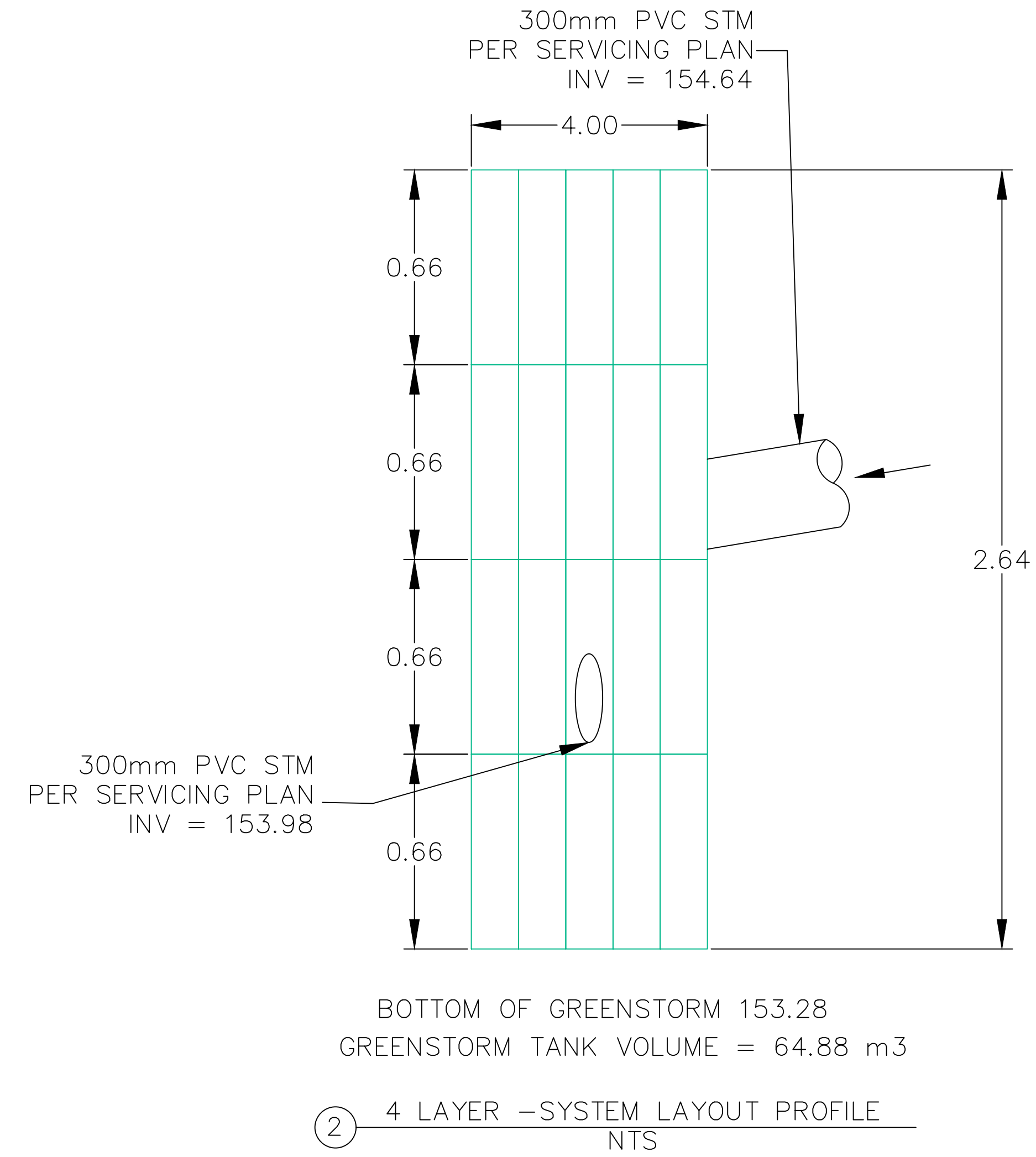
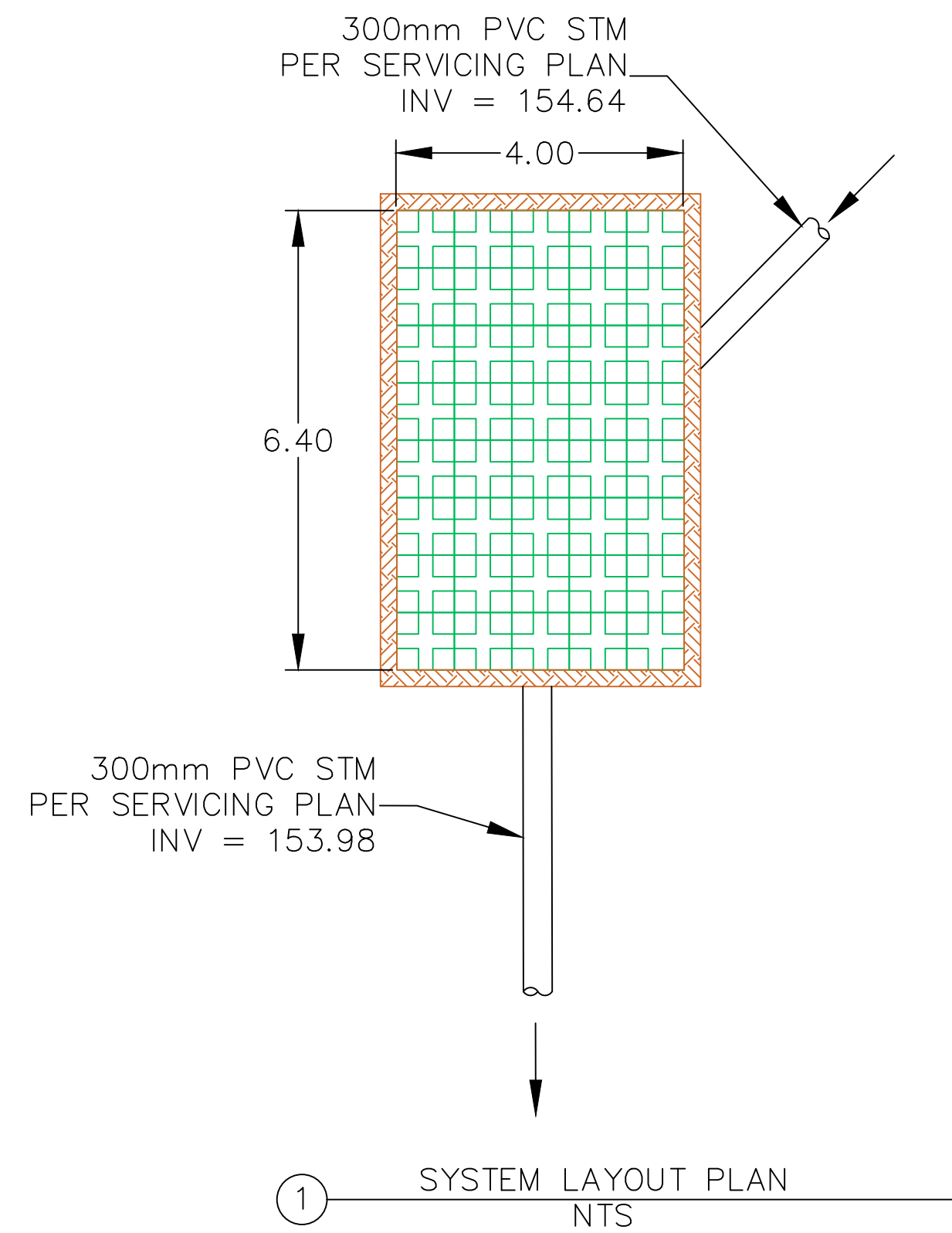
**PROPOSED SYSTEM ELEVATIONS**

