

1672735 Ontario Inc.

Functional Servicing and Stormwater Management Report (FSR/SWM)

**Residential Development
2620 Chalkwell Close, Mississauga**

December 2023

Functional Services and Stormwater Management Report
2620 Chalkwell Close, Mississauga

Functional Services and Stormwater Management Report (FSR/SWM)

Residential Development at 2620 Chalkwell Close, Mississauga

December 22, 2023

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Version Control

Revision No.	Date Issued	Description	Prepared/Reviewed By
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1 Introduction

1.1 Background

Arcadis Professional Services (Canada) Inc. (Arcadis) was retained by 1672735 Ontario Inc (the “Owner”) to prepare a Functional Servicing and Stormwater Management Report for the proposed residential development located at 2620 Chalkwell Close, in the City of Mississauga (the “City”).

The purpose of this report is to provide detailed design information for the City’s review with respect to the infrastructure required to support the proposed development regarding storm drainage, sanitary sewers and water supply.

A request to the City’s engineering records department was carried out to obtain existing information in preparation of this report.

The following documents were available for our review for the preparation of this report:

- Plan and Profile of Chalkwell Close, Drawing No. D-6446 from the Region of Peel, dated September 1958
- Plan and Profile of Chalkwell Close, Drawing No. 41354-D from the Region of Peel, dated August 2010

In addition, Arcadis IBI was also provided with the following information from the applicant:

- Topographic Survey prepared by R. Avis Surveying Inc. dated August 25, 2023
- 2620 Chalkwell Close Site Plan prepared by 1672735 Ontario Inc., dated December 13, 2023

1.2 Existing Site Description

The existing 19,862 m² (1.99 ha) Site is located in the City of Mississauga at the west end of Chalkwell Close, west of Karenza Road and borders the east side of Sandgate Park. The Site currently consists of landscaped area but was previously the Site of an elementary school. The legal description is as follows: All of Block B, registered plan 619, City of Mississauga. The Site's municipal address is 2620 Chalkwell Close in Mississauga, Ontario, L5J 2B9. Please refer to **Figure FIG-1** and **Figure FIG-2 (Appendix A)** for the Site Location Plan and Aerial Plan.

The existing Site was previously occupied by a single storey elementary school, but is currently abandoned and partially demolished. The Site generally slopes from the west to the east towards Chalkwell Close. The flow is primarily collected by two catchbasins on the northeast end and southeast ends of the Site.

The Site is located in an area of the City that is serviced by a network of municipal infrastructure including roads, sewers, watermains, and other services and utilities. Locations and conditions of all utilities should be verified at the time of construction.

2 Site Proposal

The proposed Site will contain 12 3-storey townhouse blocks with internal parking within each block, as well as guest vehicle parking along private roads fronting all townhouse blocks, and 2 amenity areas. Site access will be in the east corner of the Site via Chalkwell Close. Primary pedestrian access to the proposed development will also be via Chalkwell Close. The proposed private road and vehicle access is to match existing conditions at Chalkwell Close and within the Site itself. Due to grading constraints, there will be a proposed retaining wall along the north corner of the Site. The total gross floor area (GFA) for the Site is 26,252 m². Please refer to **Appendix A** for the proposed Site plan along with development statistics as prepared by 1672735 Ontario Inc.

3 Terms of Reference and Methodology

3.1 Terms of Reference

The Terms of Reference used for the scope of this report was based on current Region of Peel Transportation and Works Department Water and Wastewater Branch Standards and the City of Mississauga's Transportation and Works Development Requirements Manual and Standard Drawings.

3.2 Methodology: Sanitary Discharge

The sanitary sewage discharge from the Site will be determined using sanitary sewer design sheets that consider the land use and building statistics as supplied by the design team. The calculated values provide peak sanitary flow discharge with infiltration considerations. The estimated sanitary discharge flows from the proposed Site will be calculated based on the Region of Peel criteria shown in **Table 3-1** below.

Table 3-1 Sanitary Flows

USAGE	DESIGN FLOW	UNITS	PERSONS
Residential Flow Generation	290	Litres/Person/Day	Townhouses = 3.4 ppu
Extraneous Flow (Infiltration)	0.2	Litres/Second/Hectare	N/A
Peaking Factor	$M=1+14/[4+(P/1000)^{0.5}]$	Where P is Population in Thousands	N/A

Based on the calculated peak flows, the adequacy of the existing infrastructure to support the proposed development will be discussed.

3.3 Methodology: Water Usage

The domestic water usage will be calculated based on the Region’s design criteria as outlined in **Table 3-2** below.

Table 3-2 Water Usage

USAGE	WATER DEMAND	UNITS
Residential	280	Litres/Capita/Day

Pressure and flow testing to determine the adequacy of the existing watermain to support the development with fire suppression in accordance with the FUS Guidelines will be discussed in the subsequent **Section 6**.

3.4 Methodology: Stormwater Drainage and Management

The following report provides a review of the pre- and post-development Site conditions and comments on opportunities to reduce post-development peak flows. Requirements set by the City of Mississauga, Ministry of the Environment Conservation and Parks (MECP) were reviewed. The following SWM criteria are to be applied:

Water Quantity

Post-development peak flows for all storms up to and including the 100-year event should be controlled to unit release rates.

Water Quality

Enhanced Level 1 Protection, with a long-term average removal of 80% of the Total Suspended Solids (TSS) must be achieved on an annual loading basis.

Water Balance

Runoff resulting from a 5 mm rainfall event or best efforts shall be retained on-site using Low Impact Development (LID) practices including infiltration, evapotranspiration and/or water reuse measures.

4 Stormwater Management and Drainage

4.1 Existing Conditions

According to available records, there is an existing 375 mm diameter storm sewer within Chalkwell Close that terminates at an existing maintenance hole, just east of the proposed Site entrance. There is a 525 mm storm sewer within Karenza Road that connects into a maintenance hole downstream of the 375 mm sewer within Chalkwell Close. Downstream on Chalkwell Close, the sewer becomes a 600 mm pipe leading to Sandgate Crescent.

The following drainage conditions to Chalkwell Close and Karenza Road, which is part of the Sheridan Creek watershed, currently exist for the subject lands:

- A1Pre drains northeast to a catchbasin (EX. CB1) that connects to Karenza Road.
- A2Pre drains southeast to a catchbasin (EX. CB2) that connects to Chalkwell Close.

Table 4-1 summarizes the pre-development drainage areas and their corresponding parameters. The existing drainage areas are also illustrated on **Figure DAP-1** in **Appendix B**.

Table 4-1 Existing Conditions Input Parameters

CATCHMENT	DRAINAGE AREA(HA)	RUNOFF COEFFICIENT(C)
AREA DRAINING TO KARENZA ROAD		
A1Pre	0.17	0.25
AREA DRAINING TO CHALKWELL CLOSE		
A2Pre	1.81	0.62

The Site is split into two drainage areas, 0.17 ha draining to the Karenza Road storm sewer and 1.81 ha draining to the Chalkwell Close storm sewer. Area A1Pre drains to EX. CB1 / 450 mm lead connecting to the 525 mm storm sewer in Karenza Road. Area A2Pre drains to EX. CB2, leading to the 375 mm storm sewer within Chalkwell Close.

4.2 Design Criteria

Based on a review of the City of Mississauga Guidelines, the Stormwater Management Criteria applicable to the Site are as outlined in **Table 4-2** below.

Table 4-2 Stormwater Management Criteria

CRITERIA	REQUIREMENT
Water Balance	Retain 5mm for the Sites total impervious area (excluding initial abstraction)
Quantity Control	100-Year Post to 2-Year Pre-development Control
Quality Control	80% TSS Removal

4.2.1 Stormwater Quantity

For the City of Mississauga, the allowable release rate to the municipal storm sewer system from the development Site up to and including 100-year storm event must not exceed the 2-year runoff rate from the Site under pre-development conditions.

4.2.2 Stormwater Balance

The criteria provided in the City of Mississauga's Storm Drainage criteria states that controls should be in place, such that the runoff resulting from a 5 mm rainfall event for the Sites impervious area can be retained on-site via infiltration, evapotranspiration and/or water reuse measures.

4.2.3 Stormwater Quality

For the City of Mississauga, a minimum treatment of 80% of the Total Suspended Solids (TSS) removal on an annual loading basis must be achieved. TSS removal efficiency is to be based on 100% of the runoff leaving the Site from all storm events that occurs in an average year.

4.3 Stormwater Management

4.3.1 General

Table 4-3 below summarizes the proposed conditions drainage parameters. Please refer to **Appendix B** for calculations and **Figure DAP-2** for proposed drainage areas.

Table 4-3 Proposed Condition Drainage Parameters

CATCHMENT	DRAINAGE AREA (HA)	C	TC (MIN)
A1Post	1.91	0.76	15
A2Post	0.07	0.25	15

4.3.2 Stormwater Quantity Control

Catchment A1Post a 200mm orifice pipe will be utilized to control 100-year post-development flows to such that the total flow from the Site meets the allowable flow. Catchment A2Post will flow to the EX. CB1 and flow uncontrolled to Karenza Road. Please refer to **Appendix B** for detailed calculations. A summary of the 100-year post development flows is shown below in **Table 4-4**.

Table 4-4 Post Development Flows Discharging to the Bathurst Street Right-of-Way

STORM EVENT	CATCHMENT	TARGET FLOW (L/S)	POST DEVELOPMENT FLOW (L/S)	FLOW LEAVING SITE (L/S)
100-Year	A1Post	188.0	485.2	125.7
100-Year	A2Post	7.1	6.8	6.8

The maximum storage required is 435.4 m³ and will be provided through a combination of storage pipe, storage within maintenance structures, storage chambers and rooftop storage. Please also refer to **DWG SS-01** in **Appendix E** for the location and details of storm system. Detailed storage and orifice sizing calculations are shown **Appendix B**.