(TO BE APPROVED BY ENGINEER)  
 \*ENGINEER TO CONFIRM MINIMUM AND MAXIMUM BURIAL REQUIREMENTS ARE MET

|        |  |
|--------|--|
| 159.28 | MAXIMUM ALLOWABLE GRADE (TOP OF PAVEMENT/UNPAVED): |
| 156.72 | MINIMUM ALLOWABLE GRADE                            |
| 155.92 | GREENSTORM STORAGE TOP ELEVATION LEVEL 4           |
| 155.26 | GREENSTORM STORAGE TOP ELEVATION LEVEL 3           |
| 154.60 | GREENSTORM STORAGE TOP ELEVATION LEVEL 2           |
| 153.94 | GREENSTORM STORAGE TOP ELEVATION LEVEL 1           |
| 153.28 | GREENSTORM STORAGE BOTTOM ELEVATION                |
| 153.18 | BOTTOM OF EXCAVATION                               |

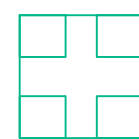

**GREENSTORM STORMWATER MANAGEMENT SYSTEM**

TOTAL STORAGE PROVIDED: 64.88m<sup>3</sup>  
 ACTIVE STORAGE ABOVE INVERT 153.98: 47.68m<sup>3</sup>  
 DEAD STORAGE BELOW INVERT 153.98: 17.20m<sup>3</sup>  
 STORAGE VOID RATIO: 0.96  
 SYSTEM AREA: 25.60 m<sup>2</sup>  
 DEPTH OF EMBEDMENT STONE: 0.00m  
 DEPTH OF BEDDING STONE: 0.00 m  
 STONE PERIMETER: 0.00 m



NOTE: ALL EXTERNAL SYSTEM STRUCTURES, INLET/OUTLET PIPES, AND PROPOSED ELEVATIONS MUST BE DESIGNED AND APPROVED BY PROJECT ENGINEER OF RECORD. PROJECT ENGINEER OF RECORD MUST ENSURE CHAMBER BURIAL REQUIREMENTS ARE MET.

**GREENSTORM LEGEND**

-  GREENSTORM ST BLOCK
-  4 OZ NON-WOVEN GEOTEXTILE

**MATERIALS LIST SUPPLIED BY STORMCON**

(SYSTEM MATERIALS LIST - SEE COVER SHEET FOR COMBINED PROJECT MATERIALS LIST)

| ITEM                                   | QUANTITY | UNIT       |
|--|----------|------------|
| GREENSTORM-ST 80x80x66 cm              | 160      | BLOCKS     |
| GREENSTORM-ST 80x80x33 cm (HALF BLOCK) | 0        | BLOCKS     |
| MULTI LAYER-CONNECTOR                  | 320      | PIECES     |
| SINGLE LAYER-CONNECTOR                 | 0        | PIECES     |
| SIDEWALL GRID                          | 104      | PIECES     |
| ADAPTER                                | 0        | PIECES     |
| 3 LAYER QUADRO-CONTROL                 | 0        | PIECES     |
| EXTENSION PIPE (6m LENGTH)             | 0        | METER      |
| CAST IRON COVER                        | 0        | PIECES     |
| 4 OZ NON-WOVEN GEOTEXTILE              | 140      | SQ. METERS |
| 8 OZ NON-WOVEN GEOTEXTILE              | 0        | SQ. METERS |
| 30MIL PVC IMPERMEABLE LINER            | 0        | SQ. METERS |
| GREENSTORM TREATMENT ROW               | 0        | METER      |
| 50MM SUBDRAIN                          | 0        | METER      |



SALES@STORMCON.CA  
 www.STORMCON.CA

THIS DRAWING WAS PREPARED TO SUPPORT THE PROJECT ENGINEER OF RECORD FOR THE PROPOSED SYSTEM. IT IS THE ULTIMATE RESPONSIBILITY OF THE PROJECT ENGINEER OF RECORD TO ENSURE THAT THE GREENSTORM SYSTEM'S DESIGN IS IN FULL COMPLIANCE WITH ALL APPLICABLE LAWS AND REGULATIONS. IT IS THE CONTRACTOR OF RECORD'S RESPONSIBILITY TO ENSURE THAT THE STORMCON PRODUCTS ARE DESIGNED IN ACCORDANCE WITH STORMCONS MINIMUM REQUIREMENTS. STORMCON DOES NOT APPROVE PLANS, SIZING, OR SYSTEM DESIGNS.