4.3.3 Stormwater Quality

For the A2Post catchment, there will be no impact to the TSS loading rate, as the runoff is generated from the landscaped areas. Therefore, 80% TSS removal has been achieved for catchment areas A2Post.

For area A1Post, quality control will be provided by a combination of an OGS and inherent treatment from rooftop/patios and landscaping. For MECP Enhanced Level protection, the proposed OGS system will be installed to treat the drainage collected from paved areas via catchbasins. The OGS unit will be installed at the downstream end of the storm sewer, prior to outletting to the municipal control maintenance hole. Please refer to **Drawing SS-01** in **Appendix E** for the location of the OGS unit and proposed storm network.

Based on water quality calculations, the TSS removal rate under post-development conditions is 81%. Therefore, the minimum TSS removal of 80% will be achieved. Detailed quality control calculations are provided in **Appendix B**.

Water quality calculations are shown below in **Table 4-5**.

Table 4-5 Water Quality Calculations

SURFACE	METHOD	EFFECTIVE TSS REMOVAL	AREA	% AREA OF SITE	OVERALL TSS REMOVAL
Roof/Patio	Inherent	80%	0.86	31%	25%
Landscape	Inherent	80%	0.40	14%	12%
Paved Controlled	OGS	80%	1.51	54%	44%
TOTAL			2.77	100%	81%

4.3.4 Stormwater Balance

As required by the City, a rainfall depth of 5mm must be retained over the total Site impervious area, excluding initial extraction. The total impervious area of the Site is 15,080 m² (1.51 ha), which equates to a required water re-use volume of 75.4 m³. Therefore, 75.4 m³ is required to be retained on Site. Measures such as infiltration systems/galleries, permeable pavers and increased topsoil depths around the property can be used to retain the required volume.

4.3.5 Proposed Storm Connection

The Site will have a gravity network within the property to collect surface runoff from the amenity spaces and private roadways, as well as connections at each block to collect roof drainage. The network will flow from north to south to a storm control maintenance hole, at the downstream end, located just east of the proposed Site entrance. The Sites municipal service connection will be made from the control maintenance hole to an existing maintenance hole at the terminating end of a 375 mm storm sewer within Chalkwell Close.

Please refer to **Drawing SS-01** in **Appendix E** for the location and cross-sections of the storm service connection.

5 Sanitary Drainage System

5.1 Existing Sanitary Drainage System

According to the reviewed information as stated in **Section 1.1**, there is an existing 250 mm diameter sanitary sewer along Chalkwell Close that terminates at a manhole at the Site access.

5.1.1 Pre-Development Sanitary Flow

The Site was previously occupied by a single storey elementary school. The calculated pre-development flow contribution is:

- Pre-Development Flow = (pop x 275 L/cap/day x peaking factor) / 86,400 s + Infiltration Allowance
- Pre-Development Flow = (200 pp x 275 L/cap/day x 4.15) / 86400 s + (1.99 ha x 0.26 L/s/ha)
- Pre-Development Flow = **3.10 L/s**

The existing sanitary discharge flow calculated above was calculated using the Region of Peel Sanitary Sewer Design Criteria of 275 litres/capita/day, and an infiltration rate of 0.26 L/s/ha. Based on the above criteria, an existing flow of 3.10 L/s was calculated for the existing Site purpose. In present day, the Site has been abandoned and partially demolished and thus currently generates no flow to the existing sanitary system. Refer to **Appendix C** for detailed calculations.

5.1.2 Post-Development Sanitary Flow

The anticipated sanitary discharge flows for the proposed Site were calculated based on the Region's design criteria outlined in **Table 3-1**, along with the proposed Site statistics found in **Appendix A**. The GFA of the townhouses along with peaking factors were considered in the analysis to evaluate the adequacy of the existing municipal infrastructure. The design inputs for the Site are shown in **Table 5-1** below.

Table 5-1 Equivalent Population Calculations

LAND USE	UNITS	POPULATION DENSITY (PP/UNIT)	TOTAL POPULATION (CAPITA)
Townhouse	180	3.4	612

The calculated post-development flow contribution is:

- Post-Development Flow = (pop x 290 L/cap/day x peaking factor) / 86,400 s + Infiltration Allowance
- Post-Development Flow = (612 pp x 290 L/cap/day x 3.93) / 86400 s + (1.99 ha x 0.20 L/s/ha)
- Post-Development Flow = **8.50 L/s**

The sanitary discharge flow calculated above was calculated using the Region of Peel Sanitary Sewer Design Criteria of 290 litres/capita/day, and an infiltration rate of 0.20 L/s/ha. Based on the above criteria, a net peak design flow of 8.50 L/s was calculated for the subject property. Refer to **Appendix C** for detailed calculations.

The post development sanitary flows calculated and identified above will be used to size and design the local sewers within the development Site.

6 Water Supply System

6.1 Existing System

According to the information reviewed as stated within **Section 1.1**, a 300 mm PVC watermain is located within the Chalkwell Close right-of-way that terminates at the developments Site access.

6.2 Proposed Water Supply

The estimated water consumption for the proposed development was calculated based on the water demand shown in **Table 3-2** in Section 3.3, based on the Region of Peel's watermain design criteria revised June 2010 and the Ontario Building Code.

The water supply for public fire protection was calculated based on the guidelines provided by the FUS, to demonstrate that the existing flows and pressure are adequate to meet the minimum requirement for fire suppression outlined in the FUS.

6.2.1 Proposed Water Demand Requirements

The estimated water consumption was calculated based on the water demand as shown in **Table 3-2** in **Section 3.3**, based on the Region of Peel Watermain Design Criteria. It is anticipated that an average daily consumption of approximately 1.98 L/s, a maximum daily demand of 3.97 L/s and a peak hourly demand of 5.95 L/s will be required to service this development with domestic water.

The Region requires that the Water Supply for Public Fire Protection calculations, as provided by the Fire Underwriters Survey (FUS), be undertaken to determine the water pressure and flow that would be required to service the new development with adequate fire suppression. Arcadis has prepared flow calculations based on the proposed building footprint for the proposed development design concept. According to our calculations, a minimum fire suppression flow of approximately 167 L/s (2650 USGPM) will be required from the nearest hydrant with at least 140 kPa (20 psi) of pressure.

Refer to the detailed demand and fire flow calculations found in **Appendix D**.

6.3 Hydrant Coverage

There is one (1) existing fire hydrant located near the Site access on the north side of Chalkwell Close. Due to the proposed development size, four additional hydrants are proposed within the Site limits to ensure there is adequate hydrant coverage. The proposed hydrants have been positioned such that the minimum coverage requirement of 70 m is satisfied. Refer to **Drawing SS-01** in **Appendix E** for the locations of the existing and proposed hydrants.

6.4 Proposed Watermain Connection

The proposed development will be serviced by a 300 mm diameter water service to service both fire and water demands. The watermain within the Site will service each block with individual connections and be metered collectively. Due to limited access from Site frontages to municipal ROW's containing watermains, the system will not be looped but will have hydrants to terminate the network within the Site. A bulk water meter, backflow preventer and detector check valve will be provided for the Site at the property line at the Site access.

Refer to **Drawings SS-01 and XS-01** for Site Servicing Plan and Cross-Sections of the watermain and service connection in **Appendix E**.

7 Site Grading

7.1 Existing Grades

The existing Site was previously occupied by an elementary school that has since been demolished. Overall, the Site grades generally fall from west to east. Elevations across the existing property range from approximately 134.00 m to 129.29 m. The existing Site is split into two portions falling to two different low points. One portion directs runoff to the northeast corner, EX. CB1, which outlets to Karenza Road, while the other falls southeast directing runoff toward EX. CB2, which outlets to Chalkwell Close. The Chalkwell Close roadway ultimately slopes away from the site toward Sandgate Crescent. Refer to **Appendix A** for the topographical survey of the existing property.

7.2 Proposed Grades and Emergency Overland Flow Routes

The proposed grades will match current drainage patterns wherever feasible and grades will be maintained along the property lines to the extent practical. In the proposed conditions, majority of the Site flows northwest to southeast via private roadways, towards Chalkwell Close. A small portion of the Site will flow towards EX. CB1. The Site's proposed grades range from approximately 133.98 m to 129.29 m. Due to the proximity of the proposed buildings and the property lines, in order to maintain consistent elevations through the structures a retaining wall has been proposed along the northwest and northeast corners of the Site. Overland flow for events, up to and including the 100-yr storm design event, will be captured within the Site. Overland flow for events exceeding the 100-yr design event, will be directed to Chalkwell Close. Refer to **Drawing SG-01** for Site Grading Plan in **Appendix E**.

8 Site Access

According to the architectural plans provided, vehicular access to the Site will be provided via a series of private laneways that connect to the west end of Chalkwell Close. Pedestrian access for the residential units will be located off of Chalkwell Close as well.

9 Utilities

As this development is within an urbanized area of the City, all utilities, including telephone, cable, electricity and gas are assumed to be readily available to service the proposed development at 2620 Chalkwell Close.

10 Conclusions and Recommendations

Based on our investigations, we conclude the following:

10.1 Storm Drainage

To satisfy stormwater management requirements to the City of Mississauga Municipal system the following has been provided:

- Quantity control is to be provided using an orifice pipe to control flow from a combination of storage pipe, structures, chambers and rooftop storage.
- 5 mm retention for water balance is maintained by using on-site infiltration facilities. MECP Enhanced Level Protection (minimum 80% TSS removal) will not be achieved but we will be implementing a best-efforts approach by including inherently clean rooftops and landscaped areas, and a stormwater filtration system for the proposed development.
- The storm discharge from the Site will be directed to the existing maintenance hole and 375 mm storm sewer within Chalkwell Close. A portion of existing uncontrolled flow will continue to flow to the existing catchbasin with a 450 mm lead to Karenza Road.

A summary of the SWM for the Site is follows in **Table 11.1**.

Table 10-1 Stormwater Drainage Summary Table

ALLOWABLE RELEASE RATE:	188.0 L/s
ACTUAL RELEASE RATE (100-YR STORM):	125.7 L/s
REQUIRED STORAGE:	435.4 m ³
ORIFICE PIPE SIZE:	200 mm
REQUIRED WATER BALANCE:	75.4 m ³
REQUIRED TSS% REMOVAL:	80%
PROVIDED TSS% REMOVAL:	81%
METHODS USED FOR QUALITY CONTROL:	Clean Water Roof and Patio Runoff & Permeable Pavers + Stormceptor OGS

10.2 Sanitary Sewers

The expected sanitary discharge flow in the post development condition from the Site is **8.50 L/s**. The flow will be directed to an existing maintenance hole / 250 mm sanitary sewer within Chalkwell Close.

10.3 Water Supply

Water supply for the Site will be provided by a connection made to the existing 300 mm watermain on Chalkwell Close. The average domestic water consumption rates anticipated to be drawn from the existing 300 mm watermain is approximately **1.98 L/s**, a maximum daily demand of **3.97 L/s** and a peak hourly demand of **5.95 L/s** for the proposed townhouse development. The Site requires a minimum flow rate of **167 L/s** (2650 USGPM) at a pressure of 140 kPa (20 psi) to account for both fire and domestic flows. Four additional hydrants are proposed within the Site to provide additional fire coverage.

10.4 Site Grading

The proposed grading of the Site will match the existing grades where possible. To the practical extent, Site flows will be accommodated by the SWM system up to and including the 100-year design event. Emergency overland flow will be directed to the Site access at Chalkwell Close. A portion of the Site and the external drainage flowing into the Site will flow uncontrolled to the existing catchbasin (EX. CB1) in the northeast corner of the Site via grassed swales on the outer side of the proposed retaining wall.

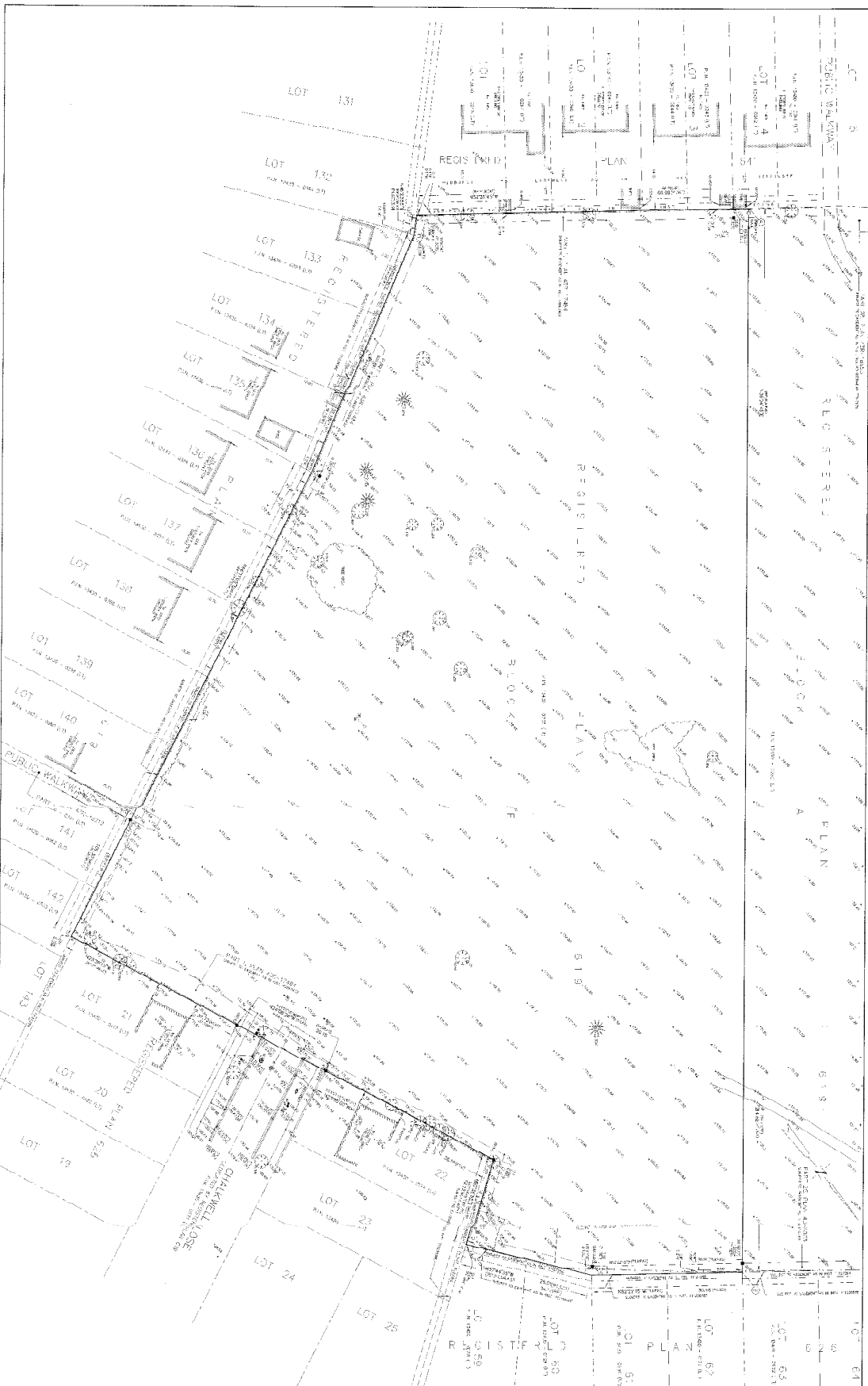
10.5 Recommendations

In summary, the Site and the proposed re-development can be adequately serviced in respect to stormwater drainage, and SWM. The stormwater quantity and quality controls can be implemented in accordance with the City, Region and MECP.

Accordingly, we hereby recommend the adoption of this report as it relates to the provision of servicing works, and for the purposes of re-zoning and Site Plan application approval.

Appendix A

Background Information



**ALL OF BLOCK B
REGISTERED PLAN 619**

CITY OF MISSISSAUGA
REGIONAL MUNICIPALITY OF HELL

SCALE: 1:200

DATE: 2008

BY: [Signature]

FOR: [Signature]

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NOTES AND LEGEND

619 PLAN 7 COORDINATES

NAD 83 UTM ZONE 18 T

EASTING: 650000.000

NORTHING: 4800000.000

SCALE: 1:200

DATE: 2008

BY: [Signature]

FOR: [Signature]

RAVIS SURVEYING INC.

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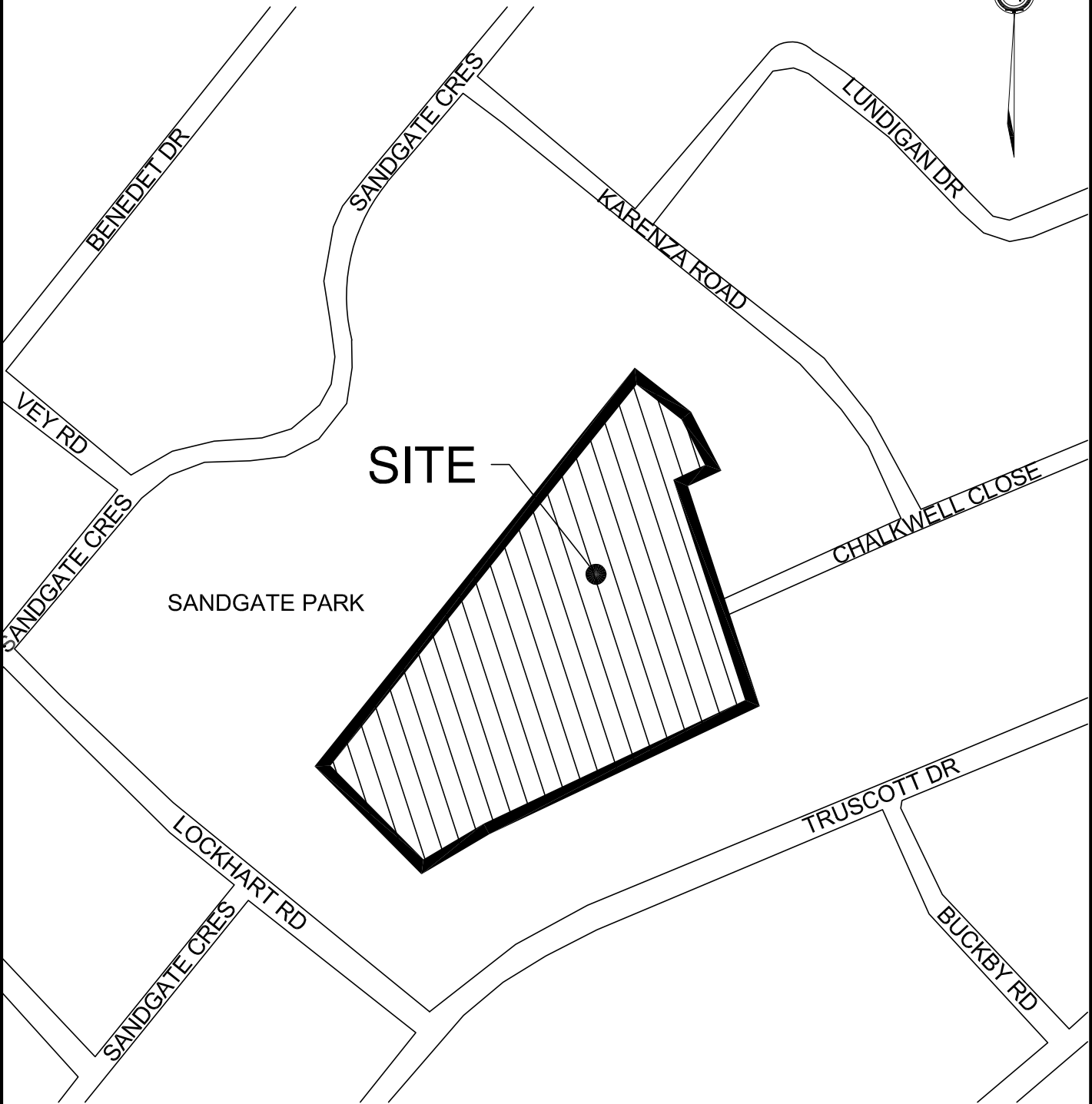
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SITE