86 THOMAS STREET, MISSISSAUGA

SYSTEM LAYOUT SHEET STORAGE TANK

**GREENSTORM STORMWATER CHAMBER**

|                       |                  |
|-----------------------|------------------|
| PROJECT NO: 21-114.00 | DATE: 08/10/2021 |
| DESIGNED BY: VS       | CHECKED BY: VS   |
| SCALE: N.T.S.         | SHEET NO: 2 OF 5 |

|                       |                          |                               |
|-----------------------|--------------------------|-------------------------------|
| Project Name          | 86 Thomas St R3          |                               |
| Location              | Mississauga, ON          |                               |
| Date                  | Tuesday, August 10, 2021 |                               |
| Chamber Model         | GreenStorm-ST            |                               |
| Number of Layers      | 4.0                      | Top Stone 0.00 m              |
| Height of Chambers    | 2.64 m                   | Bottom Stone 0.00 m           |
| Chamber Length        | 6.40                     | Perimeter Stone 0.00 m        |
| Chamber Width         | 4.00                     | Stone Qty 0.00 m <sup>3</sup> |
| Storage Void Ratio    | 0.96                     | Stone Void Ratio 40.00%       |
| System Perimeter      | 20.80                    |                               |
| System Area           | 25.60 m <sup>2</sup>     | Liner No                      |
| System Base Elevation | 153.28 m                 |                               |

| Height of System |        | GreenStorm Volume |                 | Stone Volume   |                 | Cumulative Storage Volume |                 | Elevation |        |                   |
|------------------|--------|-------------------|-----------------|----------------|-----------------|---------------------------|-----------------|-----------|--------|-------------------|
| mm               | in     | m <sup>3</sup>    | ft <sup>3</sup> | m <sup>3</sup> | ft <sup>3</sup> | m <sup>3</sup>            | ft <sup>3</sup> | m         | ft     |                   |
| 2640             | 103.94 | 0.98              | 34.72           | 0.00           | 0.00            | 64.88                     | 2,291.24        | 155.92    | 511.55 | Top of GreenStorm |
| 2600             | 102.36 | 0.61              | 21.70           | 0.00           | 0.00            | 63.90                     | 2,256.52        | 155.88    | 511.42 |                   |
| 2575             | 101.38 | 0.61              | 21.70           | 0.00           | 0.00            | 63.28                     | 2,234.83        | 155.86    | 511.34 |                   |
| 2550             | 100.39 | 0.61              | 21.70           | 0.00           | 0.00            | 62.67                     | 2,213.13        | 155.83    | 511.25 |                   |
| 2525             | 99.41  | 0.61              | 21.70           | 0.00           | 0.00            | 62.05                     | 2,191.43        | 155.81    | 511.17 |                   |
| 2500             | 98.43  | 0.61              | 21.70           | 0.00           | 0.00            | 61.44                     | 2,169.73        | 155.78    | 511.09 |                   |
| 2475             | 97.44  | 0.61              | 21.70           | 0.00           | 0.00            | 60.83                     | 2,148.04        | 155.76    | 511.01 |                   |
| 2450             | 96.46  | 0.61              | 21.70           | 0.00           | 0.00            | 60.21                     | 2,126.34        | 155.73    | 510.93 |                   |
| 2425             | 95.47  | 0.61              | 21.70           | 0.00           | 0.00            | 59.60                     | 2,104.64        | 155.71    | 510.84 |                   |
| 2400             | 94.49  | 0.61              | 21.70           | 0.00           | 0.00            | 58.98                     | 2,082.94        | 155.68    | 510.76 |                   |
| 2375             | 93.50  | 0.61              | 21.70           | 0.00           | 0.00            | 58.37                     | 2,061.25        | 155.66    | 510.68 |                   |
| 2350             | 92.52  | 0.61              | 21.70           | 0.00           | 0.00            | 57.75                     | 2,039.55        | 155.63    | 510.60 |                   |
| 2325             | 91.54  | 0.61              | 21.70           | 0.00           | 0.00            | 57.14                     | 2,017.85        | 155.61    | 510.52 |                   |
| 2300             | 90.55  | 0.61              | 21.70           | 0.00           | 0.00            | 56.52                     | 1,996.15        | 155.58    | 510.43 |                   |
| 2275             | 89.57  | 0.61              | 21.70           | 0.00           | 0.00            | 55.91                     | 1,974.46        | 155.56    | 510.35 |                   |
| 2250             | 88.58  | 0.61              | 21.70           | 0.00           | 0.00            | 55.30                     | 1,952.76        | 155.53    | 510.27 |                   |
| 2225             | 87.60  | 0.61              | 21.70           | 0.00           | 0.00            | 54.68                     | 1,931.06        | 155.51    | 510.19 |                   |
| 2200             | 86.61  | 0.61              | 21.70           | 0.00           | 0.00            | 54.07                     | 1,909.37        | 155.48    | 510.10 |                   |
| 2175             | 85.63  | 0.61              | 21.70           | 0.00           | 0.00            | 53.45                     | 1,887.67        | 155.46    | 510.02 |                   |