SANDGATE PARK

J:\145258_2620Chalkwell\7.0_Production\7.03_Design\04_Civil\Scripts\Colca\Figures\FSR Fig 1-2.dwg (Location Plan)



LOCATION PLAN
2620 CHALKWELL CLOSE
MISSISSAUGA, ONTARIO

DATE:	NOV 2023	PROJECT No.:	145258
SCALE:	N.T.S.	FIGURE No.:	FIG-1



J:\145258_2620Chalkwell\7.0_Production\7.03_Design\04_Civil\Scripts\Calca\Figures\FSR_Fig_1-2.dwg (Aerial Plan)

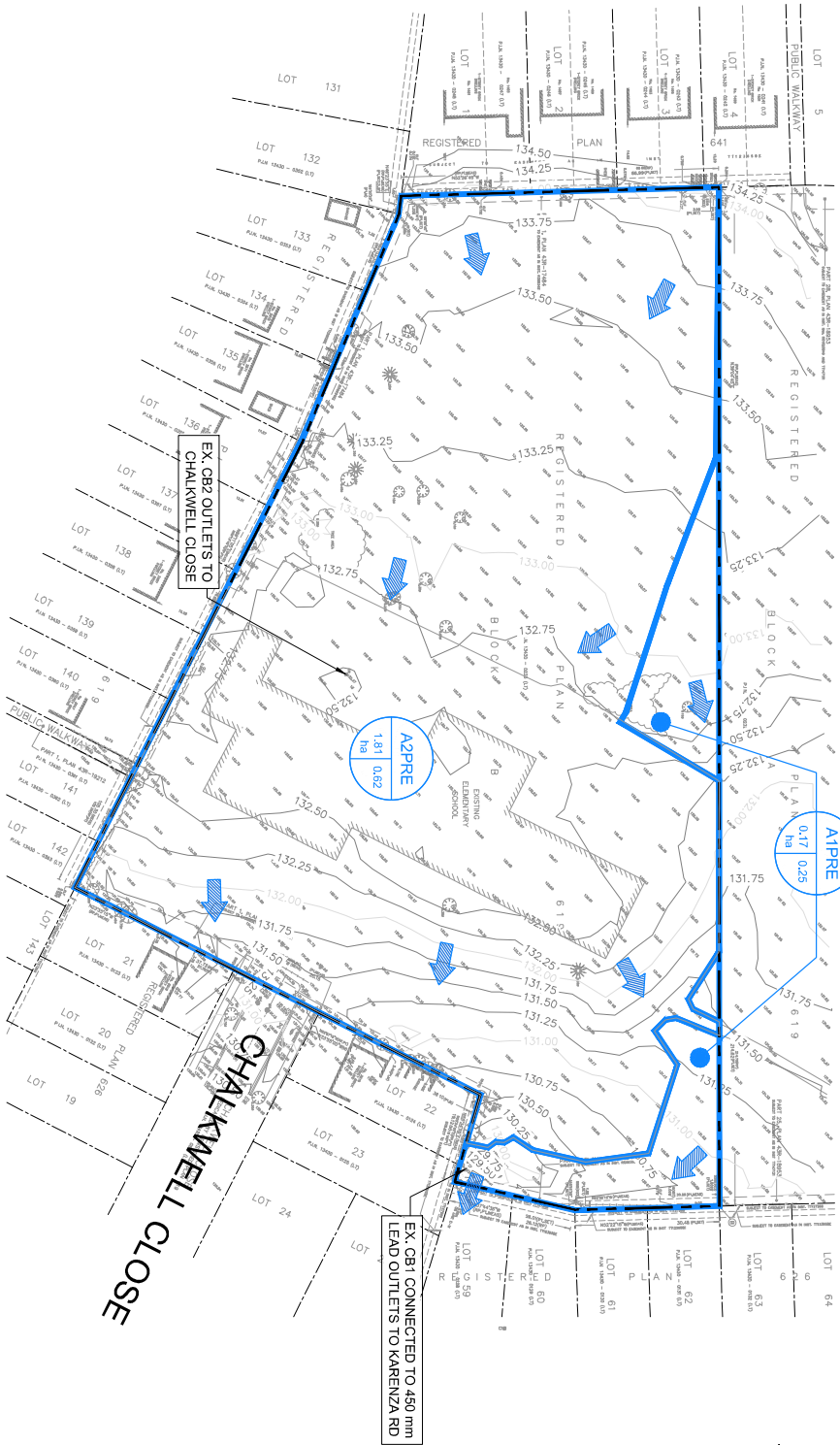


AERIAL PLAN 2620 CHALKWELL CLOSE MISSISSAUGA, ONTARIO			
DATE:	NOV 2023	PROJECT No.:	145258
SCALE:	N.T.S.	FIGURE No.:	FIG-1

Appendix B

Stormwater Data

SANDGATE PARK



- LEGEND**
- PROPERTY BOUNDARY
 - DRAINAGE AREA BOUNDARY
 - MAJOR SYSTEM DIRECTION
 - DRAINAGE AREA IN HECTARES
 - STORM DRAINAGE AREA NUMBER
 - RAINOFF COEFFICIENT

PRE-DEVELOPMENT DRAINAGE AREA PLAN

2620 CHALKWELL CLOSE
MISSISSAUGA, ON.

DATE:	NOVEMBER 2023	PROJECT No.:	145258
SCALE:	1:1000	FIGURE No.:	DAP-01



Pre-Development Composite Runoff Coefficient

2620 Chalkwell Close
145258

Prepared By: AB

November 2023

Drainage Area A1 Pre

	(ha)	
Total Area:	0.17	
ImperVIOUS:	0.00	Coefficient: 0.90
Landscaping:	0.17	Coefficient: 0.25
Composite C:	0.25	
Percent ImperVIOUS	0.00%	

Drainage Area A2 Pre

	(ha)	
Total Area:	1.81	
ImperVIOUS:	1.04	Coefficient: 0.90
Landscaping:	0.77	Coefficient: 0.25
Composite C:	0.62	
Percent ImperVIOUS	57.57%	



**Rational Method
Pre-Development Flow Calculation**

2620 Chalkwell Close
145258

Prepared By: AB

November 2023

Input Parameters

Area Number	Area	C	Tc
	(ha)		(min.)
A1 Pre	0.17	0.25	15.00
A2 Pre	1.81	0.62	15.00

Formula:	$I = a/(T+b)^c$
a,b,c	Constants
T	Time of concentration
I	Rainfall intensity

Rational Method Calculations

IDF Data Set: City of Mississauga

Event **2-Year**

a = 610.0
b = 0.780
c = 4.6

Area Number	A	C	AC	Tc	I	Q	Q
	(ha)			(min.)	(mm/h)	(m ³ /s)	(L/s)
A1 Pre	0.17	0.25	0.04	15	59.9	0.007	7.1
A2 Pre	1.81	0.62	1.13	15	59.9	0.188	188.0

IDF Data Set: City of Mississauga

Event **5-Year**

a = 820.0
b = 0.780
c = 4.6

Area Number	A	C	AC	Tc	I	Q	Q
	(ha)			(min.)	(mm/h)	(m ³ /s)	(L/s)
A1 Pre	0.17	0.25	0.04	15	80.5	0.010	9.6
A2 Pre	1.81	0.62	1.13	15	80.5	0.253	252.7

IDF Data Set: City of Mississauga

Event **10-Year**

a = 1010.0
b = 0.780
c = 4.60

Area Number	A	C	AC	Tc	I	Q	Q
	(ha)			(min.)	(mm/h)	(m ³ /s)	(L/s)
A1 Pre	0.17	0.25	0.04	15	99.2	0.012	11.8
A2 Pre	1.81	0.62	1.13	15	99.2	0.311	311.2

IDF Data Set: City of Mississauga

Event **25-Year**

a = 1160.0
b = 0.780
c = 4.60

Area Number	A	C	AC	Tc	I	Q	Q
	(ha)			(min.)	(mm/h)	(m ³ /s)	(L/s)
A1 Pre	0.17	0.25	0.04	15	113.9	0.014	13.5
A2 Pre	1.81	0.62	1.13	15	113.9	0.357	357.4

IDF Data Set: City of Mississauga

Event **50-Year**

a = 1300.0
b = 0.780
c = 4.70

Area Number	A	C	AC	Tc	I	Q	Q
	(ha)			(min.)	(mm/h)	(m ³ /s)	(L/s)
A1 Pre	0.17	0.25	0.04	15	127.1	0.015	15.1
A2 Pre	1.81	0.62	1.13	15	127.1	0.399	399.0