| 2150             | 84.65  | 0.61              | 21.70           | 0.00           | 0.00            | 52.84                     | 1,865.97        | 155.43    | 509.94 |                   |
| 2125             | 83.66  | 0.61              | 21.70           | 0.00           | 0.00            | 52.22                     | 1,844.27        | 155.41    | 509.86 |                   |
| 2100             | 82.68  | 0.61              | 21.70           | 0.00           | 0.00            | 51.61                     | 1,822.58        | 155.38    | 509.78 |                   |
| 2075             | 81.69  | 0.61              | 21.70           | 0.00           | 0.00            | 51.00                     | 1,800.88        | 155.36    | 509.69 |                   |
| 2050             | 80.71  | 0.61              | 21.70           | 0.00           | 0.00            | 50.38                     | 1,779.18        | 155.33    | 509.61 |                   |
| 2025             | 79.72  | 0.61              | 21.70           | 0.00           | 0.00            | 49.77                     | 1,757.48        | 155.31    | 509.53 |                   |
| 2000             | 78.74  | 0.61              | 21.70           | 0.00           | 0.00            | 49.15                     | 1,735.79        | 155.28    | 509.45 |                   |
| 1975             | 77.76  | 0.61              | 21.70           | 0.00           | 0.00            | 48.54                     | 1,714.09        | 155.26    | 509.37 |                   |
| 1950             | 76.77  | 0.61              | 21.70           | 0.00           | 0.00            | 47.92                     | 1,692.39        | 155.23    | 509.28 |                   |
| 1925             | 75.79  | 0.61              | 21.70           | 0.00           | 0.00            | 47.31                     | 1,670.69        | 155.21    | 509.20 |                   |
| 1900             | 74.80  | 0.61              | 21.70           | 0.00           | 0.00            | 46.69                     | 1,649.00        | 155.18    | 509.12 |                   |
| 1875             | 73.82  | 0.61              | 21.70           | 0.00           | 0.00            | 46.08                     | 1,627.30        | 155.16    | 509.04 |                   |
| 1850             | 72.83  | 0.61              | 21.70           | 0.00           | 0.00            | 45.47                     | 1,605.60        | 155.13    | 508.96 |                   |
| 1825             | 71.85  | 0.61              | 21.70           | 0.00           | 0.00            | 44.85                     | 1,583.91        | 155.11    | 508.87 |                   |
| 1800             | 70.87  | 0.61              | 21.70           | 0.00           | 0.00            | 44.24                     | 1,562.21        | 155.08    | 508.79 |                   |
| 1775             | 69.88  | 0.61              | 21.70           | 0.00           | 0.00            | 43.62                     | 1,540.51        | 155.06    | 508.71 |                   |
| 1750             | 68.90  | 0.61              | 21.70           | 0.00           | 0.00            | 43.01                     | 1,518.81        | 155.03    | 508.63 |                   |
| 1725             | 67.91  | 0.61              | 21.70           | 0.00           | 0.00            | 42.39                     | 1,497.12        | 155.01    | 508.55 |                   |
| 1700             | 66.93  | 0.61              | 21.70           | 0.00           | 0.00            | 41.78                     | 1,475.42        | 154.98    | 508.46 |                   |
| 1675             | 65.94  | 0.61              | 21.70           | 0.00           | 0.00            | 41.16                     | 1,453.72        | 154.96    | 508.38 |                   |
| 1650             | 64.96  | 0.61              | 21.70           | 0.00           | 0.00            | 40.55                     | 1,432.02        | 154.93    | 508.30 |                   |
| 1625             | 63.98  | 0.61              | 21.70           | 0.00           | 0.00            | 39.94                     | 1,410.33        | 154.91    | 508.22 |                   |
| 1600             | 62.99  | 0.61              | 21.70           | 0.00           | 0.00            | 39.32                     | 1,388.63        | 154.88    | 508.14 |                   |
| 1575             | 62.01  | 0.61              | 21.70           | 0.00           | 0.00            | 38.71                     | 1,366.93        | 154.86    | 508.05 |                   |
| 1550             | 61.02  | 0.61              | 21.70           | 0.00           | 0.00            | 38.09                     | 1,345.23        | 154.83    | 507.97 |                   |
| 1525             | 60.04  | 0.61              | 21.70           | 0.00           | 0.00            | 37.48                     | 1,323.54        | 154.81    | 507.89 |                   |
| 1500             | 59.06  | 0.61              | 21.70           | 0.00           | 0.00            | 36.86                     | 1,301.84        | 154.78    | 507.81 |                   |
| 1475             | 58.07  | 0.61              | 21.70           | 0.00           | 0.00            | 36.25                     | 1,280.14        | 154.76    | 507.73 |                   |
| 1450             | 57.09  | 0.61              | 21.70           | 0.00           | 0.00            | 35.64                     | 1,258.45        | 154.73    | 507.64 |                   |
| 1425             | 56.10  | 0.61              | 21.70           | 0.00           | 0.00            | 35.02                     | 1,236.75        | 154.71    | 507.56 |                   |