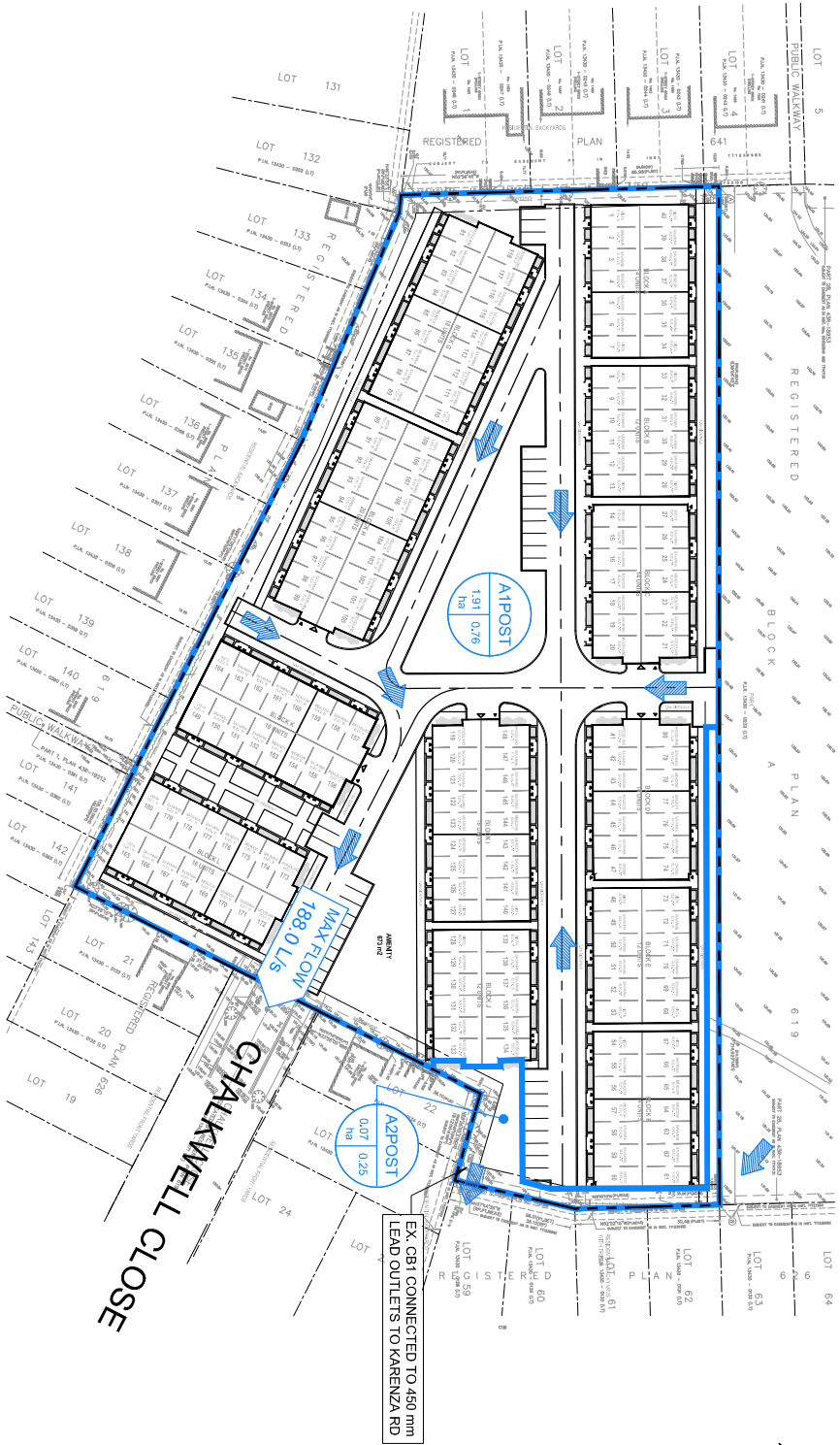
IDF Data Set: City of Mississauga

Event **100-Year**

a = 1450.0
b = 0.780
c = 4.90

Area Number	A	C	AC	Tc	I	Q	Q
	(ha)			(min.)	(mm/h)	(m ³ /s)	(L/s)
A1 Pre	0.17	0.25	0.04	15	140.7	0.017	16.7
A2 Pre	1.81	0.62	1.13	15	140.7	0.442	441.5

SANDGATE PARK



LEGEND

	PROPERTY BOUNDARY
	DRAINAGE AREA BOUNDARY
	MAJOR SYSTEM DIRECTION

	STORM DRAINAGE AREA NUMBER
	RUNOFF COEFFICIENT

POST-DEVELOPMENT DRAINAGE AREA PLAN

2620 CHALKWELL CLOSE
MISSISSAUGA, ON.

DATE:	NOVEMBER 2023	PROJECT No.:	145258
SCALE:	1:1000	FIGURE No.:	DAF-02



Post-Development Composite Runoff Coefficient

2620 Chalkwell Close
145258

Prepared By: AB

November 2023

Drainage Area A1 Post

	(ha)	
Total Area:	1.91	
ImperVIOUS:	1.51	Coefficient: 0.90
Landscaping:	0.40	Coefficient: 0.25
Composite C:	0.76	
Percent ImperVIOUS	78.95%	

Drainage Area A2 Post

	(ha)	
Total Area:	0.07	
ImperVIOUS:	0.00	Coefficient: 0.90
Landscaping:	0.07	Coefficient: 0.25
Composite C:	0.25	
Percent ImperVIOUS	0.00%	



Prepared By: AB

**Rational Method
Post-Development Flow Calculation**

2620 Chalkwell Close
145258
November 2023

Input Parameters

Area Number	Area (ha)	C	Tc (min.)
A1 Post	1.91	0.65	15.00
A2 Post	0.07	0.25	15.00

Formula:	$I = a/(T+b)^c$	
	a,b,c	Constants
	T	Time of concentration
	I	Rainfall intensity

Rational Method Calculations

IDF Data Set: City of Mississauga
Event **2-Year**
a = 610
b = 0.78
c = 4.6

Area Number	A (ha)	C	AC	Tc (min.)	I (mm/h)	Q (m ³ /s)	Q (L/s)
A1 Post	1.91	0.65	1.24	15	59.9	0.207	206.5
A2 Post	0.07	0.25	0.02	15	59.9	0.003	2.9

IDF Data Set: City of Mississauga
Event **5-Year**
a = 820
b = 0.78
c = 4.6

Area Number	A (ha)	C	AC	Tc (min.)	I (mm/h)	Q (m ³ /s)	Q (L/s)
A1 Post	1.91	0.65	1.24	15	80.5	0.278	277.7
A2 Post	0.07	0.25	0.02	15	80.5	0.004	3.9

IDF Data Set: City of Mississauga
Event **10-Year**
a = 1010.0
b = 0.780
c = 4.6

Area Number	A (ha)	C	AC	Tc (min.)	I (mm/h)	Q (m ³ /s)	Q (L/s)
A1 Post	1.91	0.65	1.24	15	99.2	0.342	342.0
A2 Post	0.07	0.25	0.02	15	99.2	0.005	4.8

IDF Data Set: City of Mississauga
Event **25-Year**
a = 1160.0
b = 0.780
c = 4.6

Area Number	A (ha)	C	AC	Tc (min.)	I (mm/h)	Q (m ³ /s)	Q (L/s)
A1 Post	1.91	0.65	1.24	15	113.9	0.393	392.8
A2 Post	0.07	0.25	0.02	15	113.9	0.006	5.5

IDF Data Set: City of Mississauga
Event **50-Year**
a = 1300.0
b = 0.780
c = 4.7

Area Number	A (ha)	C	AC	Tc (min.)	I (mm/h)	Q (m ³ /s)	Q (L/s)
A1 Post	1.91	0.65	1.24	15	127.1	0.438	438.4
A2 Post	0.07	0.25	0.02	15	127.1	0.006	6.2

IDF Data Set: City of Mississauga
Event **100-Year**
a = 1450.0
b = 0.780
c = 4.9

Area Number	A (ha)	C	AC	Tc (min.)	I (mm/h)	Q (m ³ /s)	Q (L/s)
A1 Post	1.91	0.65	1.24	15	140.7	0.485	485.2
A2 Post	0.07	0.25	0.02	15	140.7	0.007	6.8



**Modified Rational Method - 2 Year Storm
Site Flow and Storage Summary**

2620 Chalkwell Close
145258

Prepared By: AB

November-2023

2 Yr Design Storm		A1Post Controlled			A2Post Uncontrolled			Flow Summary	
a=	610.00	Area=	1.91	ha	Area=	0.07	ha	Target Flow 187.96 L/s Total Design Flow 100.00 L/s	
b=	0.780	"C" =	0.76		"C" =	0.25			
c=	4.60	AC1=	1.46		AC1=	0.02			
I=	A/(T+c)^b	Tc =	15.00	min	Tc =	15.00	min		
		Time Increment =	5.00	min	Time Increment =	5.00	min		
		Orifice Controlled Flow =	100.00	L/s	Uncontrolled Release Rate =	2.91	L/s		
		Max. Required Storage =	128.27	m ³					