| Height of System |       | GreenStorm Volume |                 | Stone Volume   |                 | Cumulative Storage Volume |                 | Elevation |        |  |
|------------------|-------|-------------------|-----------------|----------------|-----------------|---------------------------|-----------------|-----------|--------|--|
| mm               | in    | m <sup>3</sup>    | ft <sup>3</sup> | m <sup>3</sup> | ft <sup>3</sup> | m <sup>3</sup>            | ft <sup>3</sup> | m         | ft     |  |
| 1400             | 55.12 | 0.61              | 21.70           | 0.00           | 0.00            | 34.41                     | 1,215.05        | 154.68    | 507.48 |  |
| 1375             | 54.13 | 0.61              | 21.70           | 0.00           | 0.00            | 33.79                     | 1,193.35        | 154.66    | 507.40 |  |
| 1350             | 53.15 | 0.61              | 21.70           | 0.00           | 0.00            | 33.18                     | 1,171.66        | 154.63    | 507.32 |  |
| 1325             | 52.17 | 0.61              | 21.70           | 0.00           | 0.00            | 32.56                     | 1,149.96        | 154.61    | 507.23 |  |
| 1300             | 51.18 | 0.61              | 21.70           | 0.00           | 0.00            | 31.95                     | 1,128.26        | 154.58    | 507.15 |  |
| 1275             | 50.20 | 0.61              | 21.70           | 0.00           | 0.00            | 31.33                     | 1,106.56        | 154.56    | 507.07 |  |
| 1250             | 49.21 | 0.61              | 21.70           | 0.00           | 0.00            | 30.72                     | 1,084.87        | 154.53    | 506.99 |  |
| 1225             | 48.23 | 0.61              | 21.70           | 0.00           | 0.00            | 30.11                     | 1,063.17        | 154.51    | 506.91 |  |
| 1200             | 47.24 | 0.61              | 21.70           | 0.00           | 0.00            | 29.49                     | 1,041.47        | 154.48    | 506.82 |  |
| 1175             | 46.26 | 0.61              | 21.70           | 0.00           | 0.00            | 28.88                     | 1,019.77        | 154.46    | 506.74 |  |
| 1150             | 45.28 | 0.61              | 21.70           | 0.00           | 0.00            | 28.26                     | 998.08          | 154.43    | 506.66 |  |
| 1125             | 44.29 | 0.61              | 21.70           | 0.00           | 0.00            | 27.65                     | 976.38          | 154.41    | 506.58 |  |
| 1100             | 43.31 | 0.61              | 21.70           | 0.00           | 0.00            | 27.03                     | 954.68          | 154.38    | 506.50 |  |
| 1075             | 42.32 | 0.61              | 21.70           | 0.00           | 0.00            | 26.42                     | 932.99          | 154.36    | 506.41 |  |
| 1050             | 41.34 | 0.61              | 21.70           | 0.00           | 0.00            | 25.80                     | 911.29          | 154.33    | 506.33 |  |
| 1025             | 40.35 | 0.61              | 21.70           | 0.00           | 0.00            | 25.19                     | 889.59          | 154.31    | 506.25 |  |
| 1000             | 39.37 | 0.61              | 21.70           | 0.00           | 0.00            | 24.58                     | 867.89          | 154.28    | 506.17 |  |
| 975              | 38.39 | 0.61              | 21.70           | 0.00           | 0.00            | 23.96                     | 846.20          | 154.26    | 506.09 |  |
| 950              | 37.40 | 0.61              | 21.70           | 0.00           | 0.00            | 23.35                     | 824.50          | 154.23    | 506.00 |  |
| 925              | 36.42 | 0.61              | 21.70           | 0.00           | 0.00            | 22.73                     | 802.80          | 154.21    | 505.92 |  |
| 900              | 35.43 | 0.61              | 21.70           | 0.00           | 0.00            | 22.12                     | 781.10          | 154.18    | 505.84 |  |
| 875              | 34.45 | 0.61              | 21.70           | 0.00           | 0.00            | 21.50                     | 759.41          | 154.16    | 505.76 |  |
| 850              | 33.46 | 0.61              | 21.70           | 0.00           | 0.00            | 20.89                     | 737.71          | 154.13    | 505.68 |  |
| 825              | 32.48 | 0.61              | 21.70           | 0.00           | 0.00            | 20.28                     | 716.01          | 154.11    | 505.59 |  |
| 800              | 31.50 | 0.61              | 21.70           | 0.00           | 0.00            | 19.66                     | 694.31          | 154.08    | 505.51 |  |
| 775              | 30.51 | 0.61              | 21.70           | 0.00           | 0.00            | 19.05                     | 672.62          | 154.06    | 505.43 |  |
| 750              | 29.53 | 0.61              | 21.70           | 0.00           | 0.00            | 18.43                     | 650.92          | 154.03    | 505.35 |  |
| 725              | 28.54 | 0.61              | 21.70           | 0.00           | 0.00            | 17.82                     | 629.22          | 154.01    | 505.27 |  |
| 700              | 27.56 | 0.61              | 21.70           | 0.00           | 0.00            | 17.20                     | 607.53          | 153.98    | 505.18 |  |
| 675              | 26.57 | 0.61              | 21.70           | 0.00           | 0.00            | 16.59                     | 585.83          | 153.96    | 505.10 |  |
| 650              | 25.59 | 0.61              | 21.70           | 0.00           | 0.00            | 15.97                     | 564.13          | 153.93    | 505.02 |  |
| 625              | 24.61 | 0.61              | 21.70           | 0.00           | 0.00            | 15.36                     | 542.43          | 153.91    | 504.94 |  |
| 600              | 23.62 | 0.61              | 21.70           | 0.00           | 0.00            | 14.75                     | 520.74          | 153.88    | 504.86 |  |
| 575              | 22.64 | 0.61              | 21.70           | 0.00           | 0.00            | 14.13                     | 499.04          | 153.86    | 504.77 |  |
| 550              | 21.65 | 0.61              | 21.70           | 0.00           | 0.00            | 13.52                     | 477.34          | 153.83    | 504.69 |  |
| 525              | 20.67 | 0.61              | 21.70           | 0.00           | 0.00            | 12.90                     | 455.64          | 153.81    | 504.61 |  |
| 500              | 19.69 | 0.61              | 21.70           | 0.00           | 0.00            | 12.29                     | 433.95          | 153.78    | 504.53 |  |
| 475              | 18.70 | 0.61              | 21.70           | 0.00           | 0.00            | 11.67                     | 412.25          | 153.76    | 504.45 |  |
| 450              | 17.72 | 0.61              | 21.70           | 0.00           | 0.00            | 11.06                     | 390.55          | 153.73    | 504.36 |  |
| 425              | 16.73 | 0.61              | 21.70           | 0.00           | 0.00            | 10.44                     | 368.85          | 153.71    | 504.28 |  |
| 400              | 15.75 | 0.61              | 21.70           | 0.00           | 0.00            | 9.83                      | 347.16          | 153.68    | 504.20 |  |
| 375              | 14.76 | 0.61              | 21.70           | 0.00           | 0.00            | 9.22                      | 325.46          | 153.66    | 504.12 |  |
| 350              | 13.78 | 0.61              | 21.70           | 0.00           | 0.00            | 8.60                      | 303.76          | 153.63    | 504.04 |  |
| 325              | 12.80 | 0.61              | 21.70           | 0.00           | 0.00            | 7.99                      | 282.07          | 153.61    | 503.95 |  |
| 300              | 11.81 | 0.61              | 21.70           | 0.00           | 0.00            | 7.37                      | 260.37          | 153.58    | 503.87 |  |
| 275              | 10.83 | 0.61              | 21.70           | 0.00           | 0.00            | 6.76                      | 238.67          | 153.56    | 503.79 |  |
| 250              | 9.84  | 0.61              | 21.70           | 0.00           | 0.00            | 6.14                      | 216.97          | 153.53    | 503.71 |  |
| 225              | 8.86  | 0.61              | 21.70           | 0.00           | 0.00            | 5.53                      | 195.28          | 153.51    | 503.63 |  |
| 200              | 7.87  | 0.61              | 21.70           | 0.00           | 0.00            | 4.92                      | 173.58          | 153.48    | 503.54 |  |
| 175              | 6.89  | 0.61              | 21.70           | 0.00           | 0.00            | 4.30                      | 151.88          | 153.46    | 503.46 |  |
| 150              | 5.91  | 0.61              | 21.70           | 0.00           | 0.00            | 3.69                      | 130.18          | 153.43    | 503.38 |  |
| 125              | 4.92  | 0.61              | 21.70           | 0.00           | 0.00            | 3.07                      | 108.49          | 153.41    | 503.30 |  |
| 100              | 3.94  | 0.61              | 21.70           | 0.00           | 0.00            | 2.46                      | 86.79           | 153.38    | 503.22 |  |
| 75               | 2.95  | 0.61              | 21.70           | 0.00           | 0.00            | 1.84                      | 65.09           | 153.36    | 503.13 |  |
| 50               | 1.97  | 0.61              | 21.70           | 0.00           | 0.00            | 1.23                      | 43.39           | 153.33    | 503.05 |  |
| 25               | 0.98  | 0.61              | 21.70           | 0.00           | 0.00            | 0.61                      | 21.70           | 153.31    | 502.97 |  |
| 0                | 0.00  | 0.00              | 0.00            | 0.26           |                 |                           |                 |           |        |  |