Time (min)	Rainfall Intensity (mm/hr)	Storm Runoff (m ³ /s)	Runoff Volume (m ³)	Target Release Volume (m ³)	Total Required Storage Volume (m ³)	Storm Runoff (m ³ /s)	Runoff Volume (m ³)
15.0	59.9	0.243	218.27	90.00	128.27	0.0029	2.62
20.0	50.2	0.203	243.76	120.00	123.75	0.0024	2.93
25.0	43.4	0.176	263.75	150.00	113.75	0.0021	3.17
30.0	38.4	0.156	280.22	180.00	100.22	0.0019	3.36
35.0	34.6	0.140	294.25	210.00	84.25	0.0017	3.53
40.0	31.5	0.128	306.50	240.00	66.50	0.0015	3.68
45.0	29.0	0.118	317.39	270.00	47.39	0.0014	3.81
50.0	26.9	0.109	327.20	300.00	27.20	0.0013	3.93
55.0	25.2	0.102	336.14	330.00	6.14	0.0012	4.04
60.0	23.6	0.096	344.37	360.00	0.00	0.0011	4.13
65.0	22.3	0.090	351.99	390.00	0.00	0.0011	4.23
70.0	21.1	0.085	359.10	420.00	0.00	0.0010	4.31
75.0	20.1	0.081	365.77	450.00	0.00	0.0010	4.39
80.0	19.1	0.078	372.04	480.00	0.00	0.0009	4.47
85.0	18.3	0.074	377.98	510.00	0.00	0.0009	4.54
90.0	17.5	0.071	383.62	540.00	0.00	0.0009	4.61
95.0	16.9	0.068	388.99	570.00	0.00	0.0008	4.67
100.0	16.2	0.066	394.11	600.00	0.00	0.0008	4.73
105.0	15.6	0.063	399.02	630.00	0.00	0.0008	4.79
110.0	15.1	0.061	403.72	660.00	0.00	0.0007	4.85
115.0	14.6	0.059	408.24	690.00	0.00	0.0007	4.90
120.0	14.2	0.057	412.60	720.00	0.00	0.0007	4.95
125.0	13.7	0.056	416.80	750.00	0.00	0.0007	5.00
130.0	13.3	0.054	420.86	780.00	0.00	0.0006	5.05
135.0	13.0	0.052	424.79	810.00	0.00	0.0006	5.10
140.0	12.6	0.051	428.60	840.00	0.00	0.0006	5.15
145.0	12.3	0.050	432.29	870.00	0.00	0.0006	5.19
150.0	12.0	0.048	435.87	900.00	0.00	0.0006	5.23
155.0	11.7	0.047	439.36	930.00	0.00	0.0006	5.27
160.0	11.4	0.046	442.75	960.00	0.00	0.0006	5.32
165.0	11.1	0.045	446.05	990.00	0.00	0.0005	5.35
170.0	10.9	0.044	449.27	1020.00	0.00	0.0005	5.39
175.0	10.6	0.043	452.41	1050.00	0.00	0.0005	5.43
180.0	10.4	0.042	455.48	1080.00	0.00	0.0005	5.47
185.0	10.2	0.041	458.47	1110.00	0.00	0.0005	5.50
190.0	10.0	0.040	461.40	1140.00	0.00	0.0005	5.54
195.0	9.8	0.040	464.26	1170.00	0.00	0.0005	5.57
200.0	9.6	0.039	467.06	1200.00	0.00	0.0005	5.61
205.0	9.4	0.038	469.81	1230.00	0.00	0.0005	5.64
210.0	9.3	0.037	472.50	1260.00	0.00	0.0005	5.67
215.0	9.1	0.037	475.14	1290.00	0.00	0.0004	5.70
220.0	8.9	0.036	477.72	1320.00	0.00	0.0004	5.74
225.0	8.8	0.036	480.26	1350.00	0.00	0.0004	5.77
230.0	8.6	0.035	482.75	1380.00	0.00	0.0004	5.80
235.0	8.5	0.034	485.20	1410.00	0.00	0.0004	5.82
240.0	8.4	0.034	487.61	1440.00	0.00	0.0004	5.85
245.0	8.2	0.033	489.97	1470.00	0.00	0.0004	5.88
250.0	8.1	0.033	492.29	1500.00	0.00	0.0004	5.91
255.0	8.0	0.032	494.58	1530.00	0.00	0.0004	5.94
260.0	7.9	0.032	496.83	1560.00	0.00	0.0004	5.96
265.0	7.8	0.031	499.04	1590.00	0.00	0.0004	5.99
270.0	7.6	0.031	501.22	1620.00	0.00	0.0004	6.02
275.0	7.5	0.031	503.37	1650.00	0.00	0.0004	6.04
280.0	7.4	0.030	505.48	1680.00	0.00	0.0004	6.07
285.0	7.3	0.030	507.57	1710.00	0.00	0.0004	6.09
290.0	7.2	0.029	509.62	1740.00	0.00	0.0004	6.12
295.0	7.1	0.029	511.65	1770.00	0.00	0.0003	6.14



**Modified Rational Method - 100 Year Storm
Site Flow and Storage Summary**

2620 Chalkwell Close
145258

Prepared By: AB

November-2023

100 Yr Design Storm		A1 Post Controlled			A2 Post Uncontrolled			Flow Summary	
a=	1450.00	Area=	1.91	ha	Area=	0.07	ha	Target Flow 187.96 L/s Total Design Flow 125.67 L/s	
b=	0.780	"C" =	0.76		"C" =	0.25			
c=	4.90	AC1=	1.46		AC1=	0.02			
l=	A/(T+c)^b	Tc =	15.00	min	Tc =	15.00	min		
		Time Increment =	5.00	min	Time Increment =	5.00	min		
		Orifice Controlled Flow =	125.67	L/s	Uncontrolled Release Rate =	6.84	L/s		
		Max. Required Storage =	435.41	m ³					

Time (min)	Rainfall Intensity (mm/hr)	Storm Runoff (m ³ /s)	Runoff Volume (m ³)	Target Release Volume (m ³)	Total Required Storage Volume (m ³)	Storm Runoff (m ³ /s)	Runoff Volume (m ³)
15.0	140.7	0.570	512.72	113.11	399.61	0.0068	6.16
20.0	118.1	0.478	573.97	150.81	423.16	0.0057	6.89
25.0	102.4	0.415	622.02	188.51	433.51	0.0050	7.47
30.0	90.8	0.368	661.62	226.21	435.41	0.0044	7.94
35.0	81.8	0.331	695.35	263.91	431.43	0.0040	8.35
40.0	74.6	0.302	724.77	301.62	423.15	0.0036	8.70
45.0	68.7	0.278	750.91	339.32	411.59	0.0033	9.01
50.0	63.8	0.258	774.45	377.02	397.43	0.0031	9.30
55.0	59.6	0.241	795.90	414.72	381.18	0.0029	9.55
60.0	56.0	0.227	815.63	452.42	363.20	0.0027	9.79
65.0	52.8	0.214	833.90	490.13	343.77	0.0026	10.01
70.0	50.0	0.203	850.93	527.83	323.10	0.0024	10.22
75.0	47.6	0.193	866.89	565.53	301.36	0.0023	10.41
80.0	45.4	0.184	881.93	603.23	278.70	0.0022	10.59
85.0	43.4	0.176	896.14	640.93	255.21	0.0021	10.76
90.0	41.6	0.168	909.63	678.64	231.00	0.0020	10.92
95.0	40.0	0.162	922.47	716.34	206.13	0.0019	11.07
100.0	38.5	0.156	934.73	754.04	180.69	0.0019	11.22
105.0	37.1	0.150	946.46	791.74	154.72	0.0018	11.36
110.0	35.8	0.145	957.71	829.44	128.27	0.0017	11.50
115.0	34.7	0.140	968.52	867.15	101.38	0.0017	11.63
120.0	33.6	0.136	978.93	904.85	74.09	0.0016	11.75
125.0	32.6	0.132	988.98	942.55	46.43	0.0016	11.87
130.0	31.6	0.128	998.68	980.25	18.42	0.0015	11.99
135.0	30.7	0.124	1008.06	1017.96	0.00	0.0015	12.10
140.0	29.9	0.121	1017.15	1055.66	0.00	0.0015	12.21
145.0	29.1	0.118	1025.97	1093.36	0.00	0.0014	12.32
150.0	28.4	0.115	1034.53	1131.06	0.00	0.0014	12.42
155.0	27.7	0.112	1042.85	1168.76	0.00	0.0013	12.52
160.0	27.0	0.109	1050.94	1206.47	0.00	0.0013	12.62
165.0	26.4	0.107	1058.83	1244.17	0.00	0.0013	12.71
170.0	25.8	0.105	1066.51	1281.87	0.00	0.0013	12.80
175.0	25.3	0.102	1074.00	1319.57	0.00	0.0012	12.89
180.0	24.7	0.100	1081.32	1357.27	0.00	0.0012	12.98
185.0	24.2	0.098	1088.46	1394.98	0.00	0.0012	13.07
190.0	23.7	0.096	1095.45	1432.68	0.00	0.0012	13.15
195.0	23.3	0.094	1102.28	1470.38	0.00	0.0011	13.23
200.0	22.8	0.092	1108.97	1508.08	0.00	0.0011	13.31
205.0	22.4	0.091	1115.52	1545.78	0.00	0.0011	13.39
210.0	22.0	0.089	1121.93	1583.49	0.00	0.0011	13.47
215.0	21.6	0.087	1128.22	1621.19	0.00	0.0010	13.54
220.0	21.2	0.086	1134.39	1658.89	0.00	0.0010	13.62
225.0	20.9	0.084	1140.44	1696.59	0.00	0.0010	13.69
230.0	20.5	0.083	1146.38	1734.29	0.00	0.0010	13.76
235.0	20.2	0.082	1152.22	1772.00	0.00	0.0010	13.83
240.0	19.9	0.080	1157.95	1809.70	0.00	0.0010	13.90
245.0	19.5	0.079	1163.59	1847.40	0.00	0.0010	13.97
250.0	19.2	0.078	1169.13	1885.10	0.00	0.0009	14.04
255.0	19.0	0.077	1174.58	1922.80	0.00	0.0009	14.10
260.0	18.7	0.076	1179.94	1960.51	0.00	0.0009	14.17
265.0	18.4	0.075	1185.22	1998.21	0.00	0.0009	14.23