GRANT COVERAGE  
RADIUS 75m

SAN MH102A  
1200mmØ  
OPSD 701.010  
T/G=156.68  
E.INV.=152.73  
S.INV.=152.68

STM MH102  
1200mmØ  
OPSD 701.010  
T/G=156.65  
E.INV.=154.35  
SW.INV.=154.30

AD03  
TOP=156.76  
S.INV.=154.40

N 40°31'30" E 39.09 (P2, P3 & Meas) 39.13

No Fence

MH Top  
58.06  
PERMEABLE PRECAST  
PEDESTRIAN  
300mmØ-3.6m PVC STM @0.5%

Post  
150mm 45° BEND  
U.S. RECEPTACLE  
0.3 W

GRASS 40.0 m³ UNDERGROUND  
STORMWATER TANK

250mmØ-31.7m PVC SAN @1.5%

300mmØ-30.3m PVC STM @0.5%

PROP. 150mmØ WM

300mmØ-11.0m PVC STM @0.5%

PERMEABLE PRECAST  
CONCRETE UNIT

150mmØ-10.6m PVC STM SUBDRAIN

STM CBMH101  
1200mmØ  
OPSD 701.010  
T/G=156.59  
E.INV.=153.66  
N.INV.=153.66

FFE=157.00

25mm WATER  
CONN. WITH V&B TYP

GARBAGE AND  
RECYCLING BINS

125mm

0.04 (Meas)  
& P3

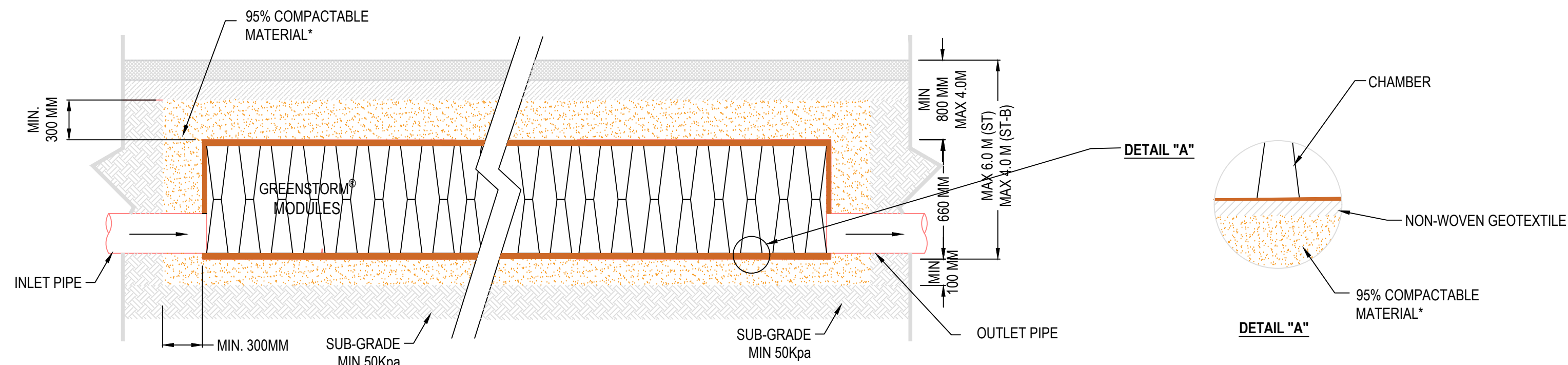


SALES@STORMCON.CA  
WWW.STORMCON.CA

THIS DRAWING WAS PREPARED TO SUPPORT THE PROJECT ENGINEER OF RECORD FOR THE PROPOSED SYSTEM. IT IS THE ULTIMATE RESPONSIBILITY OF THE PROJECT ENGINEER OF RECORD TO ENSURE THAT THE GREENSTORM SYSTEM'S DESIGN IS IN FULL COMPLIANCE WITH ALL APPLICABLE LAWS AND REGULATIONS. IT IS THE CONTRACTOR OF RECORD'S RESPONSIBILITY TO ENSURE THAT THE STORMCON PRODUCTS ARE DESIGNED IN ACCORDANCE WITH STORMCONS MINIMUM REQUIREMENTS. STORMCON DOES NOT APPROVE PLANS, SIZING, OR SYSTEM DESIGNS.