Orifice Control

2620 Chalkwell Close

145258

November-2023

ORIFICE PIPE

$$Q = C \times A \times \sqrt{2 \times g \times h}$$

Storm Event	Orifice Coefficient	Diameter of Orifice (mm)	Orifice Invert (m)	Headwater Elevation (m)	Total Head (m)	Area of Orifice (m ²)	Release Rate (L/s)
2-Year	0.82	200	129.59	130.46	0.77	0.031	100.00
5-Year	0.82	200	129.59	130.53	0.85	0.031	105.00
10-Year	0.82	200	129.59	130.62	0.93	0.031	110.00
25-Year	0.82	200	129.59	130.70	1.02	0.031	115.00
50-Year	0.82	200	129.59	130.79	1.11	0.031	120.00
100-Year	0.82	200	129.59	130.90	1.21	0.031	125.67



ARCADIS

Water Quality Calculations

2620 Chalkwell Close
145258

Prepared By: AB

November-2023

Surface	Method	Effective TSS Removal	Area (ha)	% Area of Site	Overall TSS Removal
Conventional Roof	Inherent	80%	0.86	31%	25%
Landscaped	Inherent	80%	0.40	14%	12%
Paved Controlled	OGS	80%	1.51	54%	44%
Total			2.77	100%	81%

Appendix C

Sanitary Data

Appendix D

Water Data

DOMESTIC WATER DEMAND



Project: 2620 Chalkwell Close
 Date: Nov 2023
 Cal'ed by: AB

Proj. # 145258

Note:

Based on the City of St.Catherines Standards, Niagara Region 2021 Water and Wastewater Master Servicing Plan and the Ontario Building Code, Section 3.1.17.1 "Occupant Load Determination", Table 8.1.17.1.

	Site Component	PROP		
Residential Occupancy Data	Studio / 1 / 1+d bed units	0		
	People per unit	<i>n/a</i>		
	2 bed units / 2+D	0		
	People per unit	<i>n/a</i>		
	3 bed units	0		
	People per unit	<i>n/a</i>		
	4 bed units	0		
	People per unit	<i>n/a</i>		
	Townhouse units	180		
People per unit	3.4			

Unit Quantity by Site Component	Water Demand	Units	Equivalent Population (persons)		
Residential Occupancies					
Residential	280	L/person/day	612.0	-	-

Daily Flow Rate (L/d)					
Residential Occupancies					
Residential		171,360.00	171,360.00	0	0

	Total Flow			
Average day (L/d)	171,360.00	171,360.00	0.00	0.00
Average day (L/s)	1.98	1.98	0.00	0.00
Max. day (L/d)	342,720.00	342,720.00	0.00	0.00
Max day (L/s)	3.97	3.97	0.00	0.00
Min. hour (L/hr)	2,856.00	2,856.00	0.00	0.00
Peak hour (L/hr)	21,420.00	21,420.00	0.00	0.00
Peak hour (L/s)	5.95	5.95	0.00	0.00

Note:

Based on the Region of Peel Watermain Guidelines and MECP Design Guidelines for Drinking Water Systems Table 3-1:
Peaking Factors

Peaking Factors			
Land Use	Minimum Hour	Peak Hour	Maximum Day
Residential	0.4	3.00	2.00

FIRE FLOW CALCULATION



Project: 2620 Chalkwell Close
 Date: Nov 2023
 Calc'ed by: AB

Proj. # 145258

Fire Resistive Construction:	YES	Site Component:			
<p>The following calculations are for the proposed development and are based on the largest floorplate area. The FUS requires that a minimum water supply source 'F' be provided at 150KPa. The minimum flow 'F' can be calculated as such:</p> $F = 220C \sqrt{A}$ <p><i>F = Required fire flow L/min</i> <i>C = Coefficient related to construction</i> <i>A = Total area in m²</i></p> <p>*Calculations, formulas and factors are as per Fire Underwriter's Survey (FUS) Water Supply for Public Fire Protection</p>	Total Floor Area	Largest Floor Area (m2)	581		
		Area Above (m2)	0		
		Area Below (m2)	0		
		Total Floor Area (m2)	581		
	Flow (F)	C (dimensionless)	1.5		
		A (m2)	581		
		F (L/min)	8000		
	Reduction Factor	F (L/min)	8000		
		f ₁ (dimensionless)	0.85		
		F' = F x f ₁ (L/min)	6800		
		<i>f₁ = occupancy factor; ie, Residential, f₁ = 0.85; for Retail or Commercial, f₁ = 1.00</i>			
	Sprinkler and Exposure Increase or Decrease	f ₂ (sprinkler factor)	0%		
		North Side	0%		
		East Side	5%		
		South Side	15%		
West Side		20%			
f ₃		40%			
<i>f₃ = Exposure factor not to exceed 75%, determined as per FUS Guide Item 4, page 18)</i>					
		F' (L/min)	6800		
		<i>S = F' * f₂ (L/min)</i>	0		
		<i>E = F' * f₃ (L/min)</i>	2720		
F'' = F' - S + E (L/min) rounded to nearest 1,000		10000			
		F'' (L/s)	167		
		F'' (USGPM)	2650		

Table 1

Sprinkler Reduction Factor (f ₂)		
No Sprinkler System	Sprinklered	Sprink. + Supervised
0%	30%	50%

Table 2

Construction Type "C" Factor			
Wood Frame	Ordinary Construction	Non-Combustible	Fire Resistive
1.5	1	0.80	0.60

Table 3

Occupancy Factor (f ₁)				
Rapid Burning	Free Burning	Combustible	Limited Combustible	Non-Combust.
25%	15%	0%	-15%	-25%

Table 4

Exposure Charge		
0 to 3m	3.1 to 10m	10.1 to 20m
25%	20%	15%

Appendix E

Engineering Figures



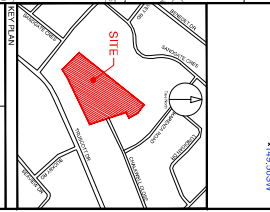
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APPROVED PROFESSIONAL ENGINEER'S CERTIFICATE
 DATE: 22-2023

DATE: 22-2023

SYMBOL	DESCRIPTION
(Symbol)	1.5% GRADE
(Symbol)	0.5% GRADE
(Symbol)	0.7% GRADE
(Symbol)	0.8% GRADE
(Symbol)	0.9% GRADE
(Symbol)	1.0% GRADE
(Symbol)	1.1% GRADE
(Symbol)	1.2% GRADE
(Symbol)	1.3% GRADE
(Symbol)	1.4% GRADE
(Symbol)	1.5% GRADE
(Symbol)	1.6% GRADE
(Symbol)	1.7% GRADE
(Symbol)	1.8% GRADE
(Symbol)	1.9% GRADE
(Symbol)	2.0% GRADE
(Symbol)	2.1% GRADE
(Symbol)	2.2% GRADE
(Symbol)	2.3% GRADE
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(Symbol)	10.0% GRADE



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PROJECT NO.
 145258

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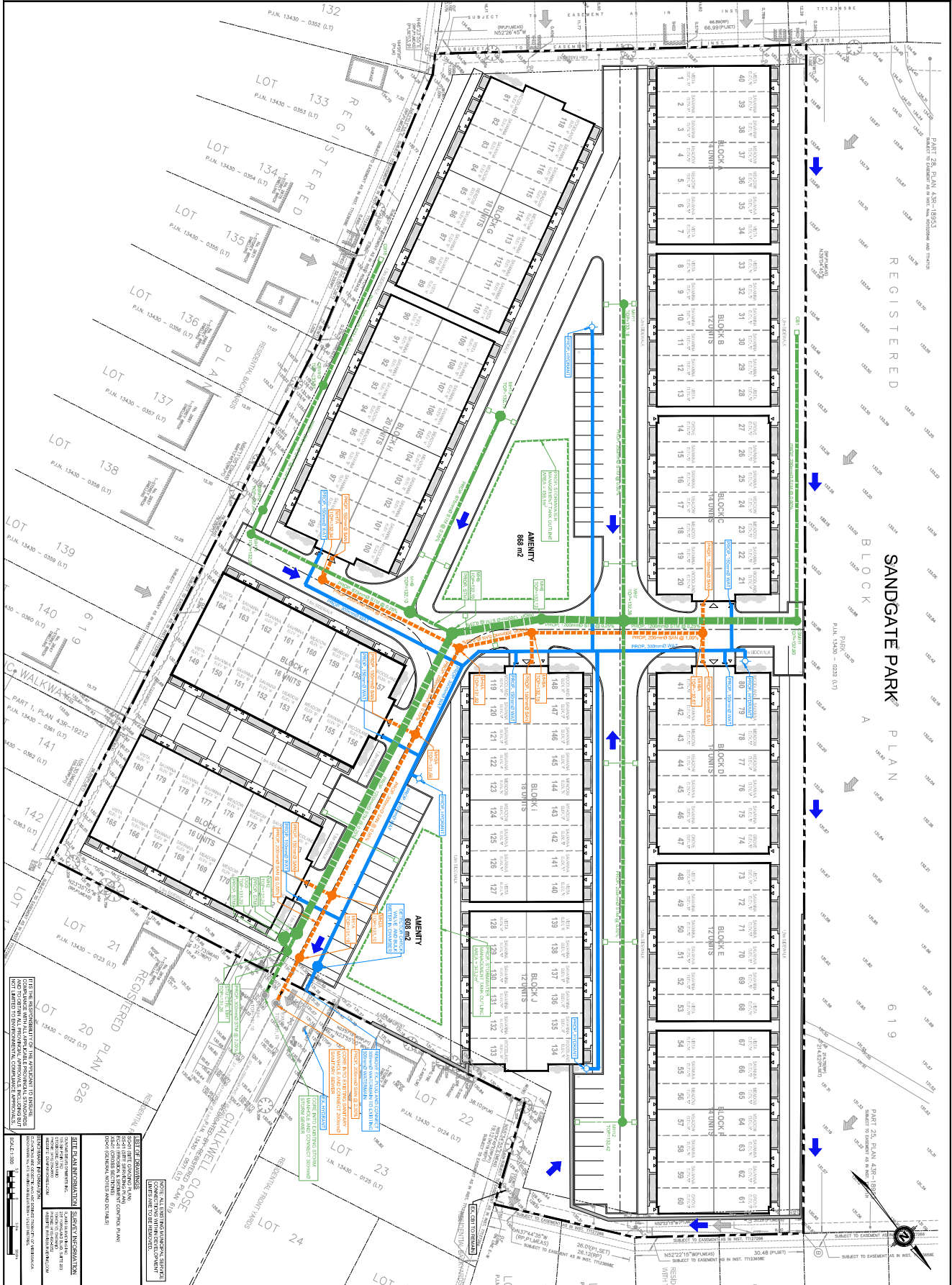
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SHEET NUMBER
SG-01