86 THOMAS STREET, MISSISSAUGA  
  
SYSTEM OVERLAY SHEET

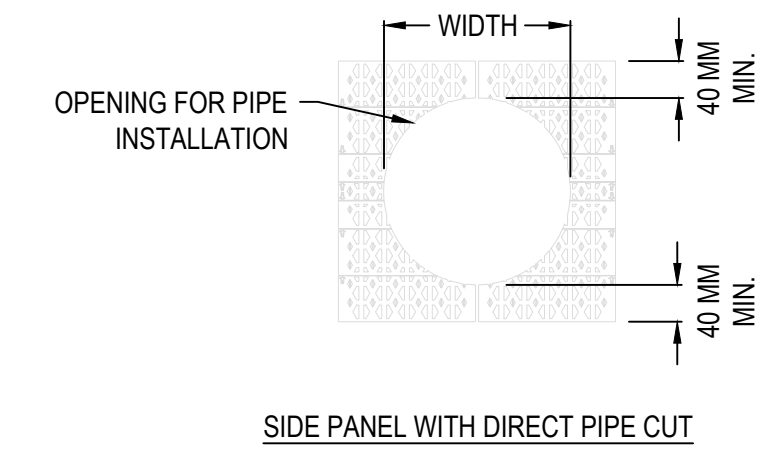
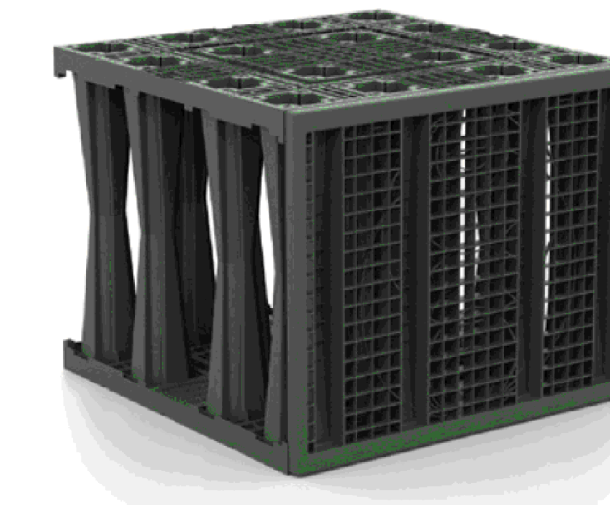
| GREENSTORM STORMWATER CHAMBER |                  |
|-------------------------------|------------------|
| PROJECT NO: 21-114.00         | DATE: 08/10/2021 |
| DESIGNED BY: VS               | CHECKED BY: VS   |
| SCALE: N.T.S.                 | SHEET NO: 4 OF 5 |



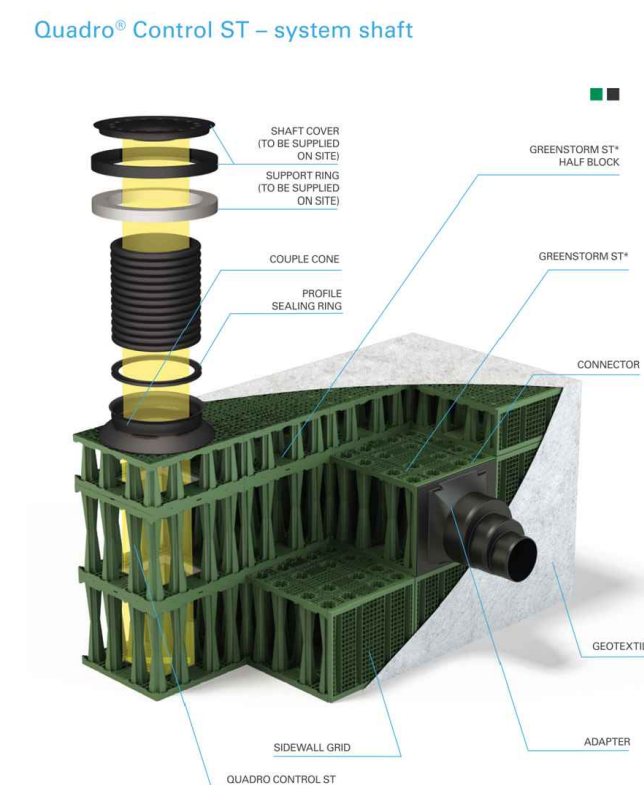
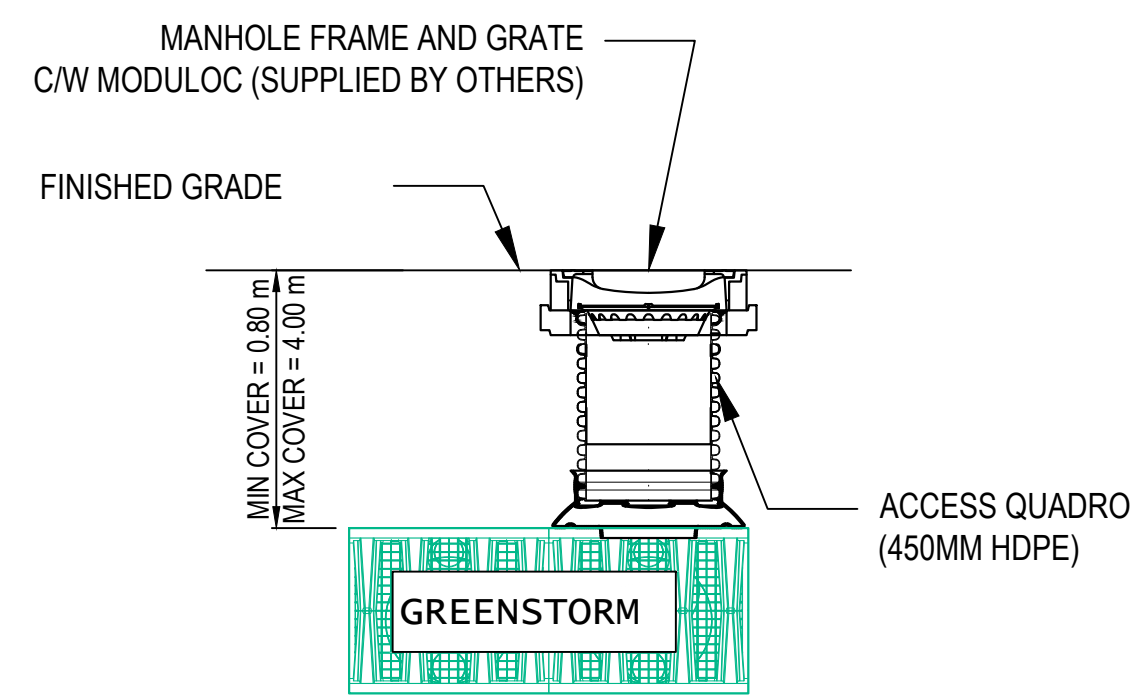
| COMPACTABLE MATERIAL LIST | LEGEND                      |
|---------------------------|-----------------------------|
| • SAND                    | — 4 OZ NON-WOVEN GEOTEXTILE |

TYPICAL ONE LAYER GREENSTORM CROSS SECTION

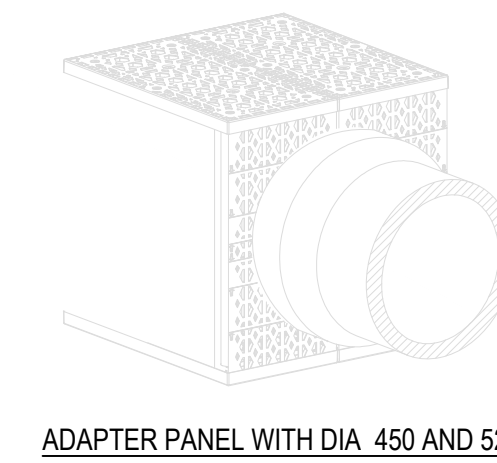
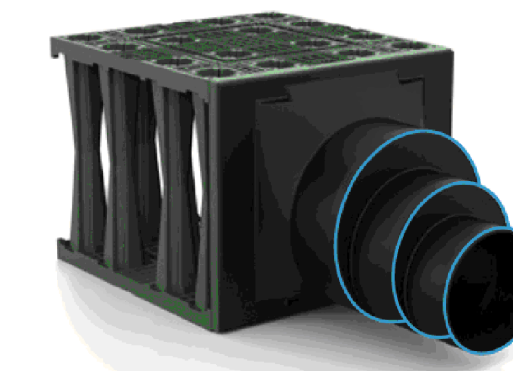
FULL CONNECTION OPTIONS  
Dia 100mm, 150 mm, 200 mm, 250 mm, 300 mm AND 375 mm



STANDARD SIDE PANEL WITH DIRECT PIPE CUT



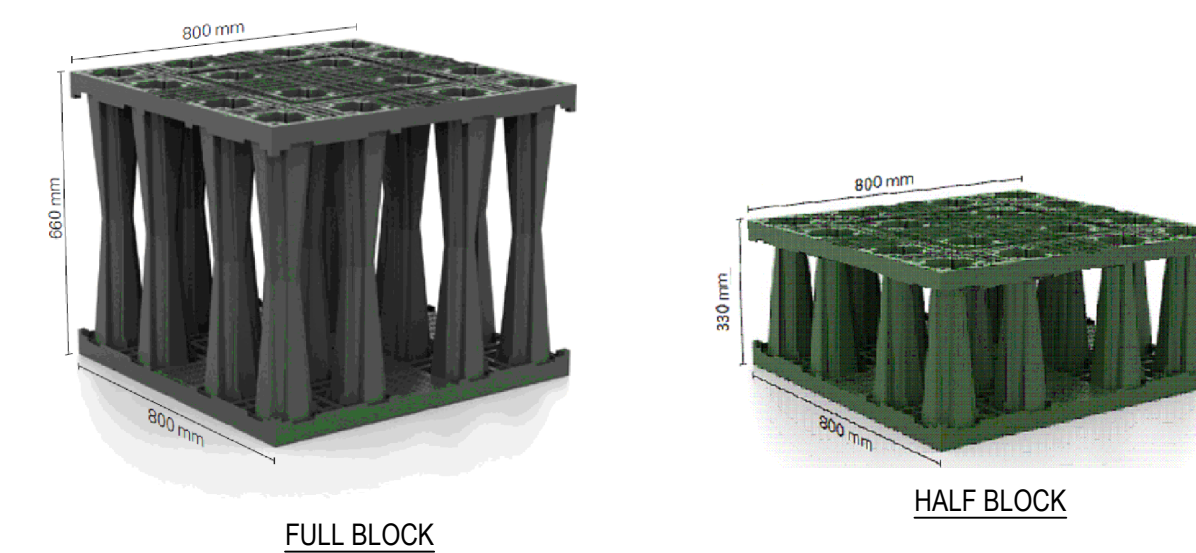
GREENSTORM ACCESS QUADRO DETAIL (WHERE APPLICABLE)



STANDARD ADAPTER PANEL WITH DIA 450 AND 525



STANDARD TREATMENT ROW DETAIL (WHERE APPLICABLE)



STANDARD GREENSTORM BLOCK DETAIL



10 CEDAR AVE  
THORNHILL ON  
L3T 3W1

SALES@STORMCON.CA  
WWW.STORMCON.CA

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DETAILS

GREENSTORM STORMWATER CHAMBER

|                       |                  |
|-----------------------|------------------|
| PROJECT NO: 21-114.00 | DATE: 08/10/2021 |
| DESIGNED BY: VS       | CHECKED BY: VS   |
| SCALE: N.T.S.         | SHEET NO: 5 OF 5 |