SHEET TITLE
SITE GRADING PLAN



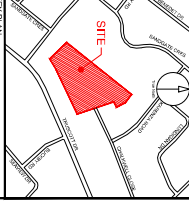
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NO.	DESCRIPTION	DATE
1	ISSUE FOR CONSTRUCTION	DEC-22-2023

LEGEND

- EXISTING BUILDING FOOTPRINT
- EXISTING DRIVEWAY
- EXISTING SIDEWALK
- EXISTING CURB
- EXISTING UTILITY
- EXISTING TREE
- EXISTING LANDSCAPE
- EXISTING FENCE
- EXISTING SIGNAGE
- EXISTING LIGHTING
- EXISTING PAVEMENT
- EXISTING CONCRETE
- EXISTING METAL
- EXISTING WOOD
- EXISTING BRICK
- EXISTING STONE
- EXISTING GLASS
- EXISTING ROOF
- EXISTING FOUNDATION
- EXISTING STRUCTURE
- EXISTING EQUIPMENT
- EXISTING FURNITURE
- EXISTING FIXTURES
- EXISTING FINISHES
- EXISTING MATERIALS
- EXISTING CONDITIONS
- EXISTING UTILITIES
- EXISTING SERVICES
- EXISTING CONNECTIONS
- EXISTING INTERFACES
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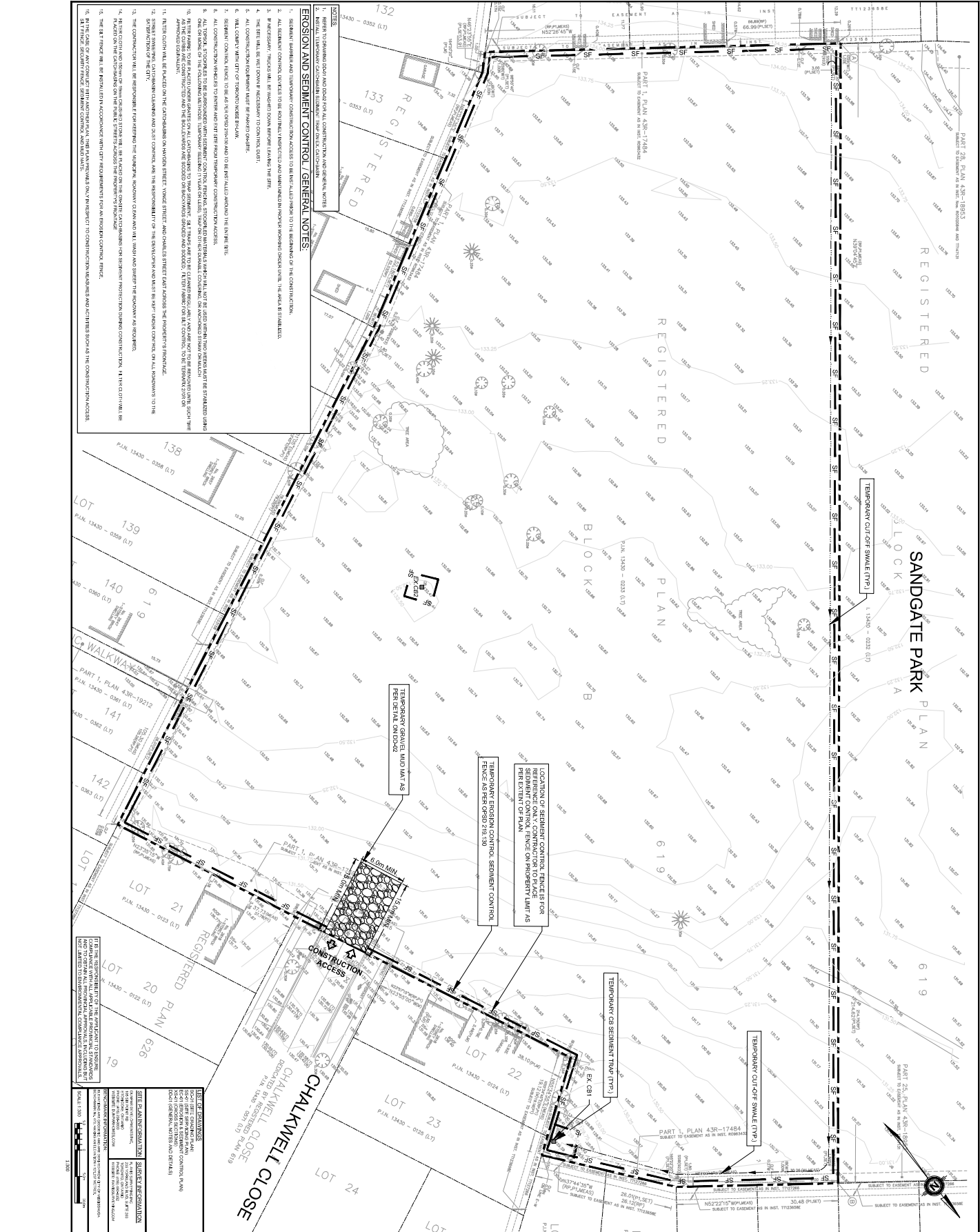
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2820 CHALKWELL CLOSE
 CITY OF MISSISSAUGA

PROJECT NO: 145258
 DESIGNER: [Name]
 APPROVED BY: [Name]

SITE SERVING PLAN

SHEET NUMBER: SS-01
 ISSUE: 01



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REVISIONS

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1	ISSUE FOR PERMIT SUBMISSION	05/27/2020

LEGEND

- TEMPORARY EROSION CONTROL SEDIMENT CONTROL FENCE
- TEMPORARY EROSION CONTROL SEDIMENT CONTROL FENCE ON PROPERTY LIMIT AS PER EXHIBIT OF PLAN
- TEMPORARY EROSION CONTROL SEDIMENT CONTROL FENCE AS PER OHS&S 218.130
- TEMPORARY GAUGES AND MUD PITS AS PER DETAIL ON D02Z
- TEMPORARY CUT-OFF SMALL (TSP?)
- TEMPORARY DRAINAGE DITCH
- TEMPORARY DRAINAGE DITCH WITH LAKE
- TEMPORARY CUT-OFF GRADE

SCALE
 1" = 30'-0"

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 CITY OF MISSISSAUGA

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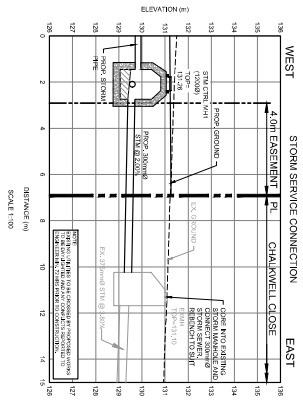
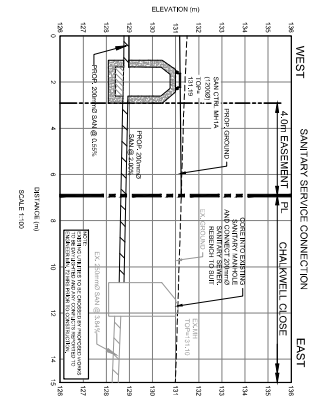
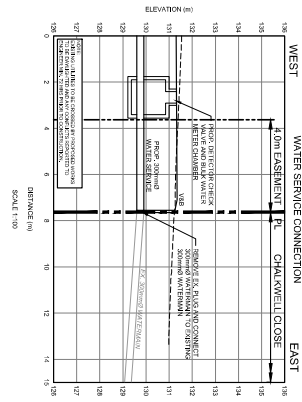
PROJECT INFORMATION

PROJECT NO.	14528
DESIGNED BY	MM
CHECKED BY	MM
PROJECT MARK	APPROVED BY
NO	MM

SHEET TITLE
 EROSION & SEDIMENT CONTROL PLAN

SHEET NUMBER
 EC-01 01

DATE
 05/27/2020

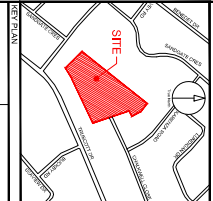


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COMPONENT

NO.	DESCRIPTION	DATE
1	ROOF DRAIN CONNECTION	20-02-2020

LEGEND



PROJECT	2020 CHALKWELL CLOSE CITY OF MISSISSAUGA
PROJECT NO.	145258
DATE	2020-02-20
DESIGNED BY	NS
APPROVED BY	NS
CROSS SECTIONS	
SHEET NUMBER	XS-01 01

LET OF DRAWINGS

NO.	DESCRIPTION	DATE
1	LET OF DRAWINGS	20-02-2020

REVISIONS

NO.	DESCRIPTION	DATE
1	REVISIONS	20-02-2020

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